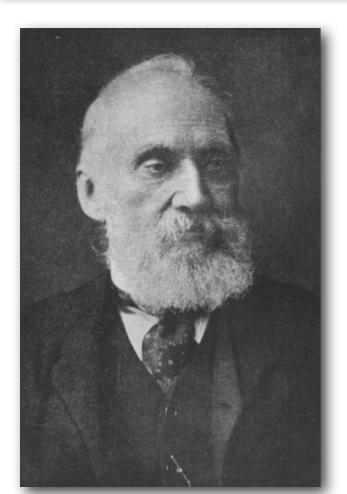
Magnetic Measurements

R. Schäfer,

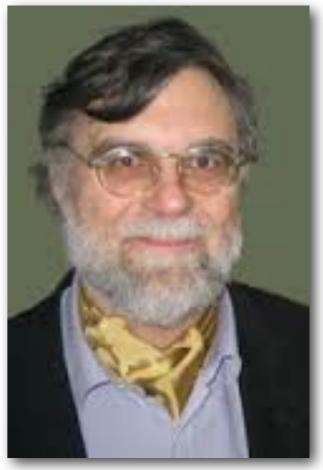
Leibniz Institute for Solid State and Materials Research (IFW) Dresden, Germany

Why Magnetic Measurements?



"I often say that when you can measure what you are speaking about and express it in numbers you know something about it. But when you cannot measure it, when you cannot express it in numbers, your knowledge is of a meager and unsatisfactory kind."

"Magnetism is an experimental science"
Mike Coey, 2010

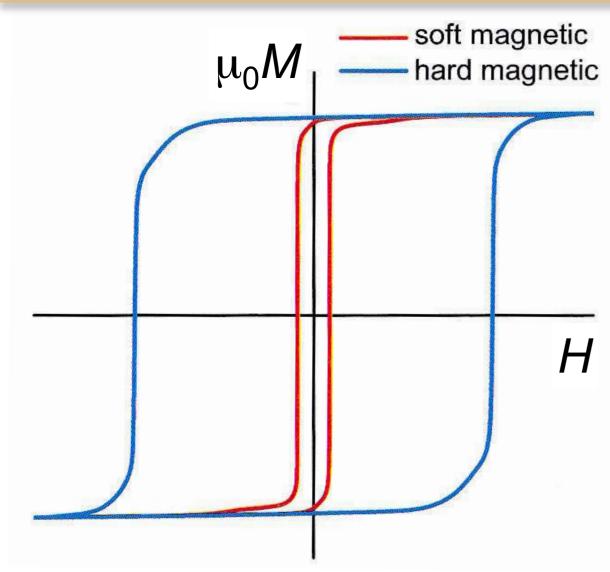


"No clear understanding of magnetism can be attained without a sound knowledge of the way in which magnetic properties are measured."

B.D. Cullity & CD Graham: Introduction to Magnetic Materials, 2009

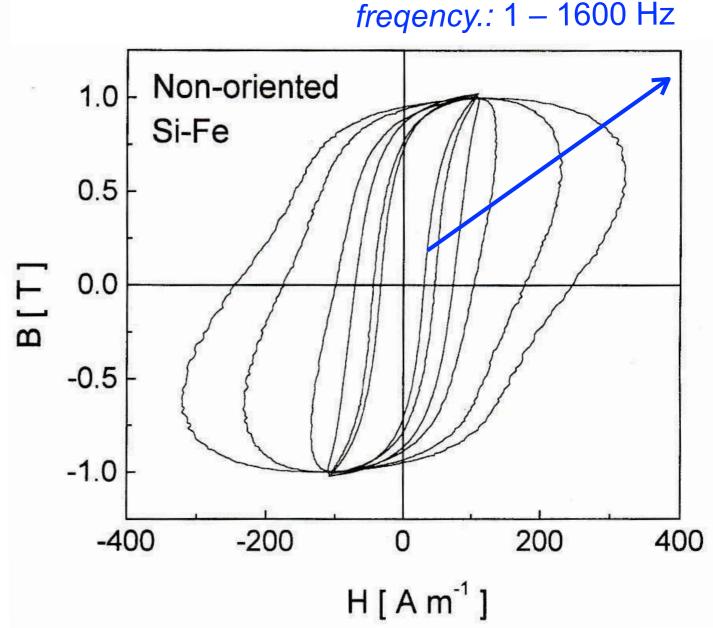
Lord Kelvin, 1883

What needs to be measured?



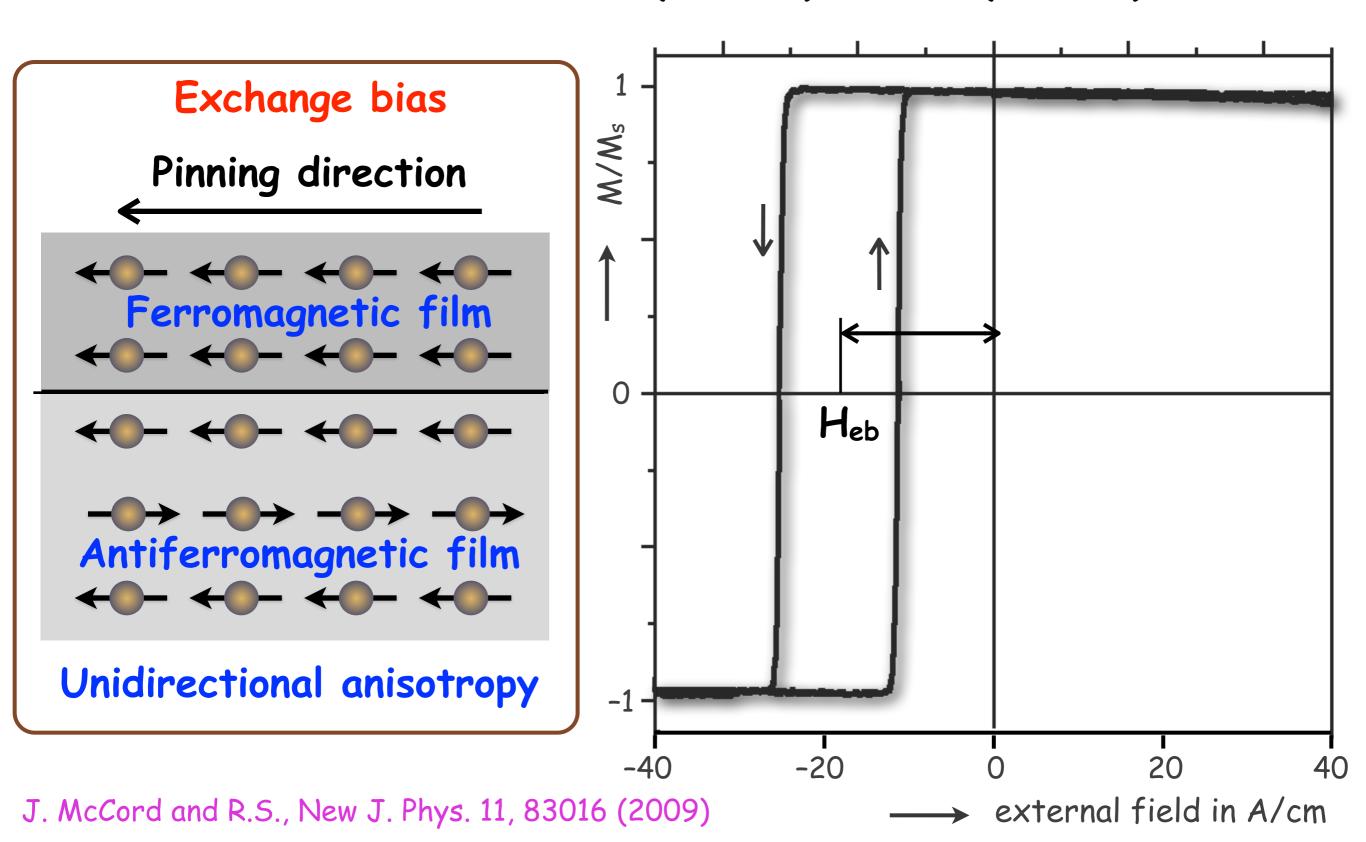
Hysteresis curve:

- ·coercivity, remanence
- permeabilities
- · energy loss
- · interactions
- ·etc.



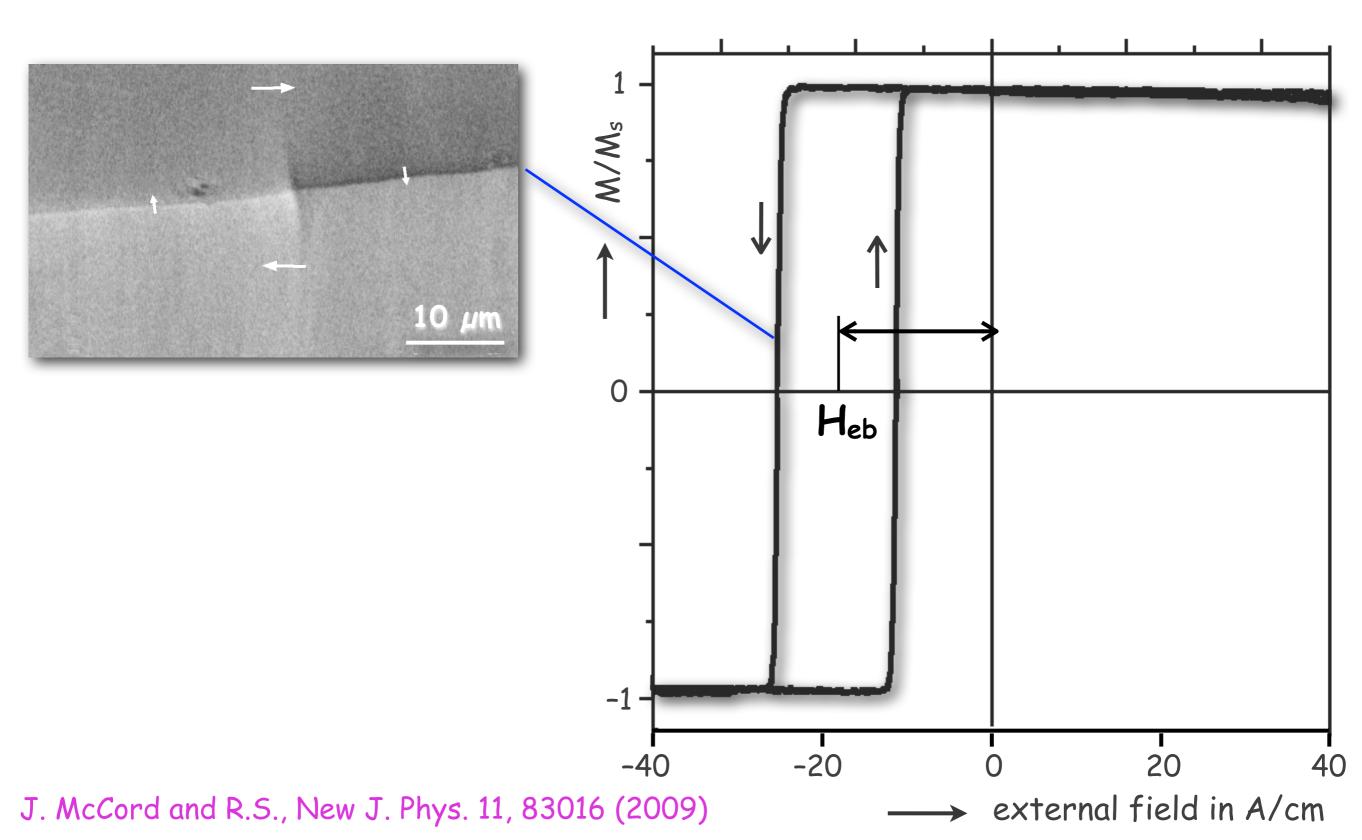
M(H) loop and domains

Reversal of Ni₈₁Fe₁₉ (30 nm) / NiO (30 nm)



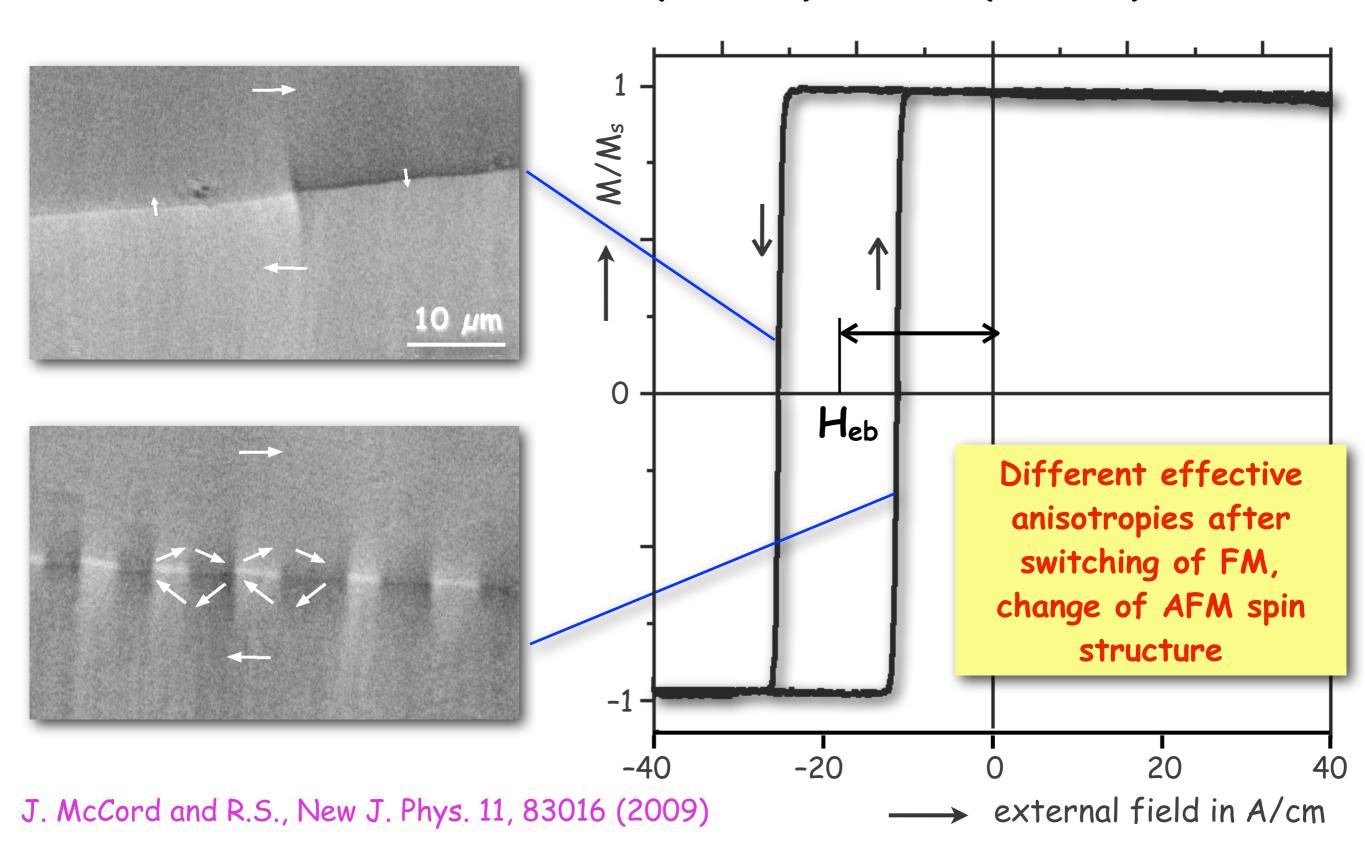
M(H) loop and domains

Reversal of Ni₈₁Fe₁₉ (30 nm) / NiO (30 nm)



M(H) loop and domains

Reversal of Ni₈₁Fe₁₉ (30 nm) / NiO (30 nm)



What needs to be measured?

Magnetization curve

Domain scale masurements (Magnetic Imaging)

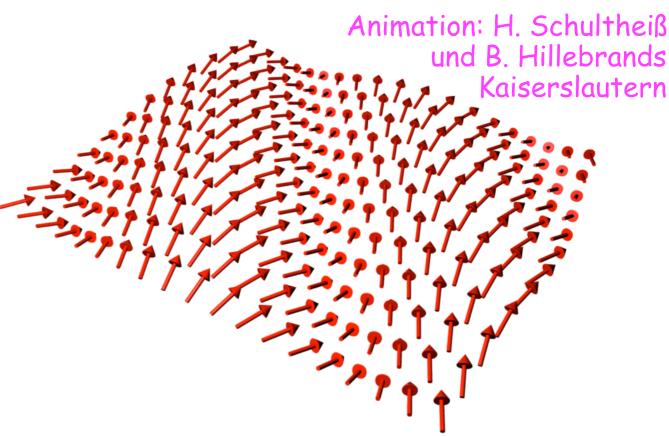
Saturation magnetization M_s

Crystal or other anisotropy constants K

Exchange or stiffness constant A

Magnetoresistance

Damping constants α Resonance frequency f_{res}



Magnetic order (neutrons)

Magnetostriction constants λ

and more...

Contents of lecture

- 1. Production of magnetic field
- 2. Measurement of magnetic field strength
- 3. Magnetic measurements to determine material parameters & properties
 - 3.1. Magnetic measurements
 - 3.2. Mechanical measurements
 - 3.3. Resonance techniques
 - 3.4. Dilatometric measurements
 - 3.5. Domain methods
- 4. Domain scale measurements (Magnetic Imaging)

UNITS FOR MAGNETIC PROPERTIES

Quantity	Symbol	Gaussian & cgs emu ^a	Conversion factor, C ^b	SI & rationalized mks ^c
Magnetic flux density, magnetic induction	В	gauss (G) d	10-4	tesla (T), Wb/m ²
Magnetic flux	Φ	maxwell (Mx), G·cm ²	10^{-8}	weber (Wb), volt second (V·s)
Magnetic potential difference, magnetomotive force	U, F	gilbert (Gb)	$10/4\pi$	ampere (A)
Magnetic field strength, magnetizing force	Н	oersted (Oe), ^e Gb/cm	$10^{3}/4\pi$	A/m ^f
(Volume) magnetization ^g	M	emu/cm ^{3 h}	10 ³	A/m
(Volume) magnetization	$4\pi M$	G	$10^3/4\pi$	A/m
Magnetic polarization, intensity of magnetization	J, I	emu/cm ³	$4\pi \times 10^{-4}$	T, Wb/m ² i
(Mass) magnetization	σ , M	emu/g	$^{1}_{4\pi\times10^{-7}}$	A·m²/kg Wb·m/kg
Magnetic moment	m	emu, erg/G	10^{-3}	A·m², joule per tesla (J/T)
Magnetic dipole moment	j	emu, erg/G	$4\pi \times 10^{-10}$	Wb·m ⁱ
(Volume) susceptibility	χ, κ	dimensionless, emu/cm ³	$4\pi (4\pi)^2 \times 10^{-7}$	dimensionless henry per meter (H/m), Wb/(A-
(Mass) susceptibility	$\chi_{ ho}$, $\kappa_{ ho}$	cm³/g, emu/g	$4\pi \times 10^{-3} \\ (4\pi)^2 \times 10^{-10}$	m^3/kg $H \cdot m^2/kg$
(Molar) susceptibility	$\chi_{ m mol}$, $\kappa_{ m mol}$	cm³/mol, emu/mol	$4\pi \times 10^{-6} \\ (4\pi)^2 \times 10^{-13}$	m³/mol H·m²/mol
Permeability	μ	dimensionless	$4\pi \times 10^{-7}$	H/m, Wb/(A·m)
Relative permeability ^j	$\mu_{\scriptscriptstyle \mathrm{f}}$	not defined		dimensionless
(Volume) energy density, energy product ^k	W	erg/cm ³	10-1	J/m³
Demagnetization factor	D, N	dimensionless	$1/4\pi$	dimensionless

a. Gaussian units and cgs emu are the same for magnetic properties. The defining relation is $B = H + 4\pi M$.

R. B. Goldfarb and F. R. Fickett, U.S. Department of Commerce, National Bureau of Standards, Boulder, Colorado 80303, March 1985 NBS Special Publication 696 For sale by the Superintendent of Documents, U.S. Government Printing Office, Washington, DC 20402

Magnetic Units

In this presentation: SI units

$$B = \mu_0(H + M) = \mu_0 H + J$$

B, J: [T] =
$$[\frac{V \sec}{m^2}]$$

$$H, M: \left[\frac{A}{m}\right]$$

from IEEE Magn. Soc. webpage

http://www.ieeemagnetics.org/images/ stories/magnetic_units.pdf

b. Multiply a number in Gaussian units by C to convert it to SI (e.g., $1 \text{ G} \times 10^{-4} \text{ T/G} = 10^{-4} \text{ T}$).

c. SI (Système International d'Unités) has been adopted by the National Bureau of Standards. Where two conversion factors are given, the upper one is recognized under, or consistent with, SI and is based on the definition $B = \mu_0 (H + M)$, where $\mu_0 = 4\pi \times 10^{-7}$ H/m. The lower one is not recognized under SI and is based on the definition $B = \mu_0 H + J$, where the symbol I is often used in place of J.

d. 1 gauss = 10^5 gamma (γ).

Both oersted and gauss are expressed as $cm^{-1/2} \cdot g^{1/2} \cdot s^{-1}$ in terms of base units.

f. A/m was often expressed as "ampere-turn per meter" when used for magnetic field strength.

g. Magnetic moment per unit volume.

h. The designation "emu" is not a unit.

i. Recognized under SI, even though based on the definition $B = \mu_0 H + J$. See footnote c.

j. $\mu_r = \mu/\mu_0 = 1 + \chi$, all in SI. μ_r is equal to Gaussian μ .

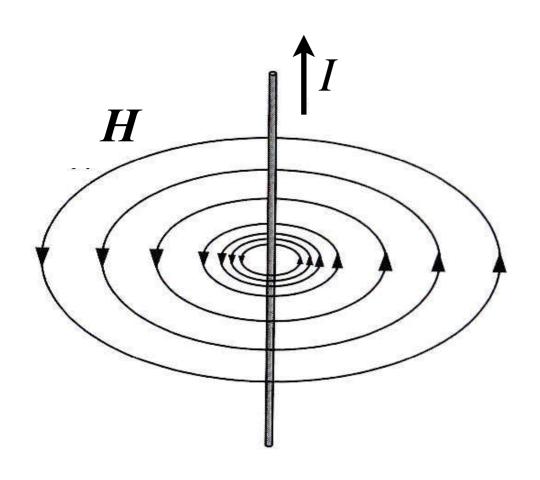
k. $B \cdot H$ and $\mu_0 M \cdot H$ have SI units J/m³; $M \cdot H$ and $B \cdot H/4\pi$ have Gaussian units erg/cm³.

For reading

- B.D. Cullity and C.D. Graham: Introduction to Magnetic Materials.
- IEEE Press and Wiley (2009)
- 5. Tumanski: Handbook of Magnetic Measurements.
- CRC Press Taylor & Francis (2009)
- F. Fiorillo: Measurement and Characterization of Magnetic Materials. Elsevier Academic Press (2004)
- R. Hilzinger and W. Rodewald: Magnetic Materials.
- Edited by Vacuumschmelze GmbH, Publicis Publishing, Erlangen (2013)
- D.C. Jiles: Introduction to Magnetism and Magnetic Materials.
- Chapman & Hall, London (1995)
- G. Bertotti: Hysteresis in Magnetism.
- Academic Press, New York (1998)

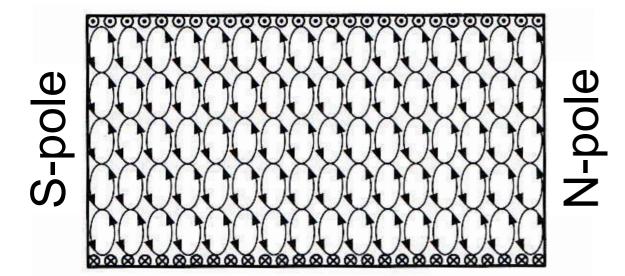
- Many figures in this presentation are taken from these references special thanks to the authors
- M. Coey: Magnetism and Magnetic Materials.
- Cambridge University Press (2010)
- A. Hubert and R.S.: Magnetic Domains. Springer Verlag (1998)

Two possibilities to generate magnetic field:



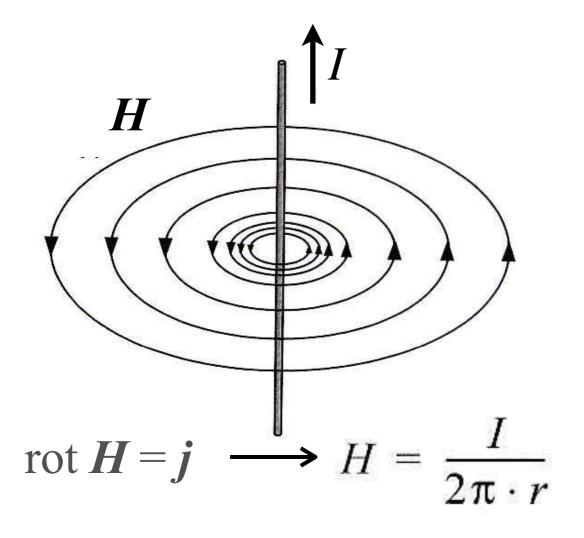
By electrical currents flowing in conductor

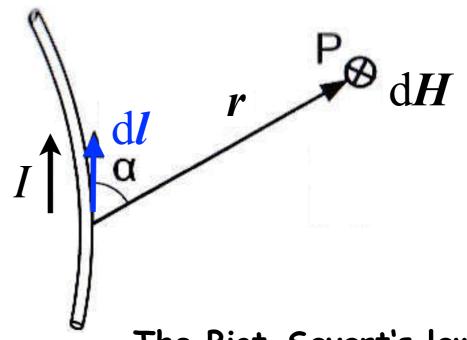
→ electromagnetic coils



By exploiting the ordered array of quantummechanical electronic currents circulating in a magnetic material (-> permanent magnets)

1.1 Electromagnetic coils

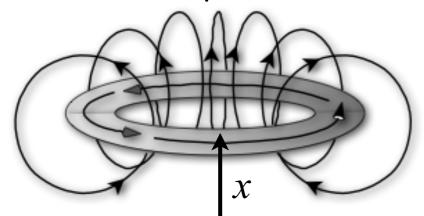




The Biot-Savart's law

$$dH = \frac{1}{4\pi \cdot r^3} \cdot I \cdot dl \times r \quad \text{or}$$

Current loop of radius r

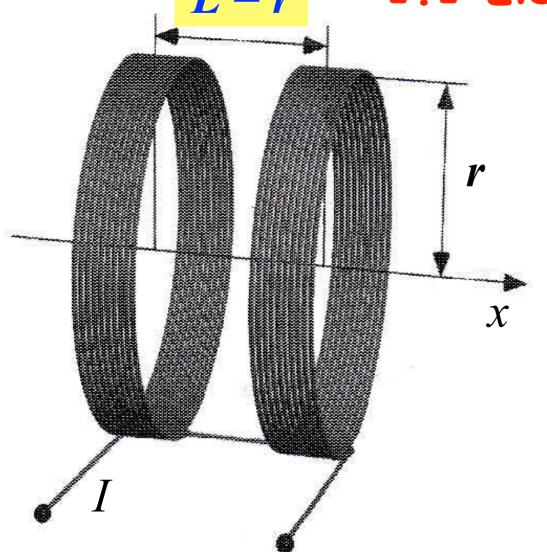


$$\int dH = \frac{1}{4\pi \cdot r^2} \cdot I \cdot dl \cdot \sin \alpha$$

$$H_x(x) = \frac{N \cdot I \cdot r^2}{2(r^2 + x^2)^{3/2}} \quad \text{Field of coil with } N \text{ windings}$$

$$H_{\rm x}(x) = \frac{N \cdot I \cdot r^2}{2(r^2 + x^2)^{3/2}}$$

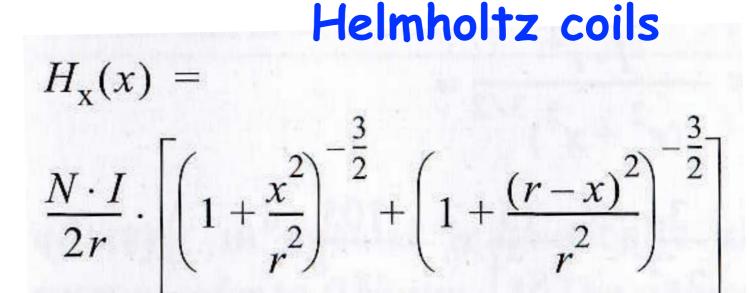
1.1 Electromagnetic coils (cont.)

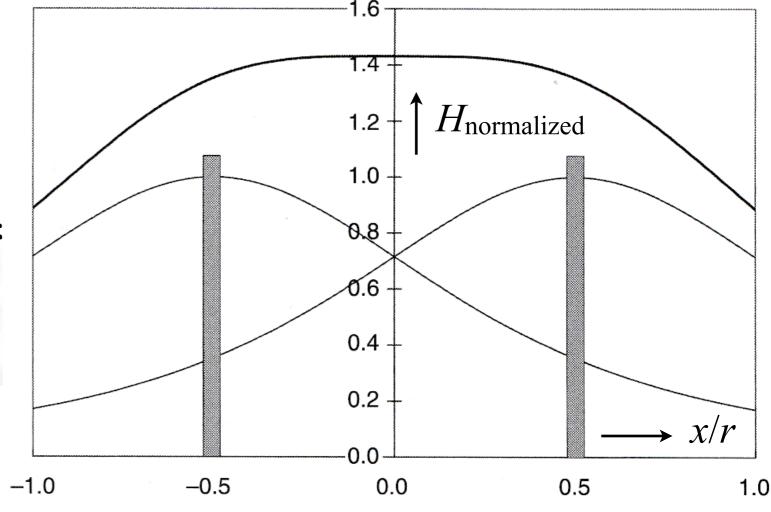


Axial field component at centre point:

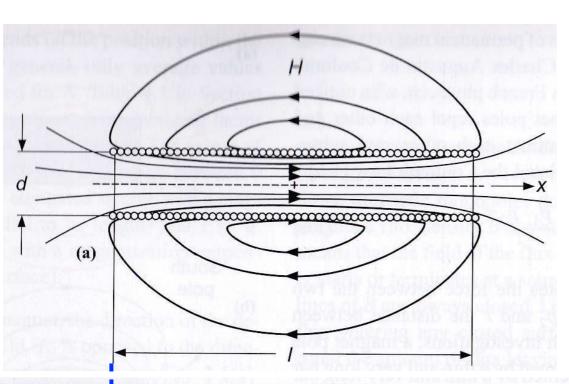
$$H_{x}(x = r/2) = 0.7155 \cdot \frac{N \cdot I}{r}$$

Homogeneous (small) field in large volume





1.1 Electromagnetic coils (cont.)



Solenoid



Solenoid with one layer of winding:

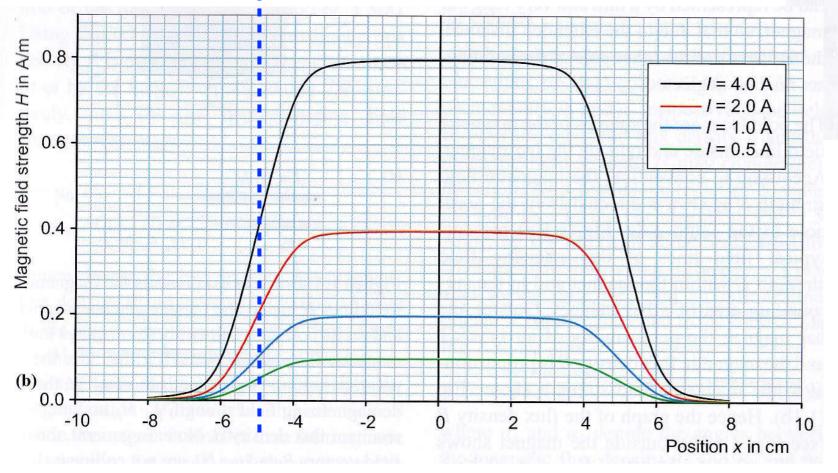
$$H(x) = \frac{N \cdot I}{l} \cdot \left\{ \frac{(l+2x)}{2\sqrt{[d^2 + (l+2x)^2]}} + \frac{(l-2x)}{2\sqrt{[d^2 + (l-2x)^2]}} \right\}$$

Field at centre:

$$H(x=0) = \frac{N \cdot I}{l} \cdot \frac{l}{\sqrt{[d^2 + l^2]}}$$

Long solenoid $(l \gg d)$:

$$H(x=0) = \frac{N \cdot I}{I}$$



1.1 Electromagnetic coils (cont.)

Remarks:

• Higher field: better increase n/l by adding more layers of winding rather than increasing current

 $H \sim I$, but $heat \sim I^2R$

Thus doubling number of winding layers and keeping current constant will double H, R, and amount of heat; whereas doubling of current will double H, but will quadruple heat

Typical field: 0.1 T*,
 higher field requires cooling

Solenoid



Solenoid with one layer of winding:

$$H(x) = \frac{N \cdot I}{l} \cdot \left\{ \frac{(l+2x)}{2\sqrt{[d^2 + (l+2x)^2]}} + \frac{(l-2x)}{2\sqrt{[d^2 + (l-2x)^2]}} \right\}$$

Field at centre:

$$H(x=0) = \frac{N \cdot I}{l} \cdot \frac{l}{\sqrt{[d^2 + l^2]}}$$

Long solenoid $(l \gg d)$:

$$H(x=0) = \frac{N \cdot I}{l}$$

^{*} Although SI unit of field is A/m, it is common to express field stregth in units of $\mu_0 H = B$ [Tesla]

1.1 Electromagnetic coils (cont.)

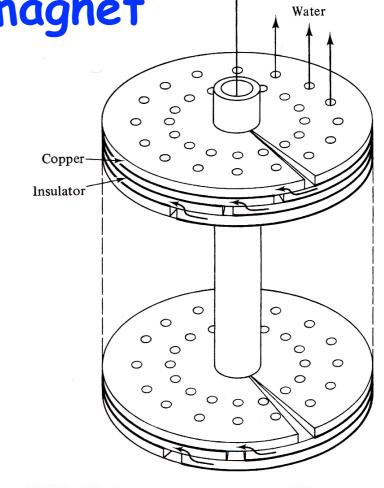
High-Field Solenoid: Bitter magnet

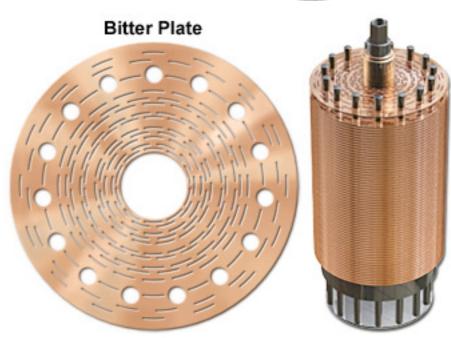
High field: requires large power input

- → two major design problems:
- 1) Large amount of heat (note: maintaining magnetic field by current is process of zero efficiency: all input power goes into heat)
- 2) Mechanical strength to resist large forces acting on current carriers has to be provided

Bitter magnet:

- Winding composed of Cu disks, ~30 cm diameter
- Insulated from each other, clamped together
- Rotated by 20°: overlap = conduction path
- Cooling water pumped through holes,
- Helical current path, acts like solenoid
- Typical field: 45 Tesla in 30 mm bore, requires current of 67.000 A, power input of 20 MW
- Requires large motor-generator sets

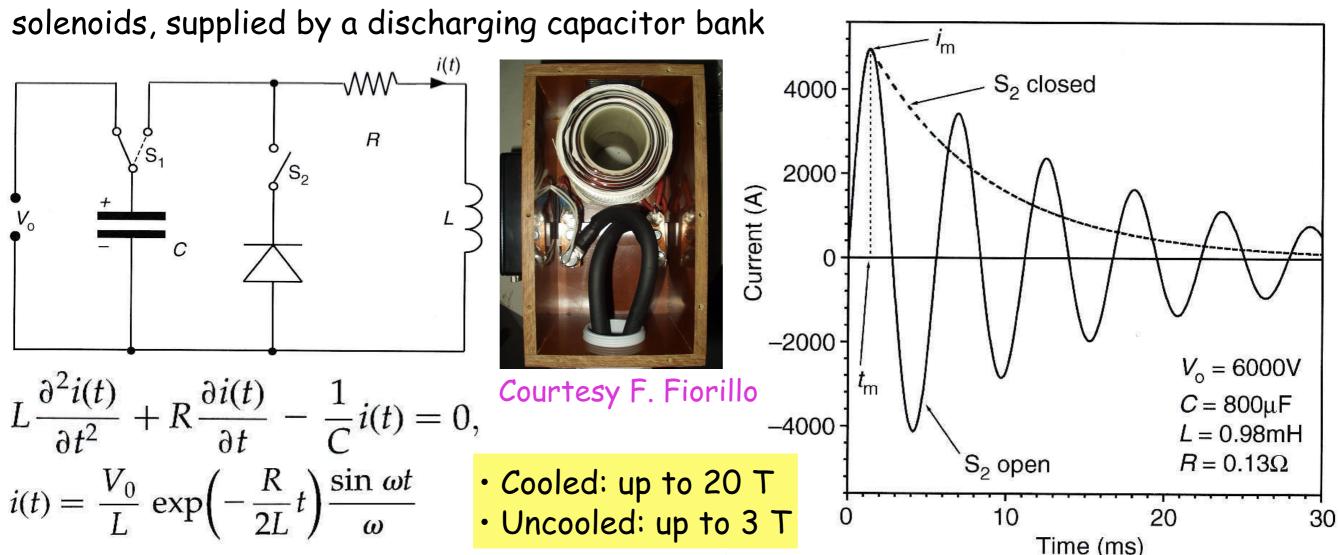




1.1 Electromagnetic coils (cont.)

High-field Solenoid: Pulsed Fields

Pulsed fields up to about 10 T (peak) can be obtained by conventional



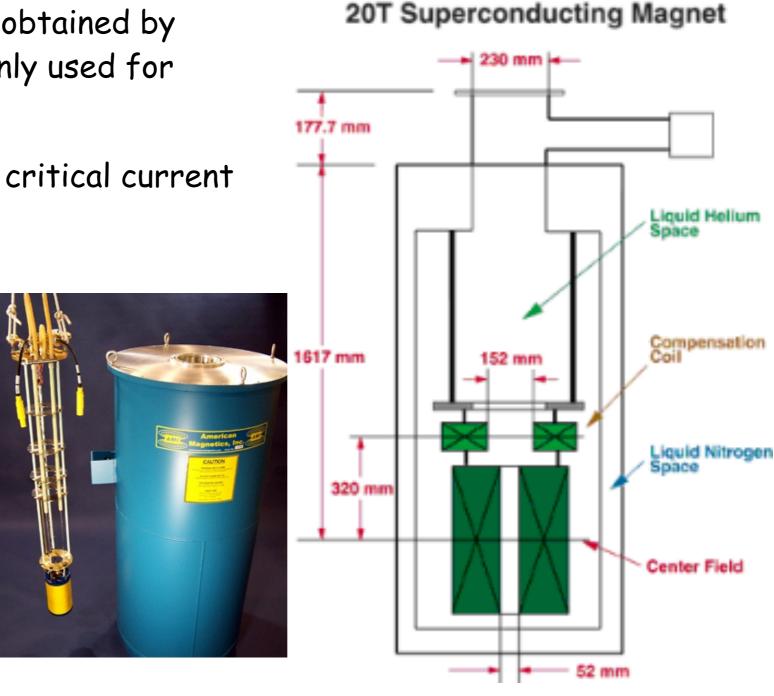
In shown arrangement with given inductance L of solenoid, an oscillating damped discharge is obtained (switch S_2 open). If S_2 is closed at maximum field, the diode prevents capacitor from discharging with reversed polarity and current decays from maximum value with time constant $\tau_1 = L/R$

1.1 Electromagnetic coils (cont.) Superconducting Solenoids

 DC fields up to about 20 T can be obtained by superconducting solenoids, commonly used for fields above 2 T

 Type II superconductor with high critical current and critical field: Nb-Ti or Nb₃Sn

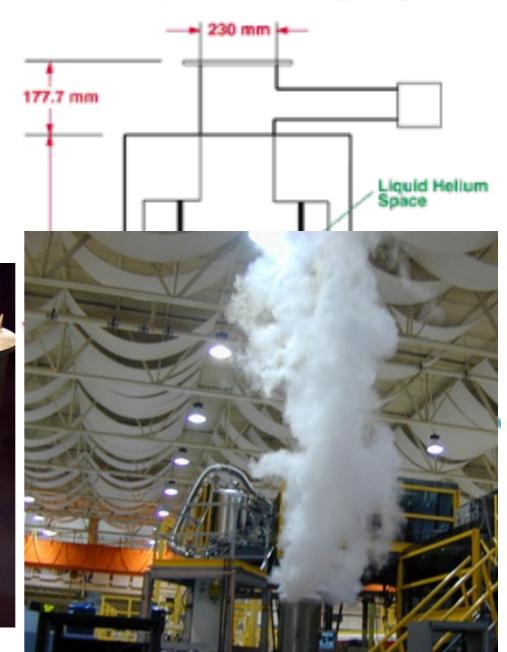
- Cooling of coil by liquid helium (4.2 K), sample temperature up to room temperature
- Shortcut of superconducting coil: persistant mode, no power consumption over months
- Danger: quench by local heating



1.1 Electromagnetic coils (cont.) Superconducting Solenoids

- DC fields up to about 20 T can be obtained by superconducting solenoids, commonly used for fields above 2 T
- Type II superconductor with high critical current and critical field: Nb-Ti or Nb₃Sn
- Cooling of coil by liquid helium (4.2 K), sample temperature up to room temperature
- Shortcut of superconducting coil: persistant mode, no power consumption over months
- Danger: quench by local heating



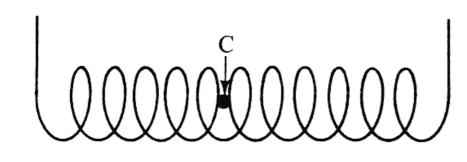


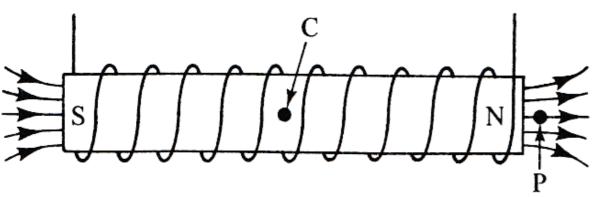
20T Superconducting Magnet

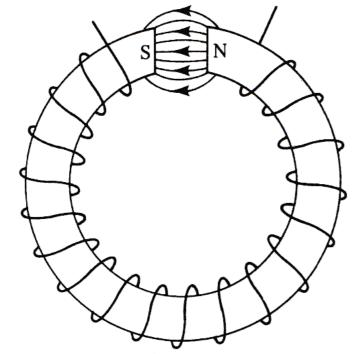
1.2 Electromagnets

DC fields up to 2 T, most commonly used magnetic field source in labs

Evolution of the electromagnet:







Solenoid, flux density at center C:

$$B = \mu_0 H = \mu_0 \; \frac{N \cdot I}{l}$$

Solenoid with iron rod, flux density at center C:

$$B = \mu_0(H + M) = \mu H$$

Iron has multiplied field due to the current by factor of μ , same field occurs just outside rod at P

In large field obtained with low current (e.g. $H_{\rm coil}$ = 1 mT, μ = 2000: $H_{\rm outside}$ = 2 T) Problem: flux lines outside iron diverge and field decreases rapidly

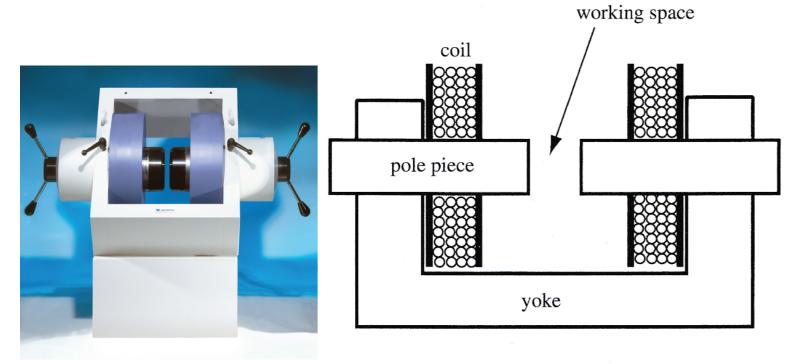
Bended iron rod with gap:

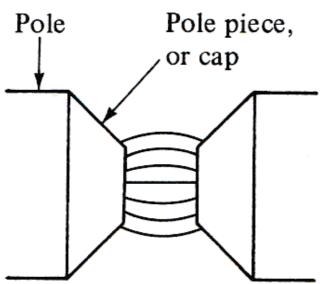
Flux travels directly from pole to pole across gap. Contribution of iron to gap field (if saturated) = 2.15 T

1.2 Electromagnets (cont.)

DC fields up to 2 T, most commonly used magnetic field source in labs

Evolution of the electromagnet:





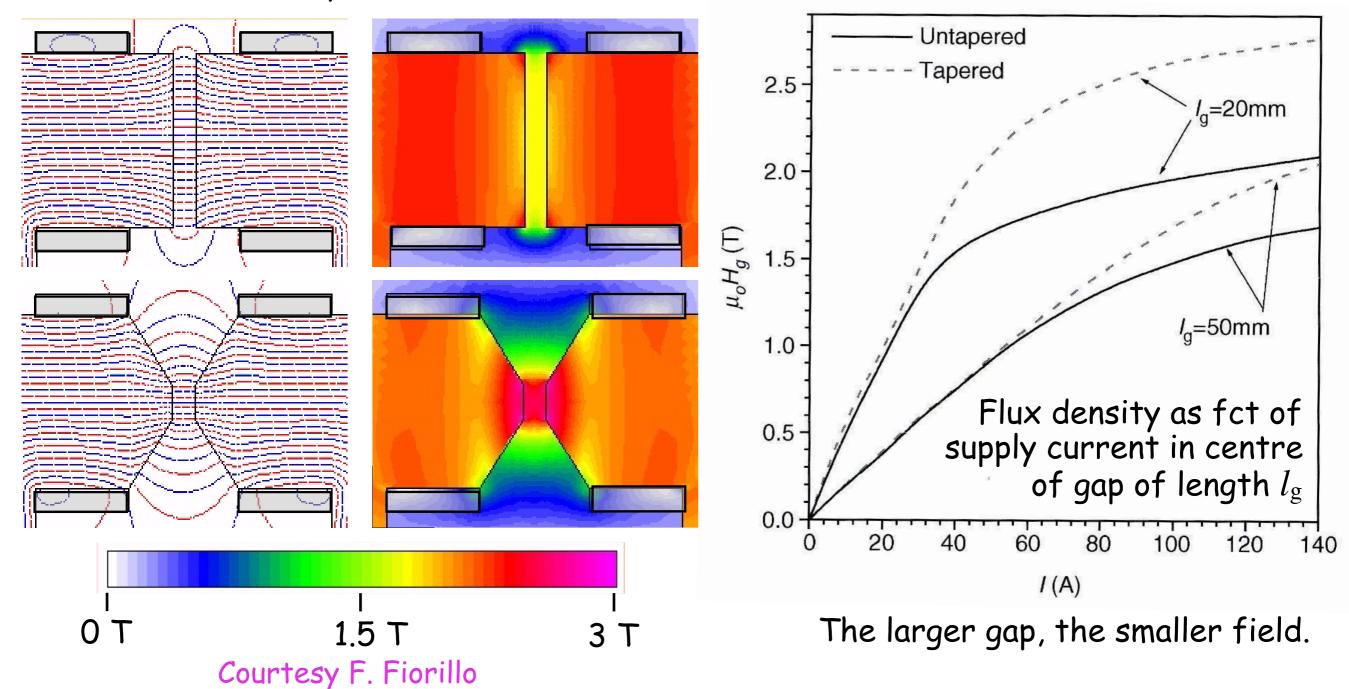
Electromagnet:

- Windings close to gap
- Core and yoke made of iron, annealed for high permeability
- Windings water-cooled
- Pole diameter: up to 30 cm
- Flat poles for uniform field
- Tapered poles: free poles formed on tappered surfaces contribute to field at gap center, can achieve fields higher than $\mu_0 M_{\rm s}$ (> 3T for gap length of 5-10 mm). Optimum taper angle: 54,74°
- Pole pieces made of CoFe $(M_{\rm S}$ about 10% higher than for pure Fe)

1.2 Electromagnets (cont.)

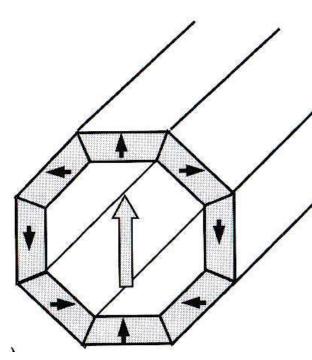
DC fields up to 2 T, most commonly used magnetic field source in labs

Finite element simulations: lines and contour maps of induction \boldsymbol{B}

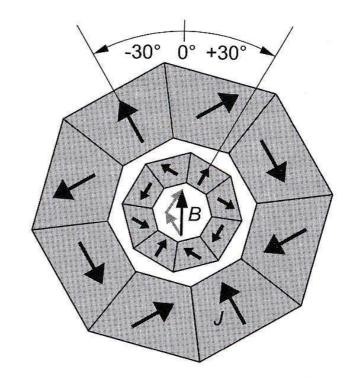


1.3 Permanent Magnets

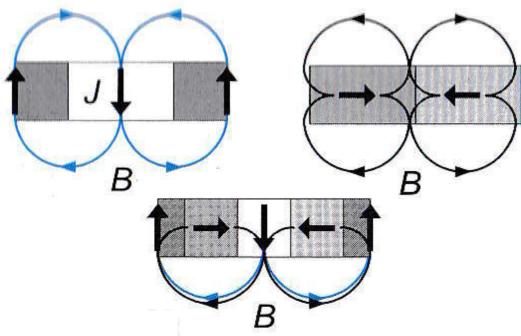
Fields up to ~2T by appropriate arrangement of permanent magnets



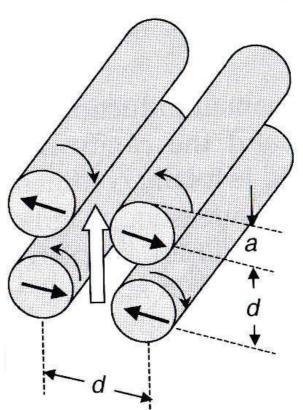
Technical design of Halbach cylinder: array of uniformly magnetized NdFeB magnets, uniform field accross diameter



Two concentric
Halbach arrays:
vectorial addition of
flux density in centre.
By synchronous but
opposite rotation, the
field strength can be
continuously varied



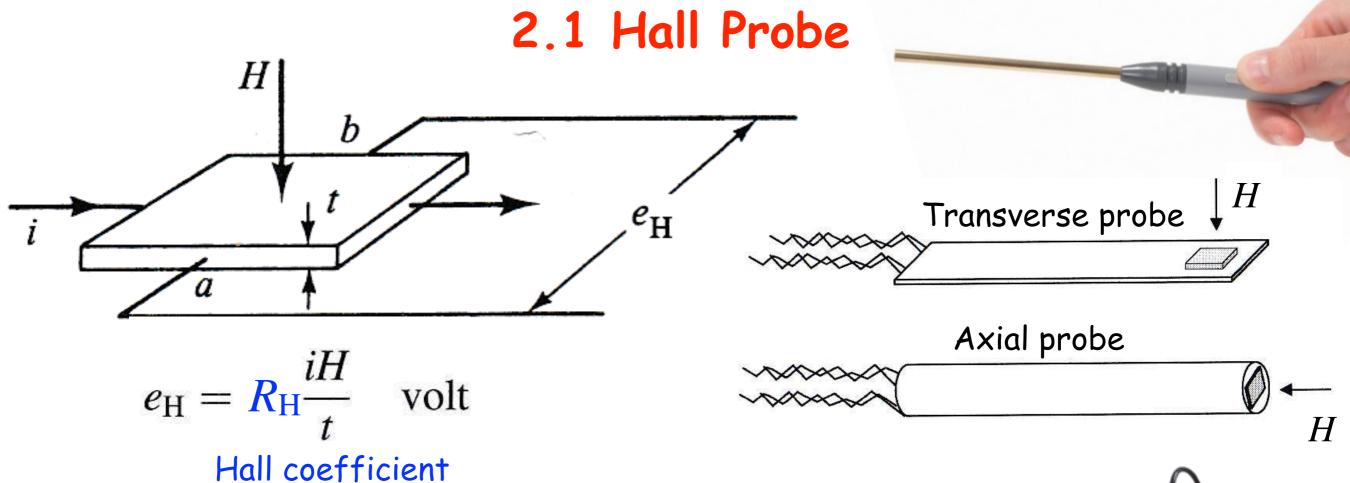
One-sided field by superposition



Simplification of above aray: continuously varying field by counter rotation of 4 transversly magnetized rods

2.

Measurement of Magnetic Field Strength



- Hall probe = plate made of InSb or GaAs semiconductor
- H-field perpendicular to plate distorts current path and emf $e_{\rm H}$ is developed between a and b
- Multirange instruments, sensitive to field range from μT to 3T
- Uncertainty in field reading: 1-5% in hand-held Gaussmeters
- · Alternating fields up to some 10 kHz can be measured
- · Calibration by accuratly known fields required
- Low-field probes: zero must be set with probe in magnetically shielded cylinder to eliminate Earth's field



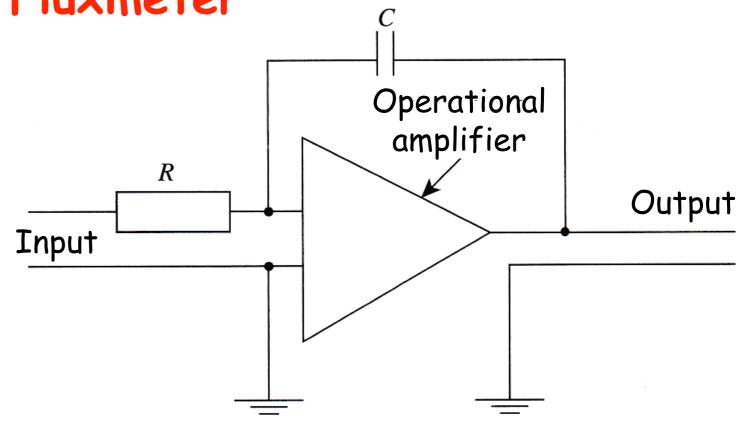
2.2 Fluxmeter

• Faraday's law: a changing magnetic flux φ through a coil of N turns generates a voltage in coil proportional to rate of change of flux:

$$U(t) = -N\frac{d\varphi}{dt} \quad \text{[Volt]}$$

$$U(t) dt = -N d\varphi$$

$$\int_{0}^{t} U(t) dt = -N \int_{\Phi_{1}}^{\Phi_{2}} d\varphi = -N \Delta \varphi \qquad U_{\text{out}} = -1/RC \int U_{\text{in}} dt$$



- Instrument to integrate voltage from pick-up coil is called fluxmeter
 electronic integrator (based on capacitive feedback around operational amplifier)
 that provides voltage output
- With $B = \varphi/A$ (flux density in pick-up coil of cross section A):

$$\int U(t) dt = -NA \Delta B \text{ [Vs]}$$

Fluxmeter measures changes in flux density

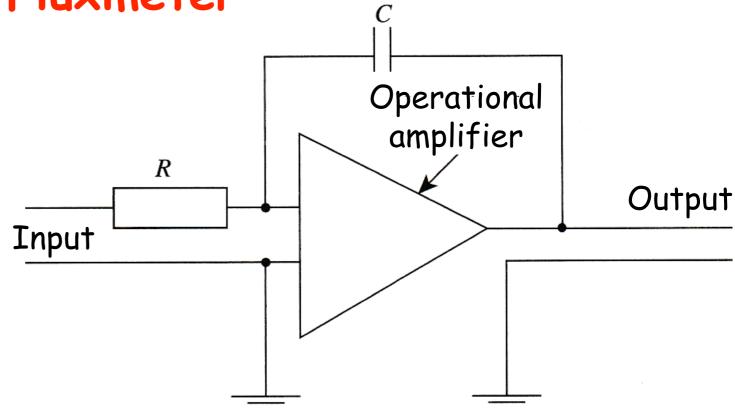
2.2 Fluxmeter

 Faraday's law: a changing magnetic flux φ through a coil of N turns generates a voltage in coil proportional to rate of change of flux:

$$U(t) = -N \frac{d\varphi}{dt} \quad \text{[Volt]}$$

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- Instrument to integrate voltage from pick-up coil is called fluxmeter = electronic integrator (based on capacitive feedback around operational amplifier) that provides voltage output
- With $B = \varphi/A$ (flux density in pick-up coil of cross section A):

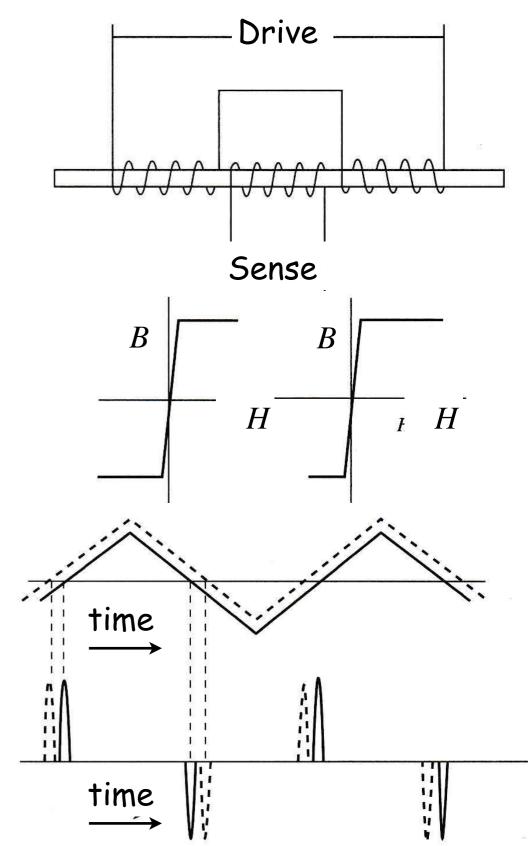
$$\int U(t) dt = -NA \Delta B \text{ [Vs]}$$

Fluxmeter measures changes in flux density

Measurement of constant field: search coil must be moved to zero-field region, or rotated through 180°

2.3 Fluxgate Magnetometer

- Instrument for accurate measurement of fields comparable to Earth's field (used in e.g. geomagnetic and archeological surveys)
- Principle: high-permeability soft magnetic strip or wire with drive and sense coil
- AC (triangular) current in drive coil drives strip to pos. and neg. saturation, sense coil picks up ${\rm d}B/{dt}$
- No external dc field: symmetric B(H)-loop, positive and negative voltage pulses equally spaced
- With dc field H along strip: asymmetric loop, pulses unevenly spaced
- For triangular drive field: change in pulse spacing is direct measure for dc field
- Typical field range: 0.1 mT



2.4 Magnetic Potentiometer (Rogowski-Chattok coil)

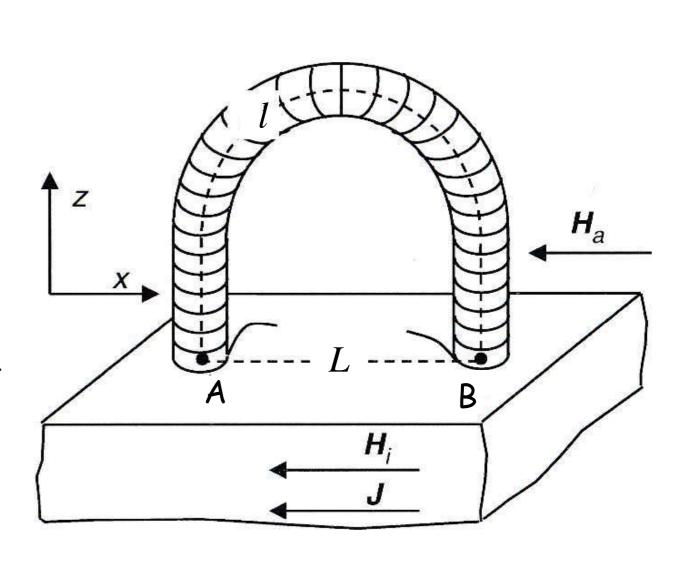
- · Tightly wound coil whose ends lie in same plane
- · Field at surface of magnetic sample is the same as internal field
- If no current flows in coil: line integral $\int Hdl$ around dotted path must be zero:

$$\int_{A}^{B} H dl + \int_{B}^{A} H dL = 0$$

• If field is uniform along L:

$$\int_{B}^{A} H dL = H \Delta L = -\int_{A}^{B} H dl$$

- If output of coil is connected to integrator: the integrated voltage is proportional to change of ${\cal H}$ along the line ${\cal L}$
- Is used to measure magnetic field in flux-closing yokes (like singe sheet testers for electrical steel)



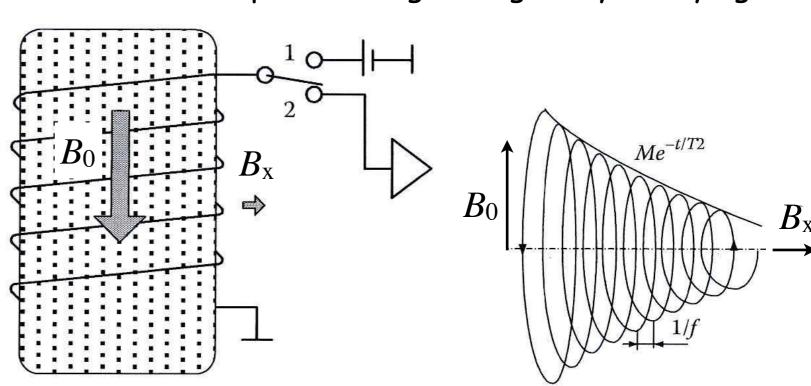
2.5 Proton Precession Magnetometer

- High-precision measurement of weak magnetic field (like Earth's field, with uncertainty 1 ppm), also used for calibration
- Relies on Nuclear Magnetic Resonance (NMR): applyig magnetic field \rightarrow magnetic moment of nucleus rotates in selected quantum directions with resonance frequency which strictly depends on value of field
- To measure weak magnetic field (like Earth's field):
 - (1) sample (e.g. 1 liter of water) is exposed to strong dc magnetic field B_0 (~10 mT) perpendicluar to the measured field $B_{\rm x}$. B_0 aligns certain fraction of proton moments along coil direction

• (2) B_0 switched-off \rightarrow magnetic moments of protons align along $B_{\rm x}$ by decaying

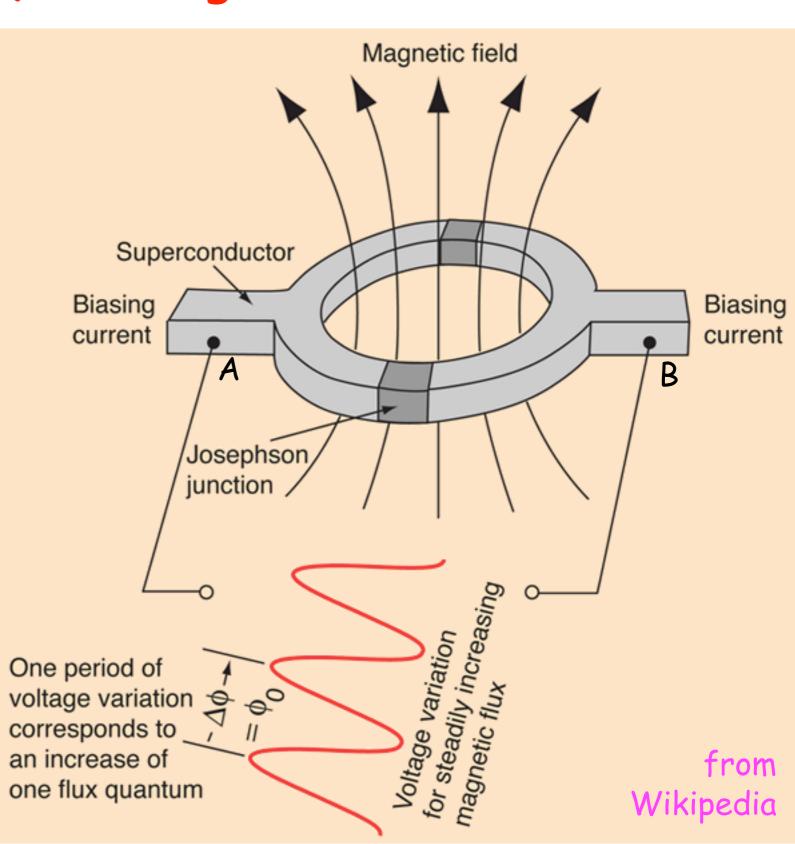
precession movement. Frequency of precession is measured by measuring frequency of induced voltage in coil. Frequency depends precisely on $B_{\rm x}$.

 Typical precessional frequency: a few kilohertz



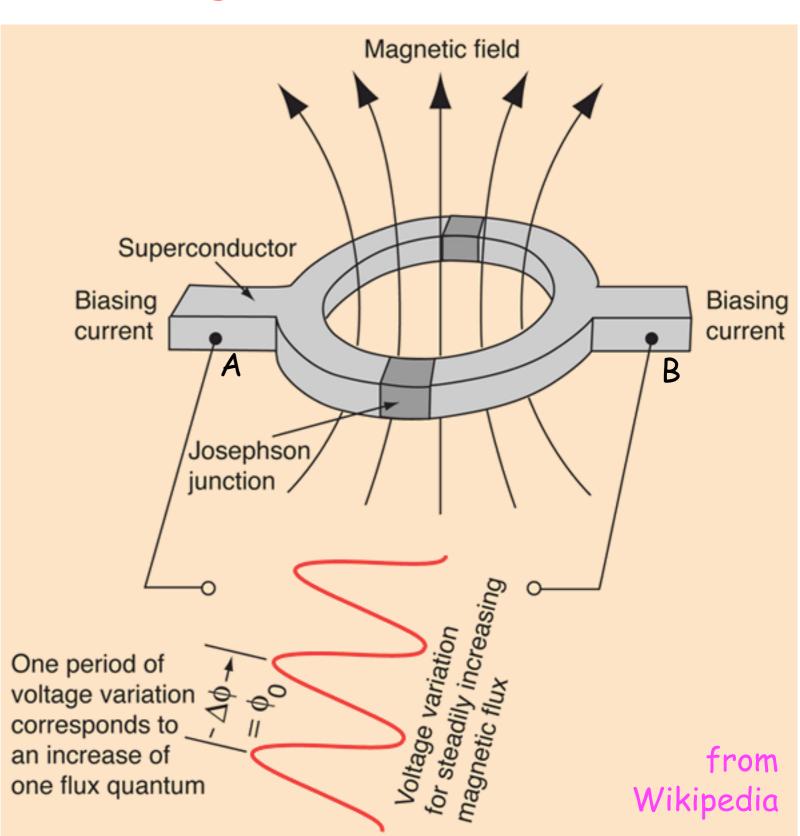
2.6 SQUID Magnetometer

- SQUID: Superconducting Quantum Interference Device magnetometer
- Based on tunneling of superconducting electrons across narrow insulating gap, called Josephson junction
- Ring-shaped device, superconducting current from A to B, equal currents pass through each junction
- Changing magnetic flux through ring: induces "screening" current in ring (Faraday's law) which generates magnetic field that cancels external flux. Induced current adds to measuring current in one junction, subtracts in other



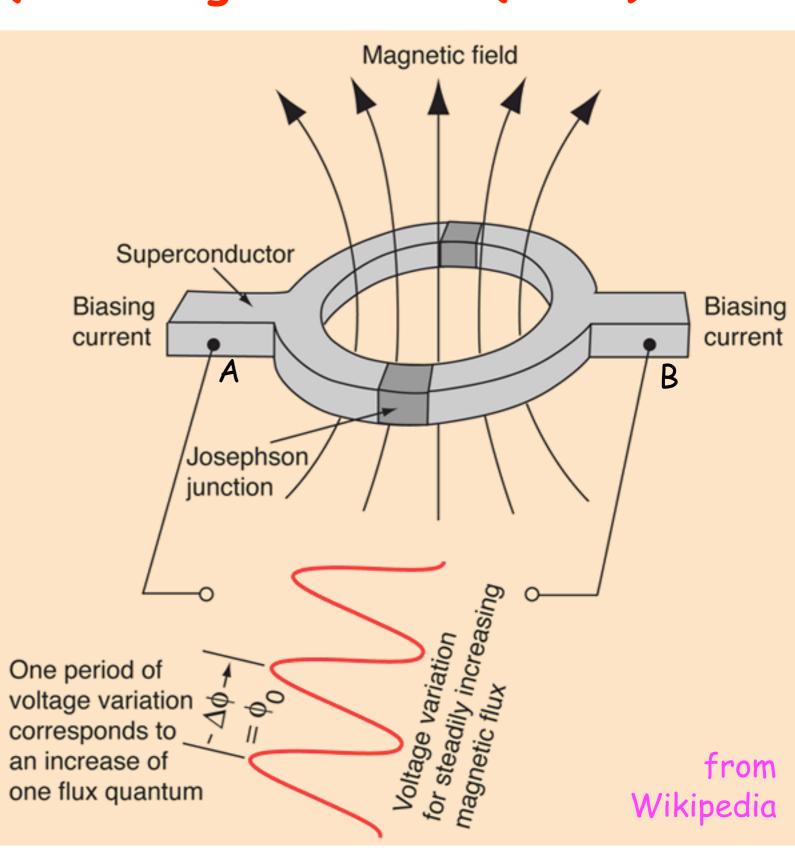
2.6 SQUID Magnetometer (cont.)

- As soon as current in either branch exceeds the critical current of the Josephson junction, a voltage appears across the junction
- In superconducting ring the magnetic flux is quantized, i.e because of wave nature of superconducting current (quantummechanics) the flux enclosed by the ring must be an integer number of the flux quantum $\Phi_0 = h/2e$



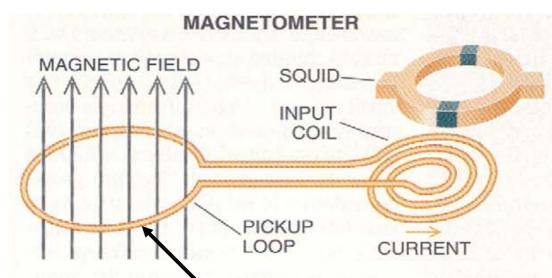
2.6 SQUID Magnetometer (cont.)

- Now suppose the external flux is further increased until it exceeds $\Phi_0/2$. Since the flux enclosed by the loop must be integer number of flux quanta, instead of screening the flux the SQUID now energetically prefers to increase it to Φ_0 . The screening current now flows in the opposite direction.
- \rightarrow screening current changes direction every time the flux increases by half integer multiples of \varPhi_0
 - → critical current oscillates as a function of the applied flux
 - ightarrow voltage between A and B is function of applied magnetic field and a period equal to $arPhi_0$

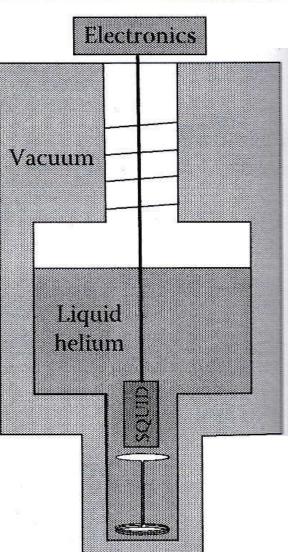


2.6 SQUID Magnetometer (cont.)

- In practise: SQUID is not directly contacted with magnetic source, device is rather linked to transformer coil to measure flux from small sample, i.e. sample magnetization
- SQUID magnetometer is high-sensitivity static fluxmeter
- Sensitivity: femto- to pico-Tesla
- Since SQUID requires low-T operation, it is usually used in conjunction with superconducting coil







3.

Magnetic Measurements to determine material parameters & properties

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

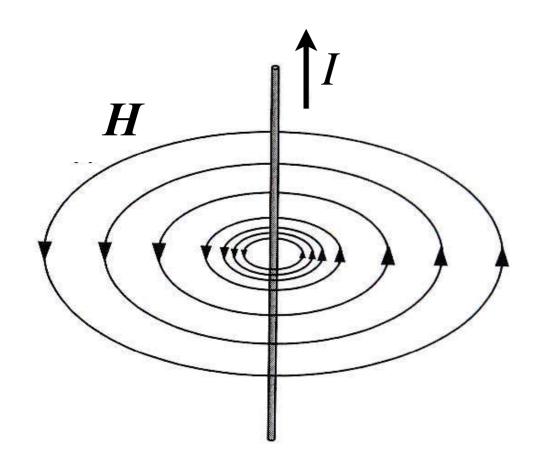
General aspects

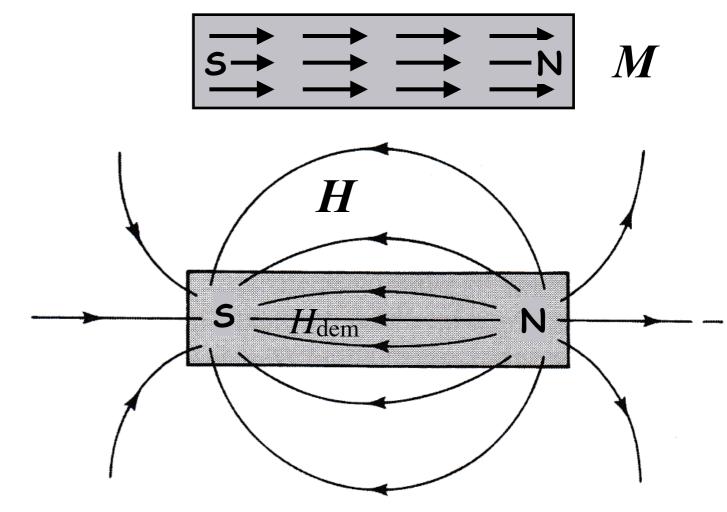
Magnetic field H

Field produced by currents:

Lines of \boldsymbol{H} are continuous and form closed loops

Field produced by magnetic poles: Lines of H begin at north poles and end at south poles (here: $H_{\rm applied} = 0$)





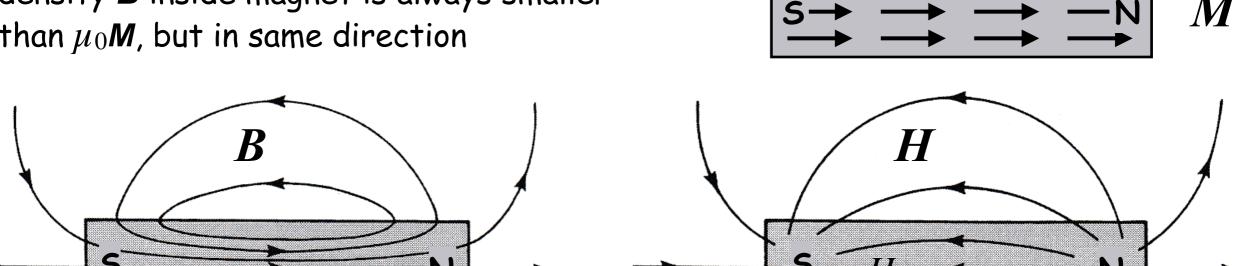
Demagnetizing field $H_{dem} = -N\overline{M}$: acts opposite to magnetization M that creates it

General aspects

Magnetic field H and Induction B

- $B = \mu_0 (H + M) = \mu_0 (H_{\text{applied}} H_{\text{dem}} + M)$
- If $H_{\rm applied}=0$: $H_{\rm dem}$ is only field acting, and ${\bf B}=-\mu_0{\bf H}_{\rm dem}+\mu_0{\bf M}$
- $\mu_0 H_{\text{dem}}$ can never exceed $\mu_0 M$, i.e. flux density B inside magnet is always smaller than $\mu_0 M$, but in same direction

Field produced by magnetic poles: Lines of H begin at north poles and end at south poles (here: $H_{\text{applied}} = 0$)



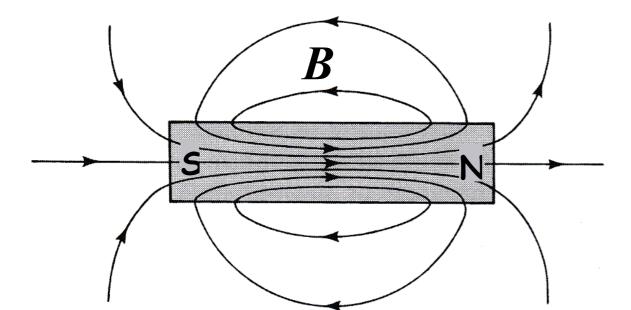
• Lines of **B** are continuous, from S to N inside magnet, outside $\mu_0 H = B$

Demagnetizing field $H_{\text{dem}} = -N\overline{M}$: acts opposite to magnetization M that creates it

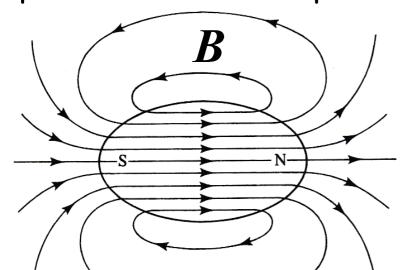
General aspects

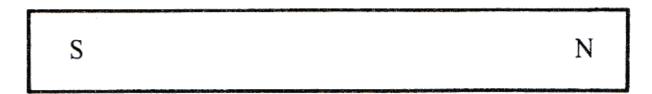
Magnetic field H and Induction B

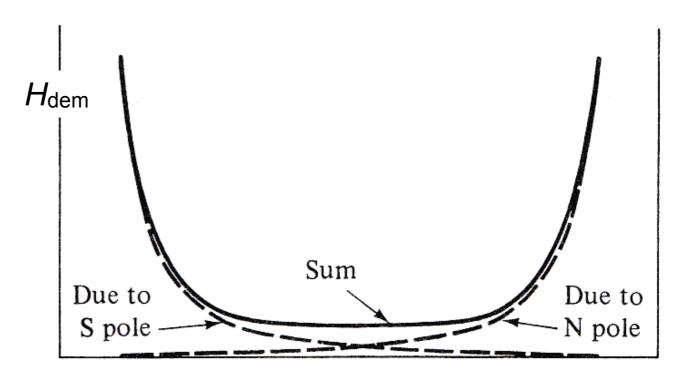
- Flux density of bar magnet is not uniform:
 B-lines diverge towards the ends → flux
 density is less than in center
- Reason: H_{dem} is stronger near the poles



• Exception: rotational ellipsoid:



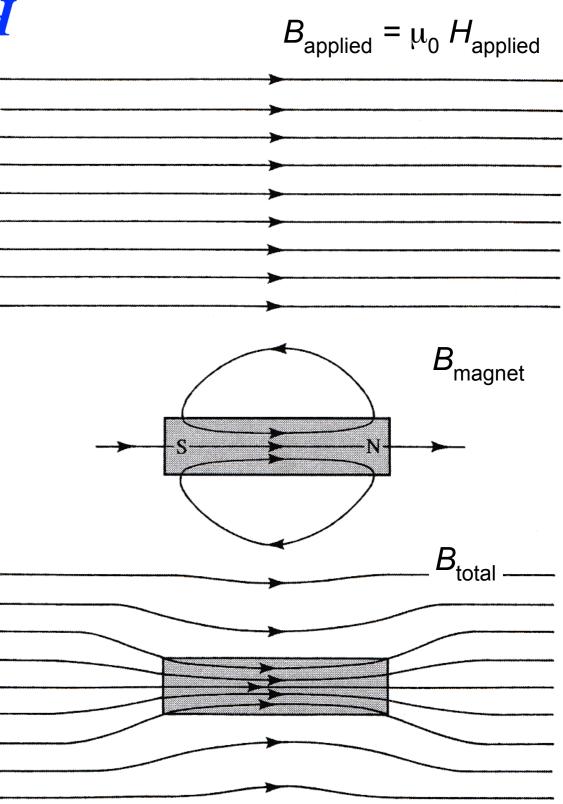




General aspects

Finite sample in applied field H

- When soft magnetic body is placed in field, it alters shape of field.
- This is demonstrated by asuming a fully magnetized bar magnet. The total field $B_{\rm total}$ is the vector sum of applied field $B_{\rm applied}$ and B-field of magnet
- The flux tends to crowd into the magnet, as though it were more permeable than surrounding air (→ term "permeability"). At points outside the magnet: field is reduced
- The same result is obtained if the body that is placed in the field is originally unmagnetized, because the field itself will produce magnetization (for material with $\mu >> 1$)
- For strongly magnetic materials the disturbance of field is considerable

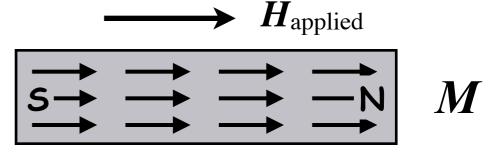


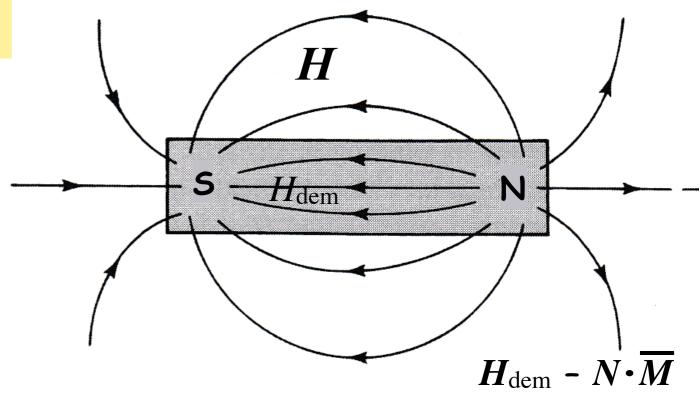
General aspects

Closed and open samples

Open sample

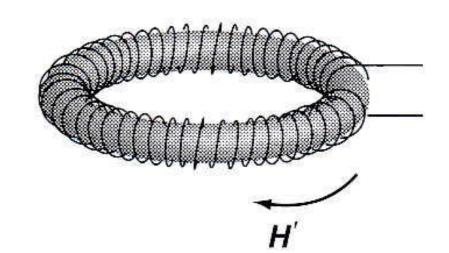
Internal field: $H_{\rm in} = H_{\rm applied} - N \cdot \overline{M}$





Closed sample

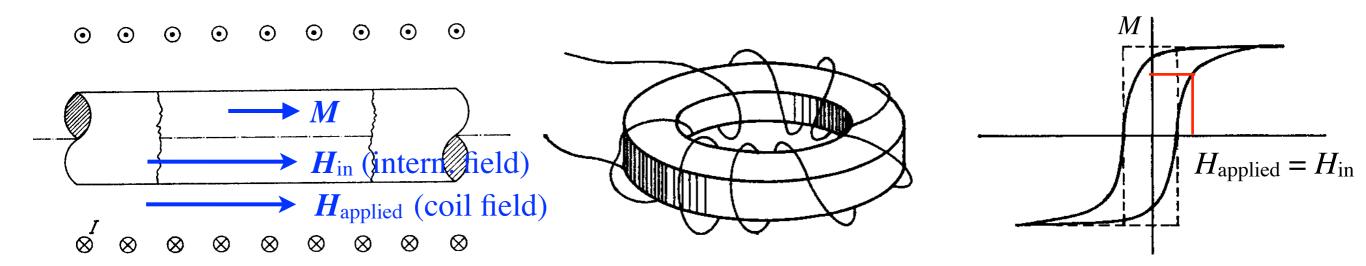
Internal field: $H_{in} = H_{applied}$, N = 0



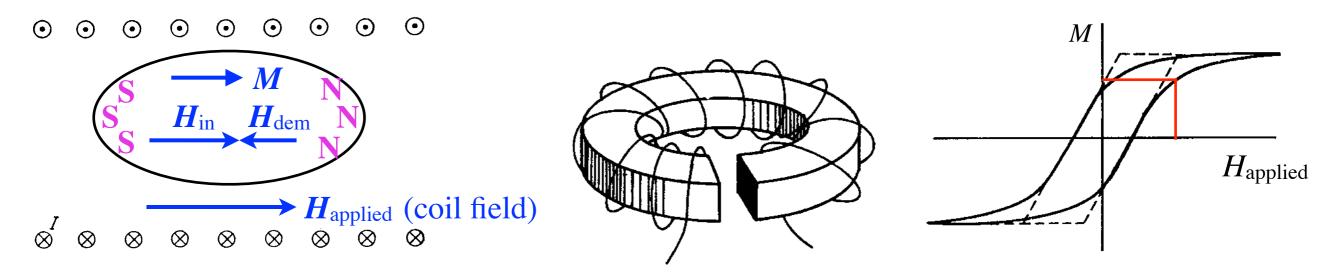
General aspects

Closed and open samples

Demagnetization effect→ Shearing of magnetization curve



Infinite sample or closed ring: unsheared hysteresis curve: N=0, i.e. $H_{\rm in}=H_{\rm ext}$



Finite sample or open core: sheared hysteresis curve due to demagnetization effect (a higher $H_{\rm applied}$ is needed to achieve a given degree of M)

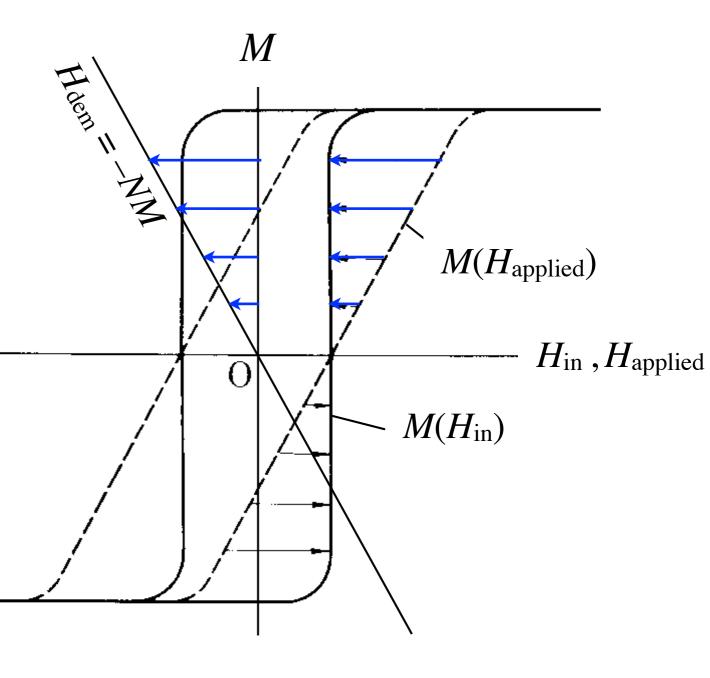
General aspects

Closed and open samples

Demagnetization effect

→ Shearing of magnetization curve

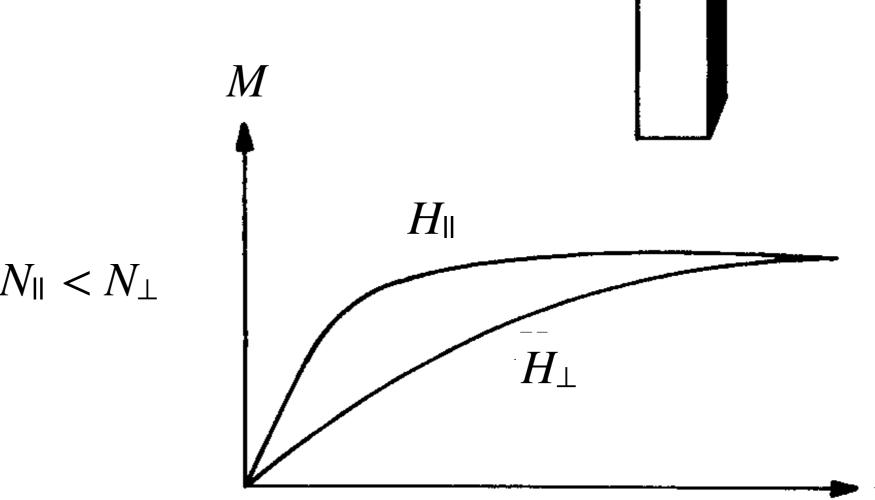
- Internal field: $H_{in} = H_{applied} N \cdot M$
- Relevant for magnetic materials is the $M(H_{\rm in})$ -curve, as it is independent of the sample shape
- If a magnetization curve was measured on a finite sample, it has to be re-sheared.



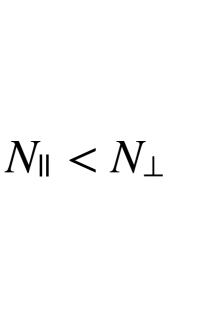
General aspects

Influence of demagnetizing factor

- Influence of sample shape on hysteresis curve: Shape anisotropy
- Larger demag. factor → stronger shearing of magnetizaton curve



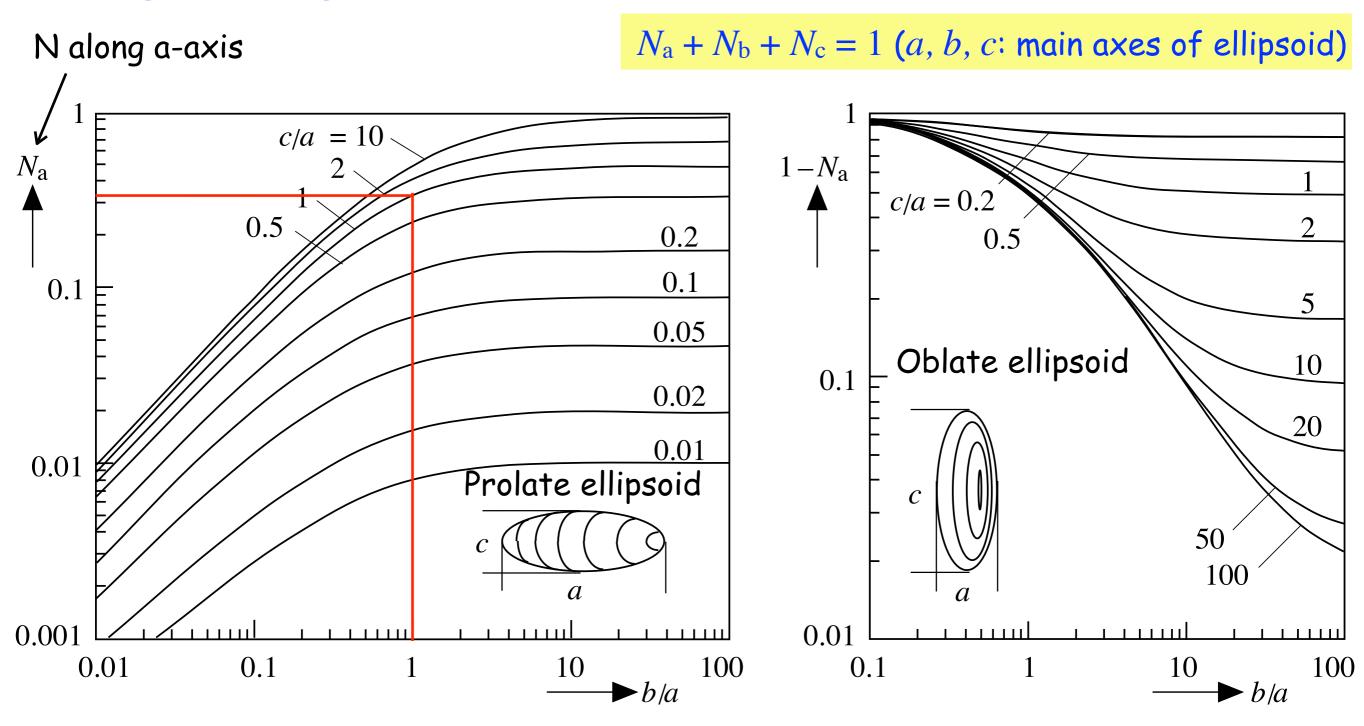
 H_{\parallel}



General aspects

Demagnetizing factor

Can only be calculated exactly for rotational ellipsoid



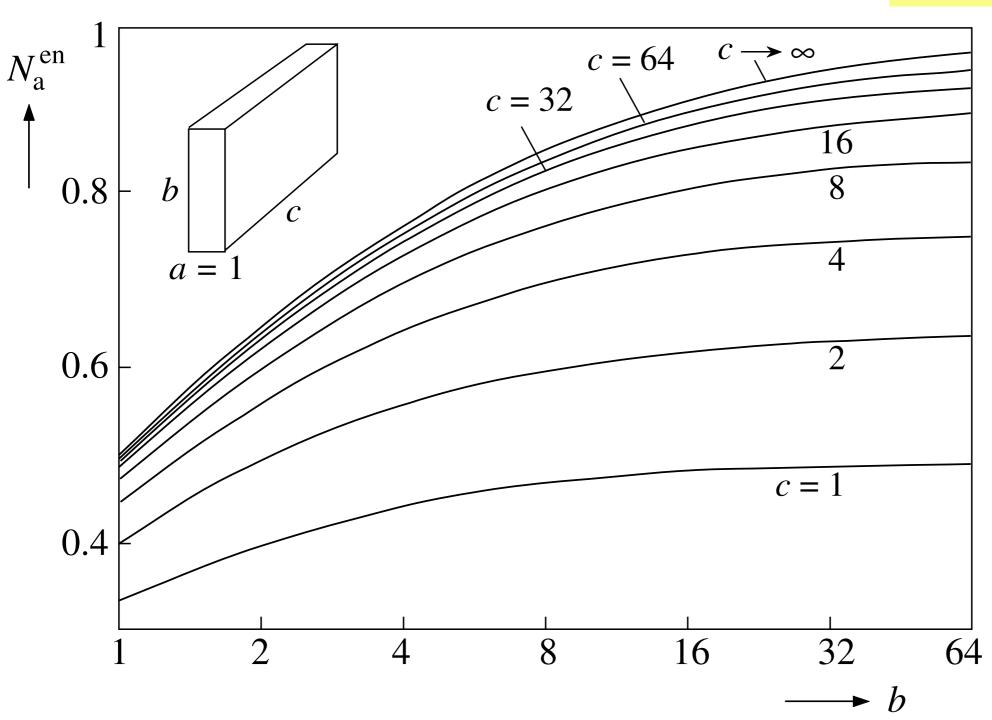
Sphere: $a = b = c \rightarrow N_a = 1/3 = N_b = N_c$

General aspects

Demagnetizing factor

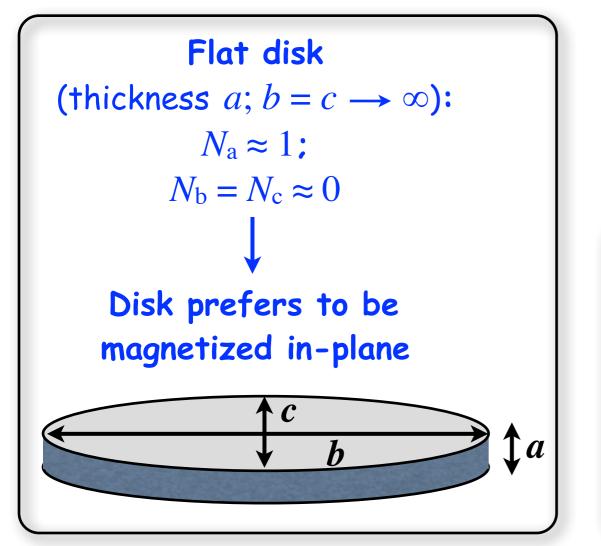
Numerical calculation for rectangular body

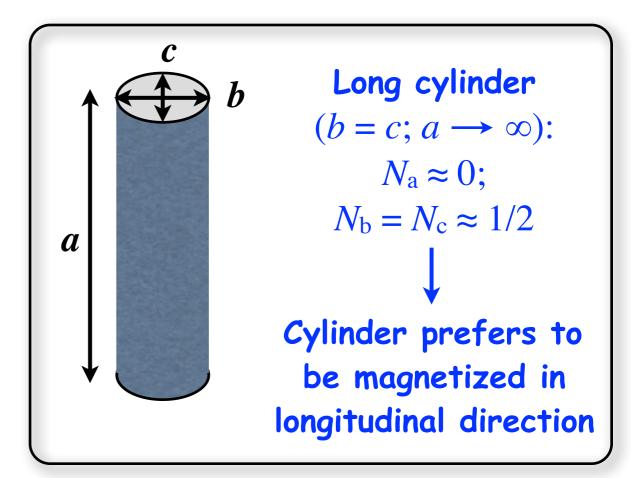
 $N_a + N_b + N_c = 1$ applies

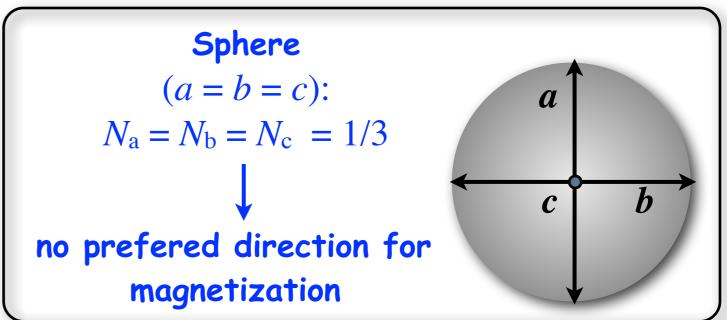


General aspects

Demagnetizing factor



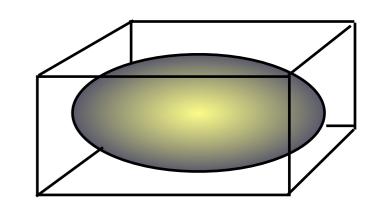


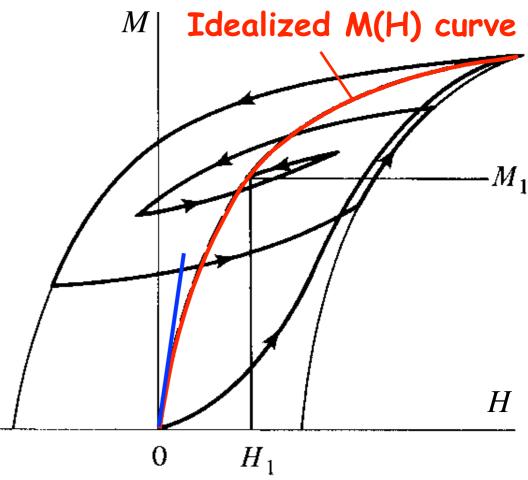


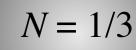
General aspects

Demagnetizing factor

- Demagnetizing factor of compact bodies is often well approximated by that of inscribed ellipsoid
- Experimental determination of the demagnetization factor:
 - For every dc-field an ac-field of decreasing amplitude is superimposed (helps to overcome barriers in magnetization process)
 - Then approximately that magnetization is achieved, the demagnetizing field of which is equal to the applied field
 - The initial slope of the magnetization curve is dM/dH = 1/N
- If possible: avoid demagnetization effect by chosing proper sample geometry for magnetic measurement







General aspects

Conclusion (demagnetization problematics):

The long-range nature of the demagnetizing field makes the measured property of any test specimen geometry-dependent

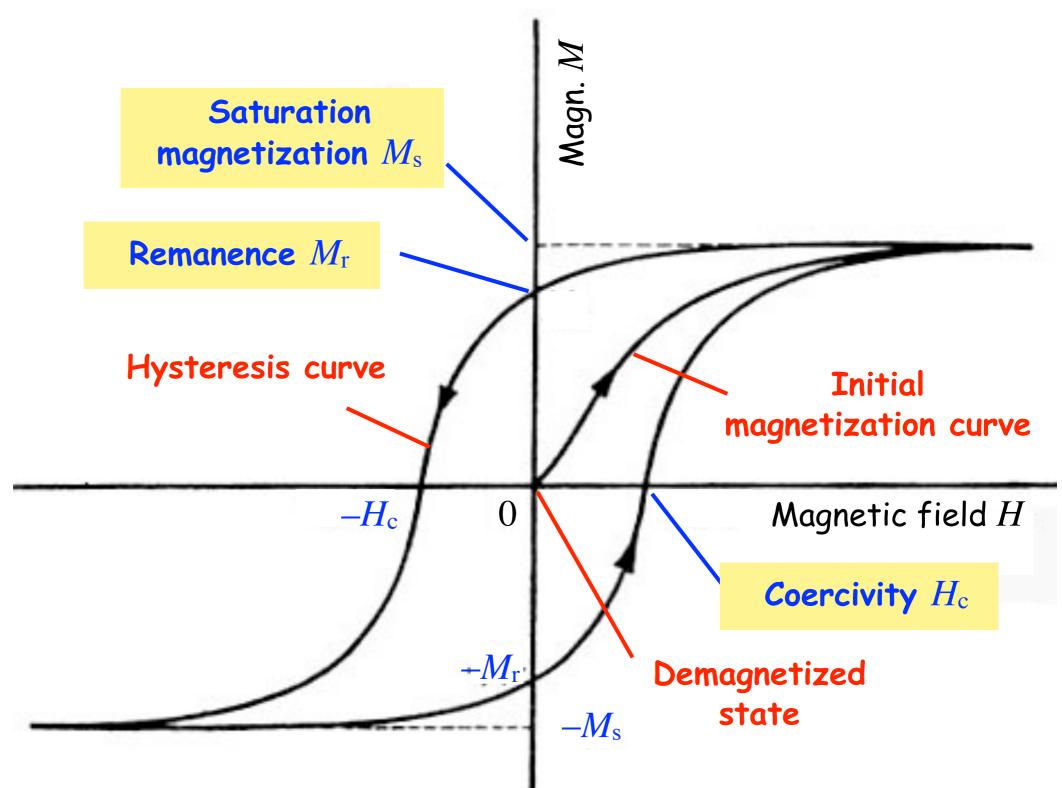
Demagnetizing field should be avoided when characterizing soft magnetic materials

Demagnetizing field can be tolerated when characterizing hard magnetic materials, provided it is accurately known and is possibly uniform

For finite, non-ellipsoidal samples the magnetization is non-uniform due to demagnetizing effects \rightarrow has to be considered when placing pick-up coil for inductive measurements

General aspects

Hysteresis curve:

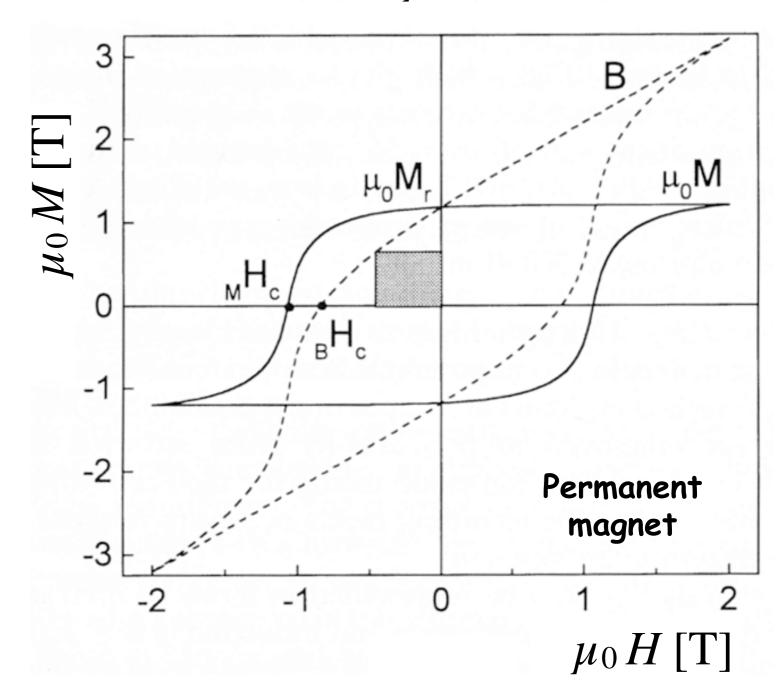


General aspects

Hysteresis curve: B and M

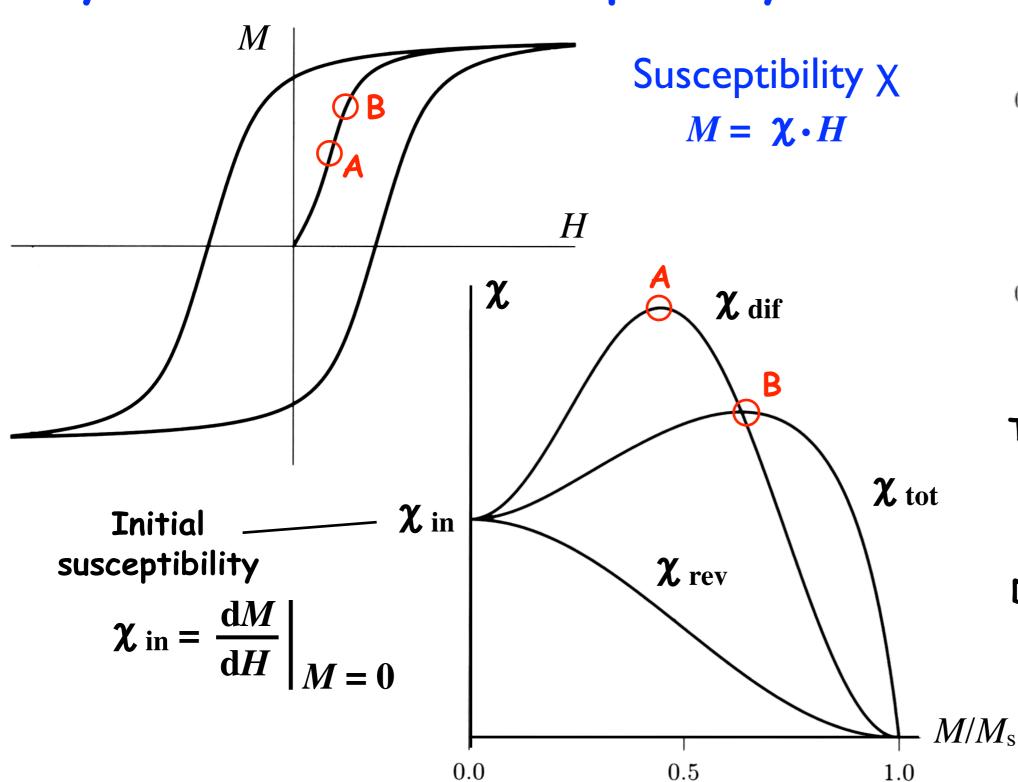
- Difference between M(H) and B(H)
- Soft magnets:
 Fields involved in hysteresis loop are much smaller than corresponding magnetization values
 - $\rightarrow B \cong \mu_0 M$
 - \rightarrow difference between B(H) and M(H) negligible
- Hard magnets: H and M have comparable orders $\to B(H)$ significantly different from M(H)

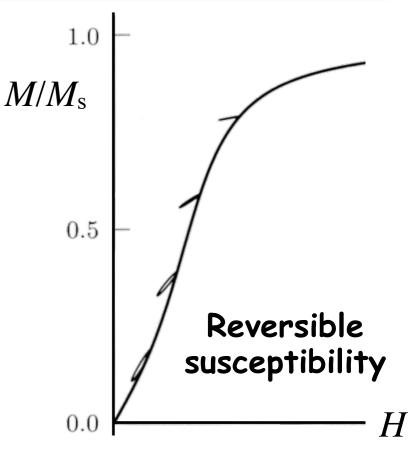




General aspects

Hysteresis curve: Susceptibility





Total susceptibility:

$$\chi_{\text{tot}} = \frac{M}{H}$$

Differential suscept.:

$$\chi_{\text{dif}} = \frac{dM}{dH}$$

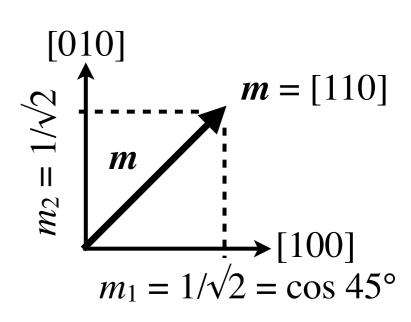
General aspects

Hysteresis curve: Anisotropy

- Magnetic anisotropy is defined as energy differences needed for saturation along different axes \rightarrow Magnetic anisotropy can be determined from M(H)-curve for single crystals by comparing magnetization curves along hard- and easy directions
- Example: cubic magnetocrystalline anisotropy (case of iron)

$$e_{\mathrm{Kc}} = K_{\mathrm{c}1} \cdot (m_1^2 m_2^2 + m_1^2 m_3^2 + m_2^2 m_3^2) + K_{\mathrm{c}2} \, m_1^2 m_2^2 m_3^2$$
 $m_{\mathrm{i}} = \mathrm{Magnetization} \; \mathrm{components} \; \mathrm{along} \; \mathrm{cubic} \; \mathrm{axes} \; (\mathrm{direction} \; \mathrm{cosine})$
 $K_{\mathrm{c}i} = \mathrm{Anisotropy} \; \mathrm{constants}$

$$m = [100]$$
: $e_{Kc} = 0$
 $m = [110]$: $m_1 = m_2 = 1/\sqrt{2}$
 $e_{Kc} = K_{c1} (1/2+0+0) = K_{c1}/4$
 $m = [111]$: $m_1 = m_2 = m_3 = 1/\sqrt{3}$
 $e_{Kc} = K_{c1} (1/9+1/9+1/9) + 1/27 K_{c2}$
 $= 1/3 K_{c1} + 1/27 K_{c2}$



3. Magne

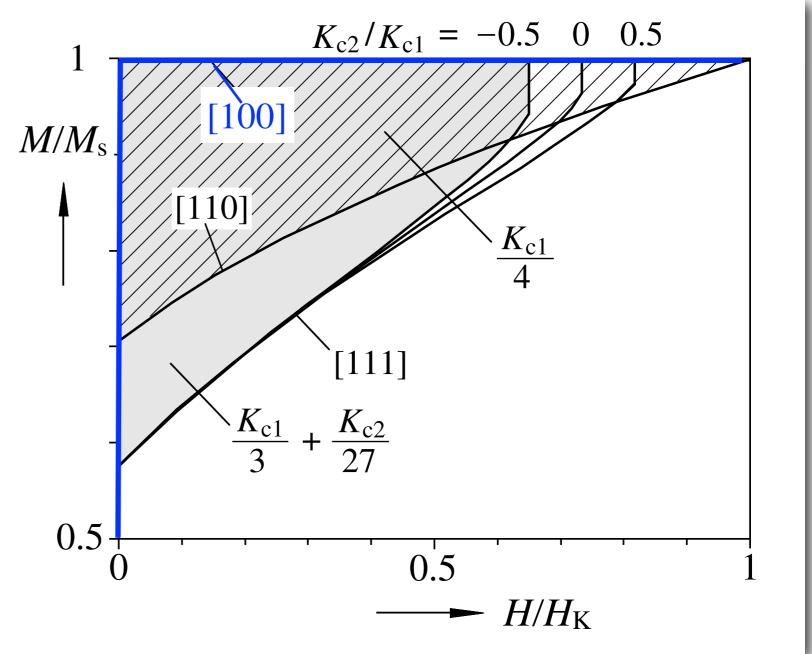
Hysteresis curve: Ar

- Magnetic anisotropy is defined different axes → Magnetic ar single crystals by comparing n
- · Example: cubic magnetocrysta

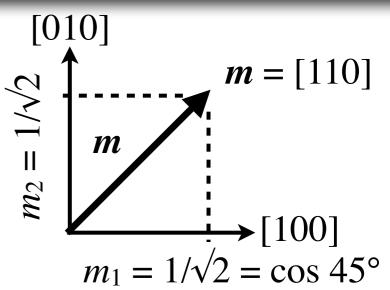
$$e_{Kc} = K_{c1} \cdot (m_1^2 m_2^2 + m_1^2 m_3^2)$$

 $m_{\rm i}$ = Magnetization com

 K_{ci} = Anisotropy constal



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General aspects

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```
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K_{\mathrm{c}i} = \mathrm{Anisotropy} \; \mathrm{constants}
```

· Limitations:

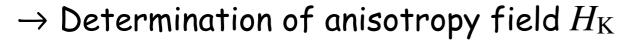
- Hysteresis effects make the determination of the area ambiguous. Relying on the idealized magnetization curve offers fair solution to this problem
- Non-ideal behaviour in approach to saturation. Internal stresses, inclusions and shape irregularities lead to a rounding of the magnetization curve. These effects depend on the magnetization direction because the magnetization deviations around such irregularities are influenced by anisotropy. The direct determination of the anisotropy from the magnetization curves is therefore often unreliable

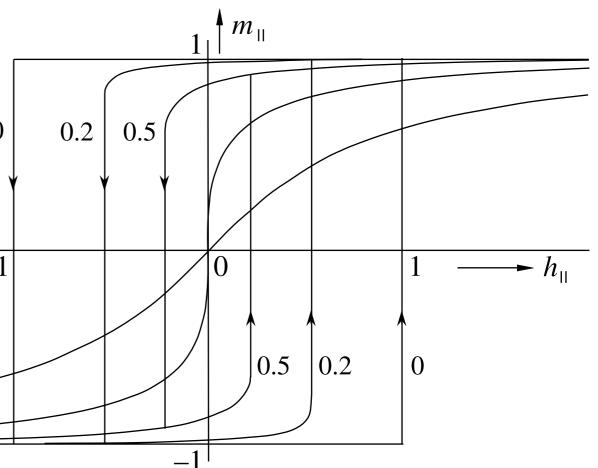
General aspects

Hysteresis curve: Anisotropy

Singular Point Detection in polycrystals

- Detects singularities in magnetization curve of polycrystalline sample which are caused by singular contributions from certain grains
- Compare magnetization curves of uniaxial particles: There are field orientations for which curves are smooth, for others they show characteristic jumps = first-order magnetization transitions $h_{\perp} = 0$
- In polycrystalline sample: jumps of accordingly oriented grains will show up _____ as singularities (maxima) in the second derivative of the magnetization curve, while the other grains only contribute to a smooth background



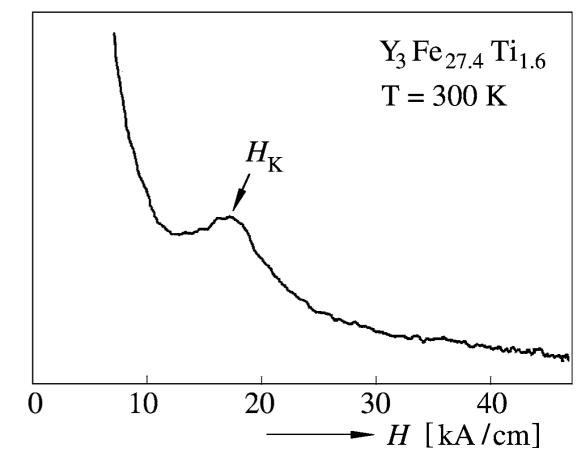


General aspects

Hysteresis curve: Anisotropy

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- In polycrystalline sample: jumps of accordingly oriented grains will show up as singularities (maxima) in the second derivative of the magnetization curve, while the other grains only contribute to a smooth background
 - ightarrow Determination of anisotropy field $H_{
 m K}$

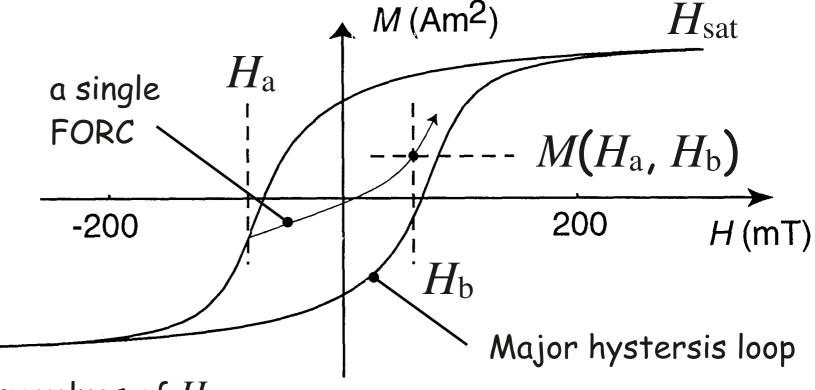


Courtesy R. Grössinger, Vienna

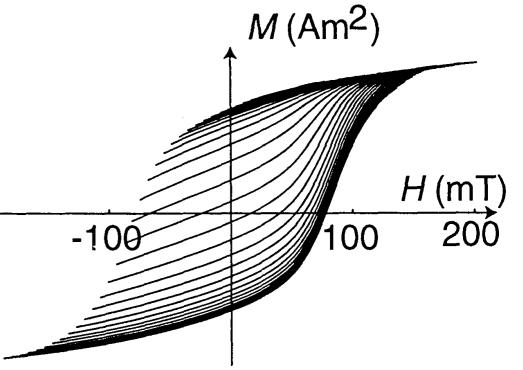
General aspects

FORC: First Order Reversal Curve

• A FORC is measured by saturating sample in field $H_{\rm sat}$, decreasing the field to a reversal field $H_{\rm a}$, then sweeping field back to $H_{\rm sat}$ in a series of equal field steps $H_{\rm b}$. The magnetization curve between $H_{\rm a}$ and $H_{\rm b}$ is a FORC

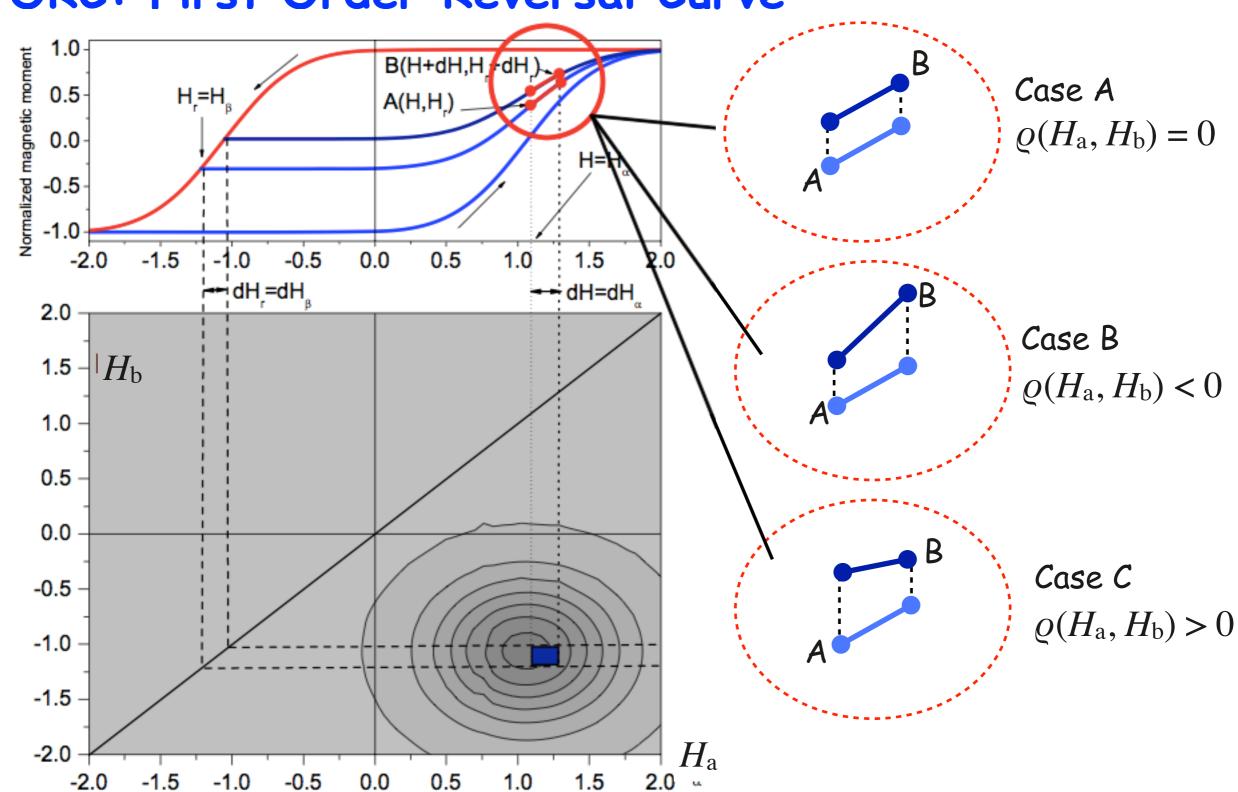


- This process is repeated for many values of $H_{\rm a}$ yielding a series of FORCs, and the measured magnetization at each step as a function of $H_{\rm a}$ and $H_{\rm b}$ gives $M(H_{\rm a},H_{\rm b})$ distribution
- The FORC distribution $\varrho(H_{\rm a},H_{\rm b})$ is defined as the mixed second derivative of the $M(H_{\rm a},H_{\rm b})$ surface: $\varrho(H_{\rm a},H_{\rm b})=-\ \partial^2 M(H_{\rm a},H_{\rm b})/\partial H_{\rm a}\ \partial H_{\rm b}$
- $\varrho(H_{\rm a},H_{\rm b})$ is plotted as contour- or 3D-plot



General aspects

FORC: First Order Reversal Curve



General aspects

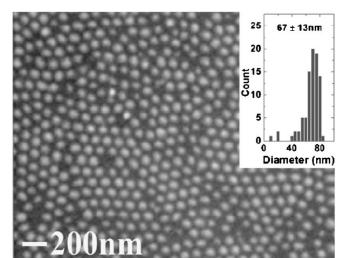
FORC: First Order Reversal Curve

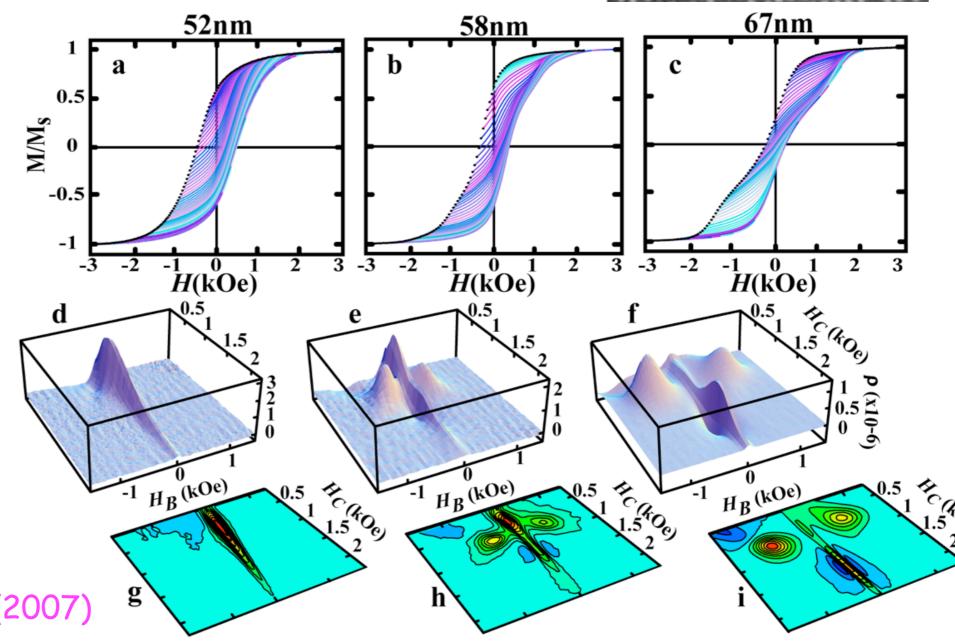
- Alternatively ϱ can be plotted in coordinates of $(H_{\rm C},H_{\rm B})$, where $H_{\rm C}$ is the local coercive field and $H_{\rm B}$ is the local interaction or bias field This transformation is accomplished by a rotation of the coordinate system defined by: $H_{\rm B} = (H_{\rm a} + H_{\rm b})/2$ and $H_{\rm C} = (H_{\rm a} H_{\rm b})/2$
- FORC distribution eliminates purely reversible components of magnetization process. Thus any non-zero ϱ corresponds to irreversible switching processes
- FORC thus provide insight into relative proportions of reversible and irreversible components of the magnetization process. Examples:
 - Exchange-coupled nanocomposite permanent magnet material: investigation of magnetostatic- and exchange interactions between hard and soft phases
 - Exchange-biased spin-valves: studies of the switching distribution and exchange bias in materials where the switching of the free layer magnetization is strongly influenced by the magnetic state of the fixed layer
 - Arrays of magnetic nanowires, nanodots or nanoparticles: investigation of irreversible magnetic interactions or processes in the array due to coupling between adjacent wires, dots or particles

General aspects

FORC: First Order Reversal Curve

Example: nanodot array of different dot diameter.
 Distinctly different reversal mechanisms, despite only subtle differences in the major hysteresis loops.



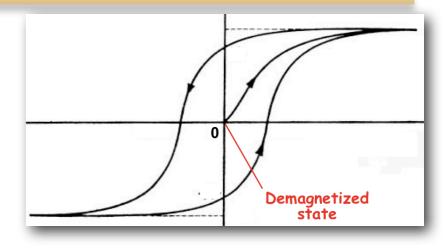


Courtesy Kai Liu, Davis Phys. Ref. B 75, 134405 (2007)

General aspects

Demagnetiziation

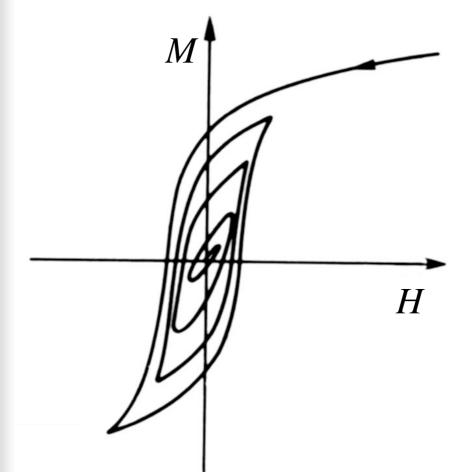
3 possibilities, to "demagnetize" a magnet (\overline{M} = 0) :



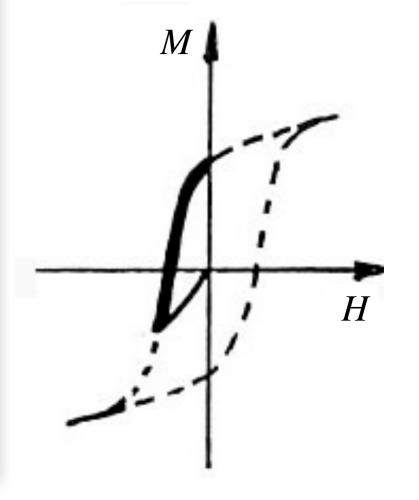
1. Thermal demagnetization

Heating above
Curie temperature
and cooling in
absence of
magnetic field

2. Cyclic (ac) demagnetization



2. dc-field demagnetization



In principle any point within or on the hysteresis loop can be obtained by choosing the right field history

3.

Magnetic Measurements to determine material parameters & properties

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

a) Inductive methods

Sample surrounded by coil, in which voltage is induced when magnetization of sample is changed or when sample is moved. Voltage is integrated \rightarrow signal proportional to magnetization

b) Magnetometric methods

For finite samples: demagnetizing field, which is proportional to mean magnetization $(H_{\rm dem} = -N\overline{M})$, is measured

c) Optical magnetometry

Surface magnetization is measured by magneto-optic effect, useful for thin films where signal of inductive or magnetometric methods are too weak

a) Inductive methods Extraction Method

 Based on flux change in pick-up coil when sample is extracted from coil, or when specimen and pick-up coil together are extracted from field

Total flux through pick-up coil:

$$\Phi_1 = BA = \mu_0(H + M)A = \mu_0(H_a - H_d + M)A = \mu_0(H_a - N_dM + M)A$$

If sample is removed from pick-up coil, the flux through the coil becomes:

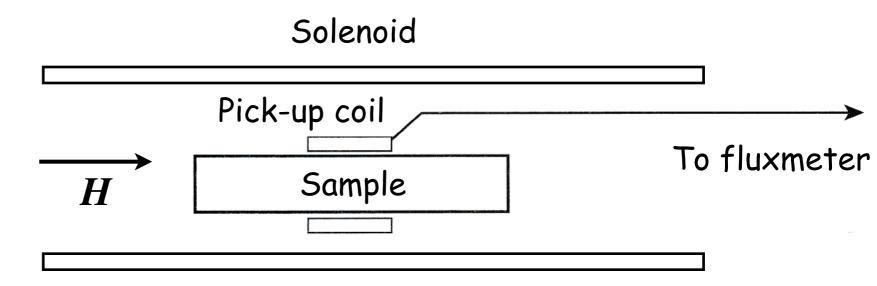
$$\Phi_2 = \mu_0 H_a A$$

A: specimen or pick-up coil area

Fluxmeter will record a value proportional to flux change:

$$\Phi_1 - \Phi_2 = \mu_0 (1 - N_d) MA$$

- Extraction method measures M directly, rather than B
- Vibrating sample
 magnetometer may be
 regarded as kind of partial
 extraction method



a) Inductive methods

Measurement of closed circuit samples

 Conventional setup with primary and secondary winding

 Procedure: vary current through primary winding and measure its magnitude by voltage drop across shunt: Primary winding

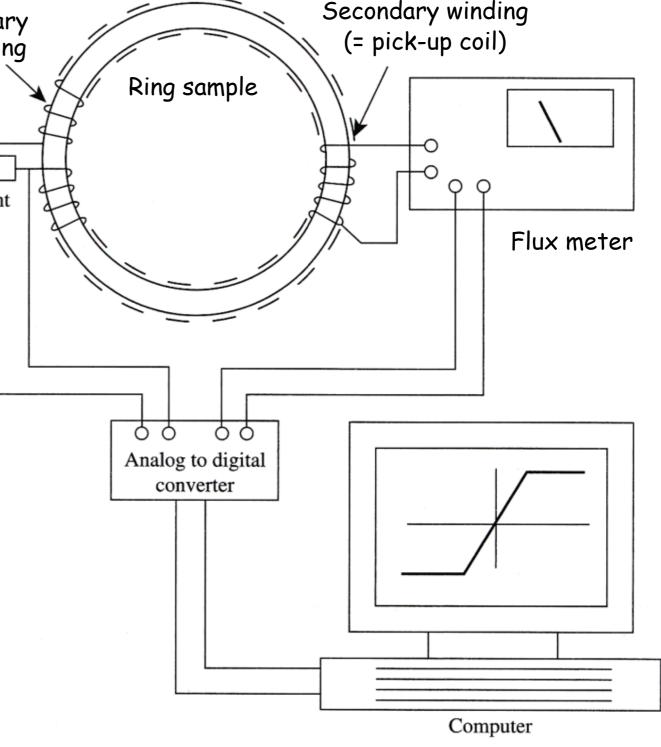
Shunt

Bipolar power supply

n: winding no.

 $H = nI/L_{\rm Fe}$ I: current, n: winding no. simultanously integrate output voltage from secondary winding with fluxmeter

 $oldsymbol{P}$ Measures flux density $oldsymbol{B}$, not M



Measurement of magnetic field strength

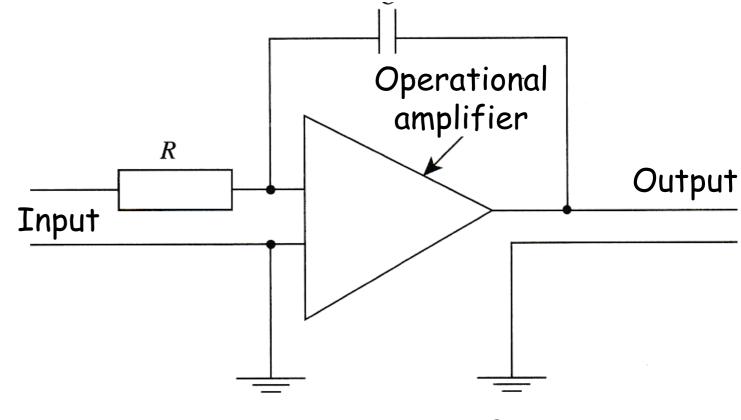
Fluxmeter

• Faraday's law: a changing magnetic flux φ through a coil of N turns generates a voltage in coil proportional to rate of change of flux:

$$U(t) = -N\frac{d\varphi}{dt} \quad \text{[Volt]}$$

$$U(t) dt = -N d\varphi$$

$$\int_{0}^{t} U(t) dt = -N \int_{\Phi_{1}}^{\Phi_{2}} d\varphi = -N \Delta \varphi \qquad U_{\text{out}} = -1/RC \int U_{\text{in}} dt$$



- Instrument to integrate voltage from pick-up coil is called fluxmeter = electronic integrator (based on capacitive feedback around operational amplifier) that provides voltage output
- With $B = \Phi/A$ (flux density in pick-up coil of cross section A):

$$\int U(t) dt = -N_{\text{pick-up}} A_{\text{pick-up}} \Delta B \text{ [Vs]}$$

Fluxmeter measures changes in flux density

Measurement of magnetic field strength

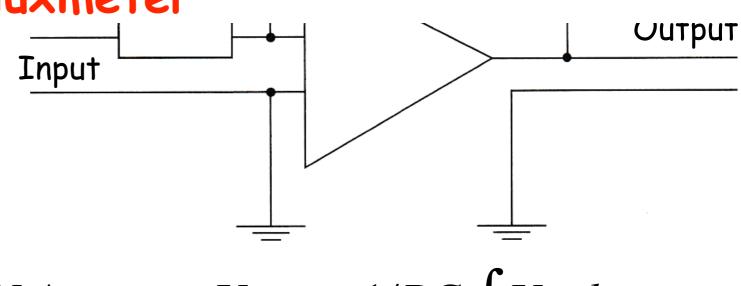
monar to rate of change of flux.

$$U(t) = -N \frac{d\varphi}{dt} \quad \text{[Volt]}$$

$$U(t) dt = -N d\varphi$$

$$\int_{0}^{t} U(t) dt = -N \int_{\Phi_{1}}^{\Phi_{2}} d\varphi = -N \Delta \varphi \qquad U_{\text{out}} = -1/RC \int U_{\text{in}} dt$$





$$U_{\rm out} = -1/RC \int U_{\rm in} \, dt$$

- Instrument to integrate voltage from pick-up coil is called fluxmeter = electronic integrator (based on capacitive feedback around operational amplifier) that provides voltage output
- With $B = \Phi/A$ (flux density in pick-up coil of cross section A):

$$\int U(t) dt = -N_{\text{pick-up}} A_{\text{pick-up}} \Delta B \text{ [Vs]}$$

Fluxmeter measures changes in flux density

Pick-up coil filled with (e.g.) iron:

$$\int U(t) dt = -N_{\text{pick-up}} A_{\text{Fe}} \Delta B \implies \Delta B = -\frac{1}{N_{\text{pick-up}} A_{\text{Fe}}} \int_{0}^{t} U(t) dt$$

a) Inductive methods

Measurement of closed circuit samples

 Conventional setup with primary and secondary winding

 Procedure: vary current through primary winding and measure its magnitude by voltage drop across shunt: Primary winding

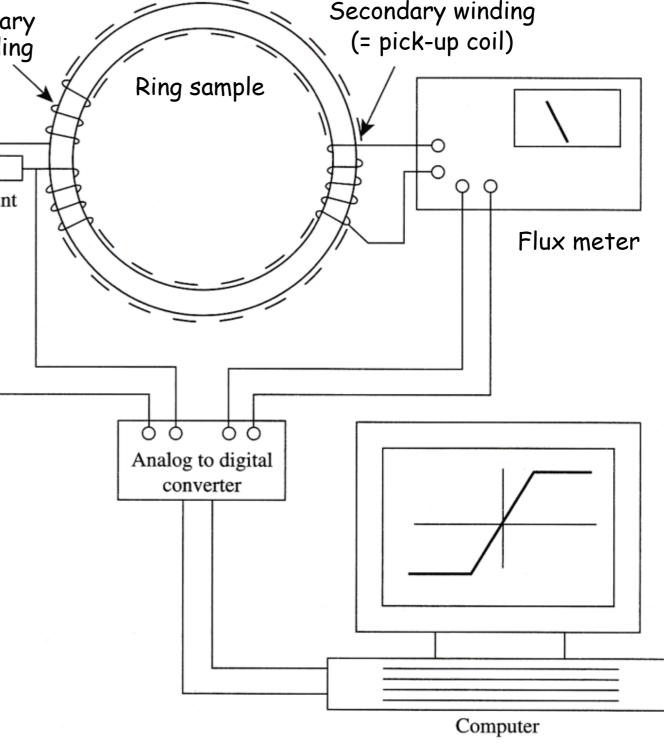
Shunt

Bipolar power supply

n: winding no.

 $H = nI/L_{\rm Fe}$ I: current, n: winding no. simultanously integrate output voltage from secondary winding with fluxmeter

 $oldsymbol{^{}}}}}}}}}}} } Not}\,M}}$



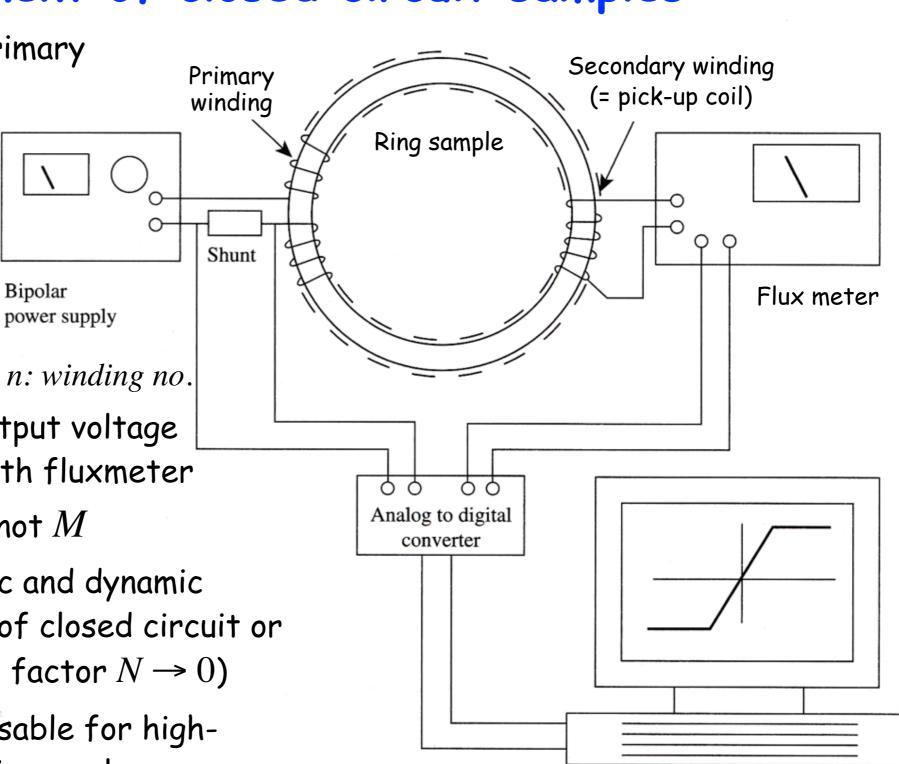
a) Inductive methods

Measurement of closed circuit samples

- Conventional setup with primary and secondary winding
- Procedure: vary current through primary winding and measure its magnitude by voltage drop across shunt:

 $H = nI/L_{\rm Fe}$ I: current, n: winding no. simultanously integrate output voltage from secondary winding with fluxmeter

- Measures flux density B, not M
- Can be used for quasistatic and dynamic hysteresis measurements of closed circuit or elongated samples (demag. factor $N \to 0$)
- Such geometry is indispensable for highpermeability, soft magnetic samples

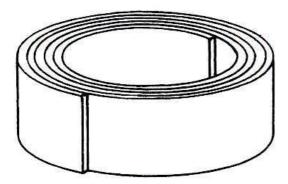


Computer

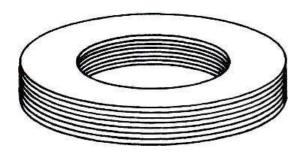
a) Inductive methods

Measurement of closed circuit samples

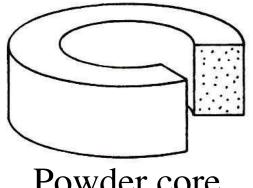




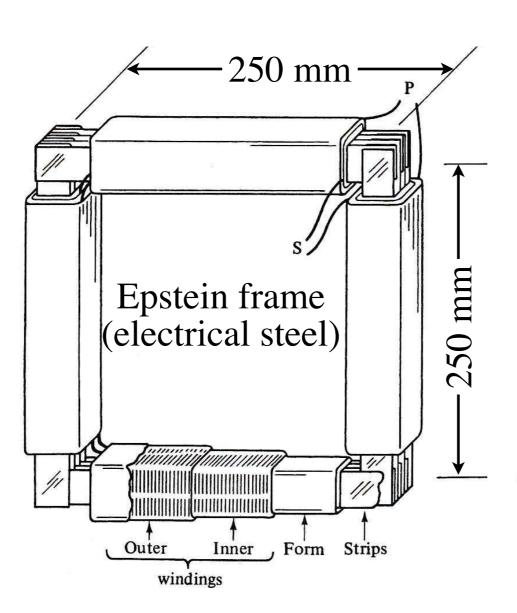
Tape-wound core

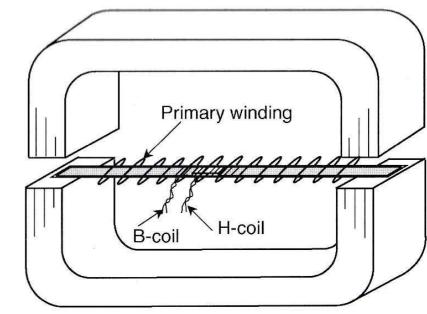


Stacked lamination

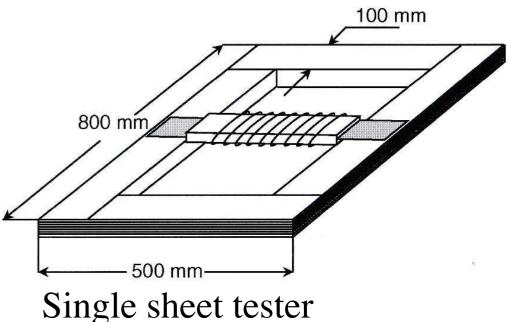


Powder core



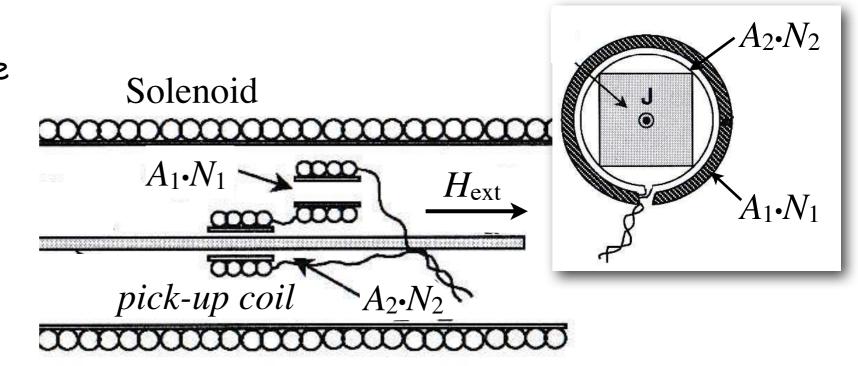


Laminated yoke for sheet samples (permeameter)



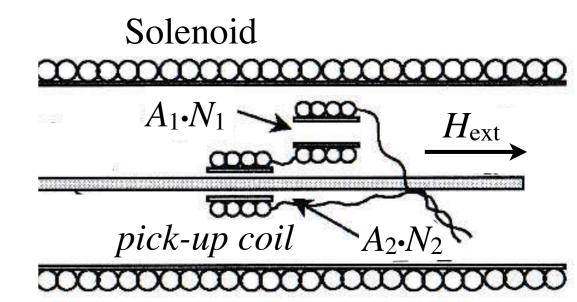
a) Inductive methods Measurement of closed circuit samples

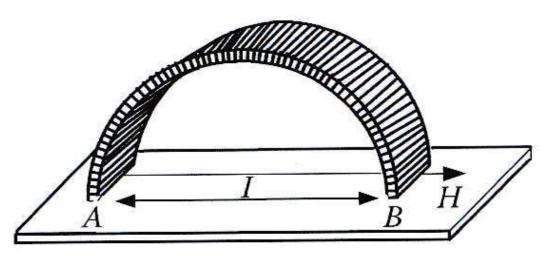
- $B = \mu_0 H + J \longrightarrow$
 - If J(H) is to be measured instead of B(H): Air flux compensation required to subtract effect of applied field
 - Compensation coil arrangement: 2 coils with equal winding areas $A_1 \cdot N_1 = A_2 \cdot N_2$ ($A_{1,2}$: cross sectional area of coils, $N_{1,2}$: number of turns) are connected electrically in opposition \rightarrow difference signal is proportional to magnetization alone, i.e. without specimen in pick-up coil: no flux recorded by fluxmeter, with specimen in pick-up coil: fluxmeter reads $J = B \mu_0 H$
 - Two possibilities: (i) two
 identical coils arranged side
 by side; (ii) external layers
 of the winding of a coil can
 be connected in such a way
 that their winding area is
 equal and opposite to the
 core winding area



a) Inductive methods Measurement of closed circuit samples

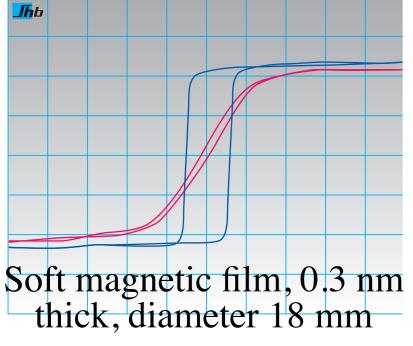
- Measurement of field strength:
 - Signal induced in compensation coil can also be used to measure the effective internal field
 - Maxwell's equations: tangential component of magnetic field must be equal on both sides of sample surface (if no current is flowing in sample surface)
 - → A coil placed close to the surface may therefore measure the internal field
 - With this technique the unsheared magnetization curve can be measured even for short samples
 - Alternative: Rogowski-Chattok coil





a) Inductive methods Loop tracer for magnetic films

- Highly sensitive commercial instrument to inductively measure M(H) loops in soft magnetic films
- Helmholtz coils: field up to 100 mT
- Frequency 1 10 Hz
- Alternative to Vibrating Sample Magnetometer



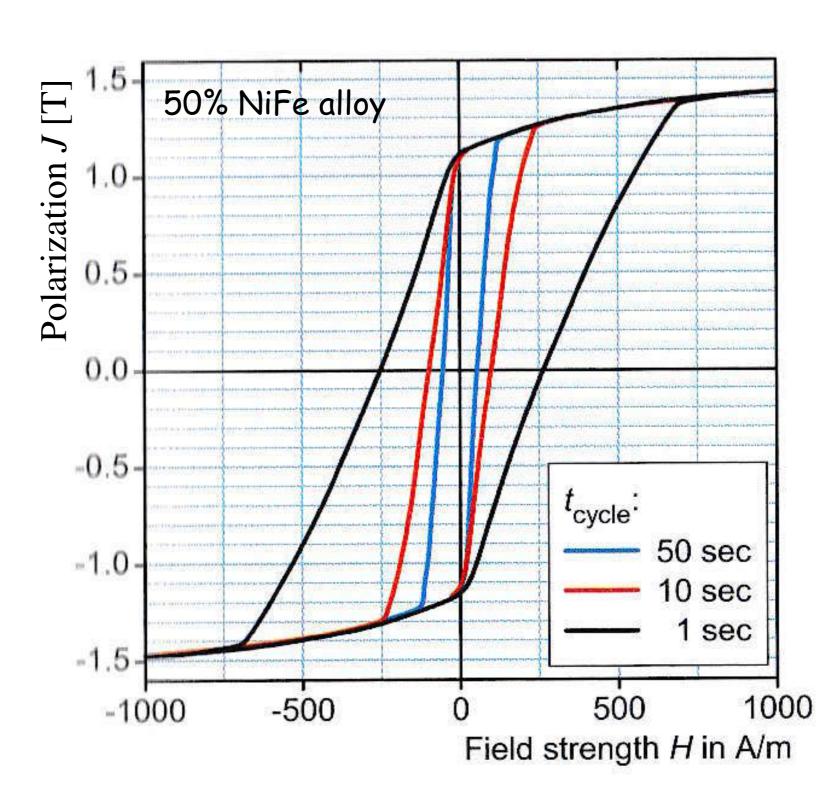


MESA http://www.shbinstruments.com



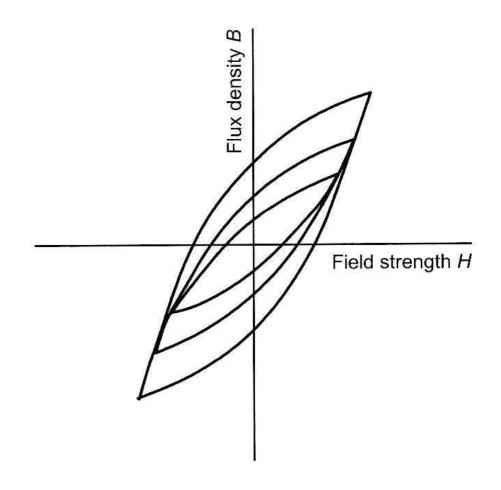
a) Inductive methods (Quasi-)static magnetization

- Quasistatic M(H) measurement: rate of magnetization $\mathrm{d}B/\mathrm{d}T$ and time for complete hysteresis cycle have to be low enough to eliminate all dynamic effects (like eddy currents, relaxaton processes etc.)
- Quasistatic loop is narrower than AC loop;
- Quasistatic coercivity is always lower than dynamic coercivity



a) Inductive methods Dynamic magnetization

- AC magnetization at low excitation level:
 - Field amplitude below coercive field (Rayleigh region)
 - Relationship between AC flux density and AC field strength can be represented by ratio factor (permeability) and phase angle (magnetic loss angle due to eddy currents)
 - Can be described in terms of classical eddy current theory



a) Inductive methods Dynamic magnetization

- · AC magnetization at high excitation level:
 - · AC excitation into region of maximum permeability and up to saturation
 - Severe distortions of magnetization due to non-linear behaviour of ferromagnetic material (S-like or rectangular hysteresis loops). Reason:
 - At high excitation level: material is subjected to rapid changes of H(t) or B(t)
 - Local magn. flux density cannot follow changes due to eddy curents
 - Consequence: Magnetization curve depends on frequency and mode of excitation
 - 2 modes of dynamic magnetization:
 - Voltage -controlled magnetization: induced voltage is controlled to be sinusoidal (by feedback loop) \rightarrow sinusoidal flux density $B(t) \rightarrow$ magnetizing current I(t) becomes dependent. Recommended as IEC standard
 - Current-controlled magnetization: magnetizing current is controlled to be sinusoidal (by high-impedence power source) \rightarrow sinusoidal field strength $H(t) \rightarrow U(t)$ and B(t) become dependent.

cont.

a) Inductive methods

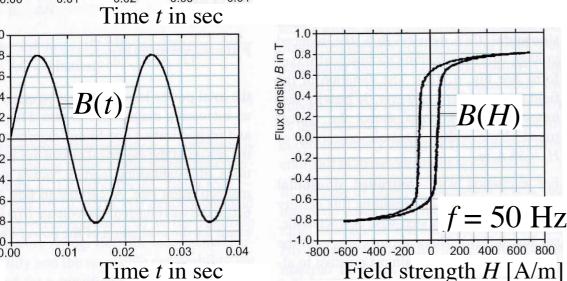
Dynamic magnetization

Controlled sinusoidal flux density B(t)

$$U(t) = (-)N_2 \cdot A_{\text{Fe}} \frac{dB}{dt}$$

→ Induced voltage U(t) also exhibits sinusoidal waveform

 $\rightarrow H(t)$ heavily distorted

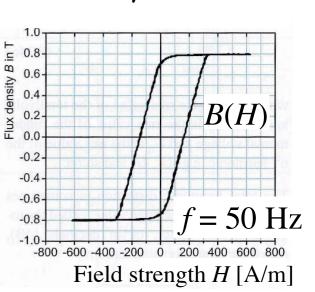


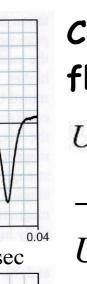
high excitation level

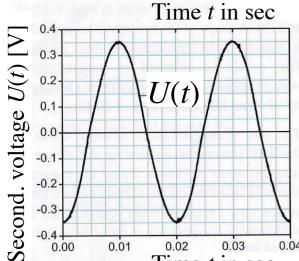
Controlled sinusoidal field strength H(t)

→ Step-wise characteristics of B(t). Abrupt changes of B(t) are traversed in short time interval

- → Spikes in induced voltage U(t)
- → Large eddy currents, sheared loop







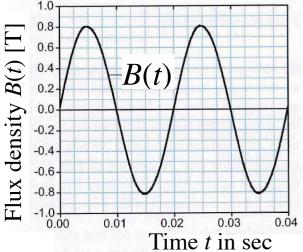
0.02

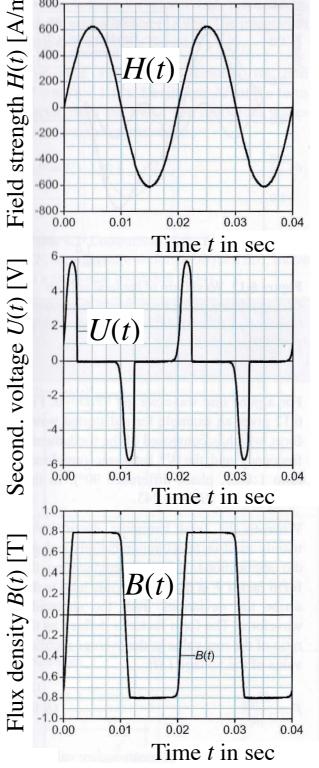
0.03

H(t)

0.01

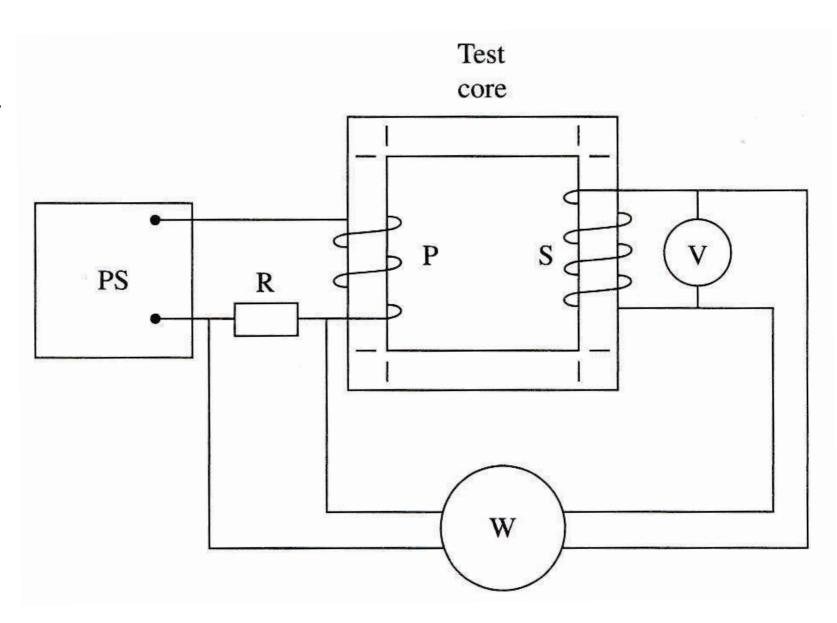
Field strength H(t) [A/m]





a) Inductive methods Loss measurement

- Wattmeter method (e.g.)
 - Measures core loss (not copper loss)
 - Losses are measured at certain maximum flux density and given frequency
 - Total weight of sample is recorded, and losses are reported in W/kg



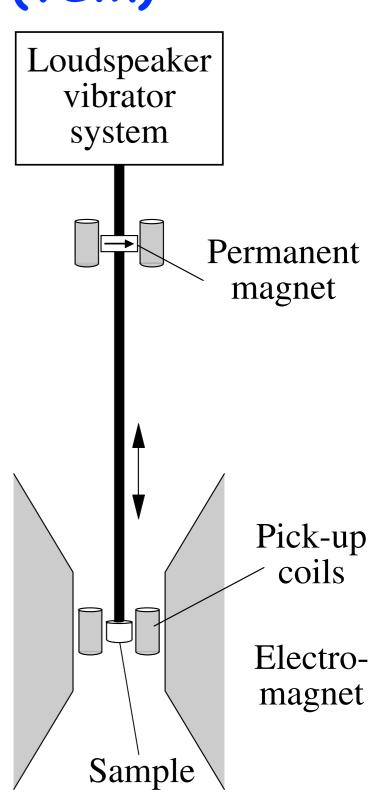
a) Inductive methods Loss measurement requency Energy loss Hysteresis loops of typical material, measured at rising frequency Frequency increases 10 \longrightarrow 100 Hz Total loss Excess eddy current loss Classical eddy current loss Hysteresis loss

Frequency

per cycle

Magnetic losses

- Sample placed inside magnet and vibrated perpendicular to field direction (frequ. ~ 100 Hz, vibration ampl. ~ 0.1 mm)
- Oscillating magnetic field of moving sample induces alternating voltage in pick-up coil, whose magnitude is proportinal to magnetic moment of sample
- The pick-up signal is amplified with lock-in amplifier and compared with the signal induced in a pair of reference coils by a permanent magnet or by some variable capacitor setup (only sensitive to vibration frequency)
- Strong external fields can be applied (superconducting magnets for hard magnetic materials)
- Since sample is well-separated from the pick-up coils, it can be surrounded by cooling or heating devices
- The sample magnetization is static in the VSM, so that no eddy current effects have to be considered
- The shape of the sample is largely arbitrary



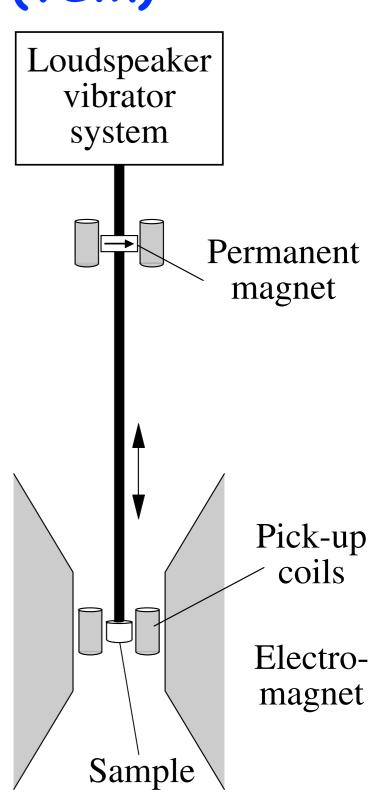
a) Inductive methods

Vibrating Sample Magnetometer (VSM)

- Sample placed inside magnet and vibrated perpendicular to field direction (frequ. ~ 100 Hz, vibration ampl. ~ 0.1 mm)
- Oscillating magnetic field of moving sample induces alternating voltage in pick-up coil, whose magnitude is proportinal to magnetic moment of sample
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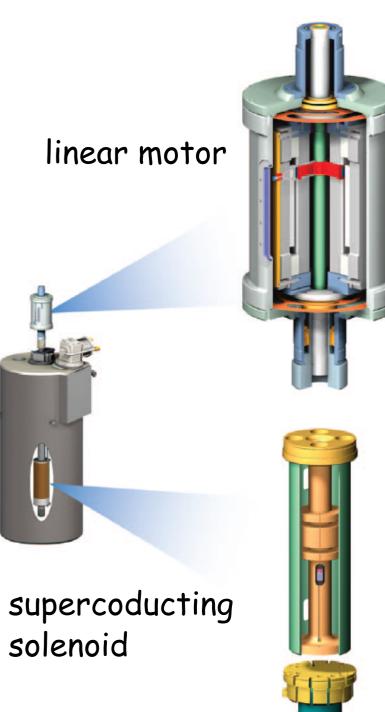


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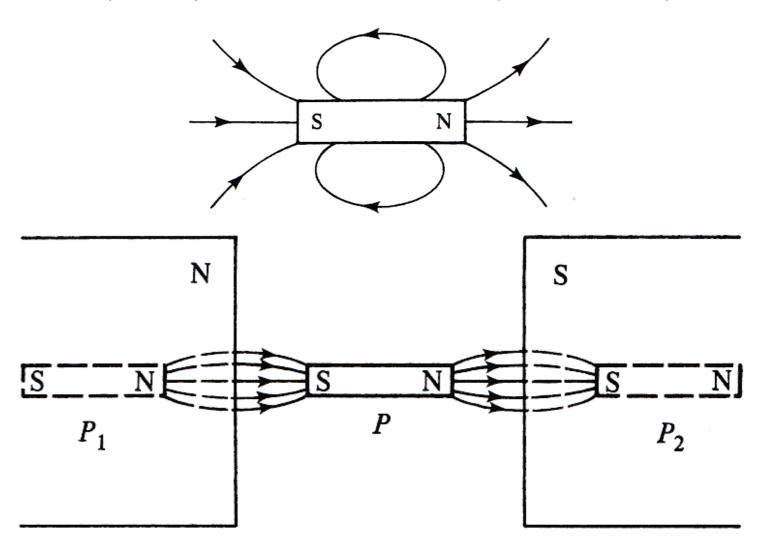
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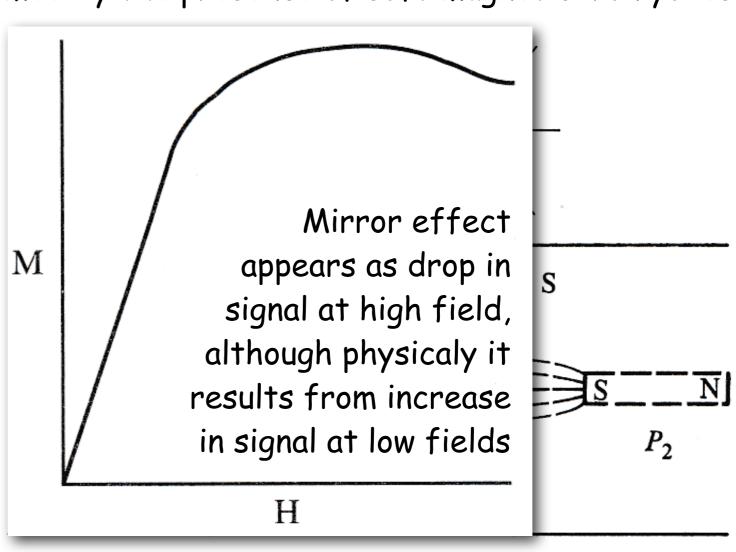


Courtesy Quantum Design.

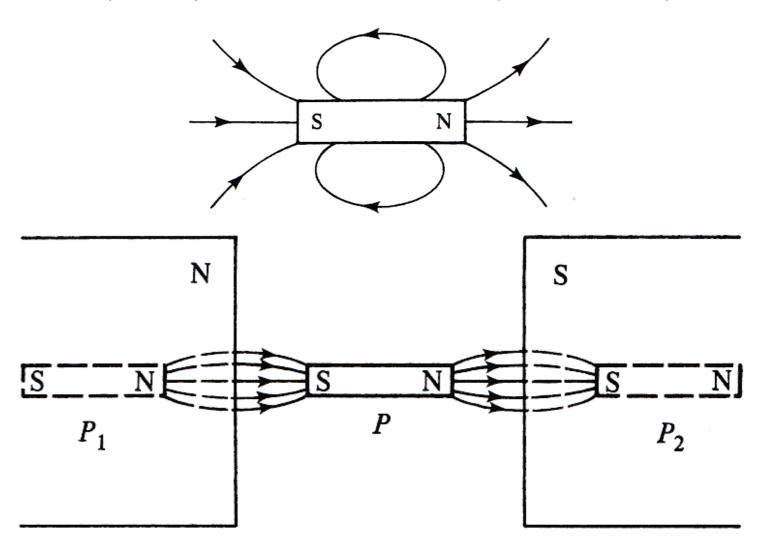
- Direct method. Ideally, no calibration would be needed to derive the magnetization of the sample if pick-up coil geometry and sample volume are known and if magnetic field could be generated by a simple air coil
- However: for electromagnets the pole material interacts with the measuring process: "mirror images" of the sample are formed by the presence of soft magnetic iron yokes
- → Mirror images also induce voltage in pick-up coil
- Strength of mirror images depends on permeability of iron yoke that in turn depends on the induction level in magnet
- → VSM must be calibrated by replacing sample by nickel sample of the same size and shape, and to rely on the accurately known saturation magnetization of nickel



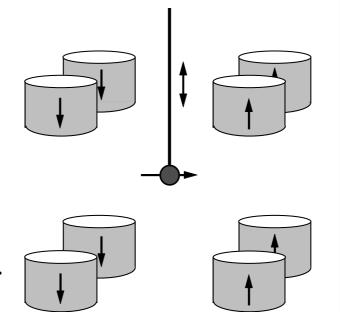
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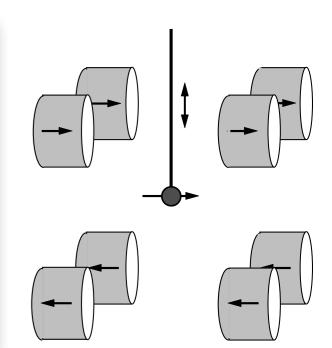


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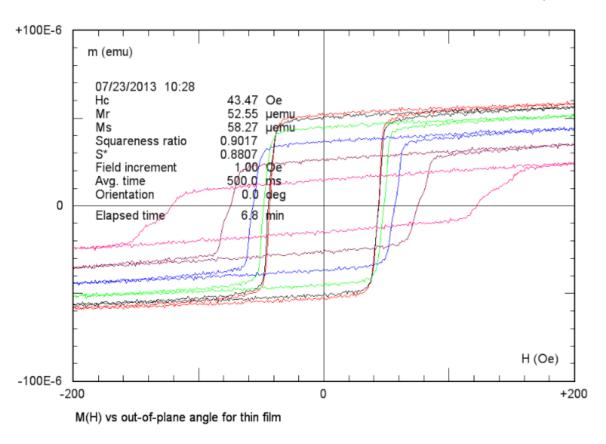


- VSM measures magnetic moment and therefore magnetization M whereas fluxmeter methods measure flux density B
- VSM is best method to measure the saturation magnetization $M_{
 m s}$ of any material because high field can be applied to reach saturation
- VSM less useful for measurement of other parameters of magnetization curve in soft magnetic materials because of demagnetization effects (real field unknown).
 Exception: thin films. For high-anisotropy or hard magnetic materials, however, the VSM is the preferred instrument for many kinds of magnetic measurements
- Sensitivity: 10^{-5} emu = 10^{-8} Am² \rightarrow small samples (< 1 gramm)
- Pick-up coil arangements to measure longitdinal and transverse magnetization components
- SQUID magnetometer: high-sensitive variant of VSM. Pick-up signal transformed to SQUID device outside magnet

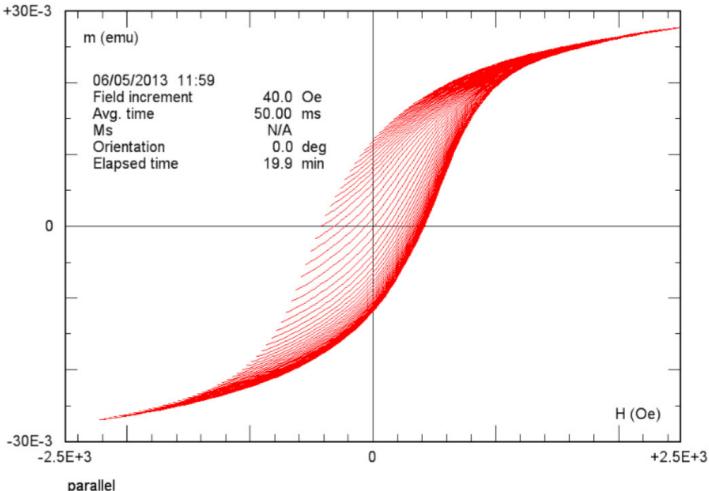




a) Inductive methods Vibrating Sample Magnetometer (VSM)



Examples



File: #3 Fe3O4 irradiated.FORC.50 ms.19 min

Courtesy Lakeshore

a) Inductive methods

Sample surrounded by coil, in which voltage is induced when magnetization of sample is changed or when sample is moved. Voltage is integrated \rightarrow signal proportional to magnetization

b) Magnetometric methods

For finite samples: demagnetizing field, which is proportional to mean magnetization $(H_{\rm dem} = -N\overline{M})$, is measured

c) Optical magnetometry

Surface magnetization is measured by magneto-optic effect, useful for thin films where signal of inductive or magnetometric methods are too weak

b) Magnetometric measurements

Field probes

 Magnetometer measures dipolar field generated by magnetized sample with the help of field detection device (like Hall probe)

In shown arrangement the difference signal of the two
probes is proportional to the
magnetic moment of the
sample, and insensitive to the
driving field



Sample

that only its dipolar field is detected \rightarrow samples should be small and short, but can be of any shape \rightarrow hard and high-anisotropy materials better suited than soft magnetic materials where demagnetization will dominate the intrinsic properties of short samples

 Advantages: (i) any sample shape, (ii) arbitrarily slow magnetization processes can be followed, (iii) sample can be easily exposed to various environmental conditions such as high or low temperature or mechanical stress.

c) Optical magnetometer

Magneto-optical Kerr effect

$$\mathbf{D} = \boldsymbol{\varepsilon} \, \mathbf{E} = \boldsymbol{\varepsilon} \, \begin{pmatrix} 1 & -i \, Q \, m_3 & i \, Q \, m_2 \\ i \, Q \, m_3 & 1 & -i \, Q \, m_1 \\ -i \, Q \, m_2 & i \, Q \, m_1 & 1 \end{pmatrix} \, \mathbf{E}$$

$$= \varepsilon \mathbf{E} + \mathrm{i} \varepsilon \mathbf{Q} \mathbf{m} \times \mathbf{E}$$

E: electric vector of light wave

D: dielectric displacement vector(= vector of light after reflection)

 m_i : components of magnetization vector (cubic crystal)

 \mathcal{E} : dielectric tensor

Q: material constant ($\sim M_s$, complex, determines strength of rotation)

c) Optical magnetometer

Magneto-optical Kerr effect

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$$= \varepsilon E + i \varepsilon Q m \times E \longrightarrow \text{concept of Lorentz force}$$

E: electric vector of light wave

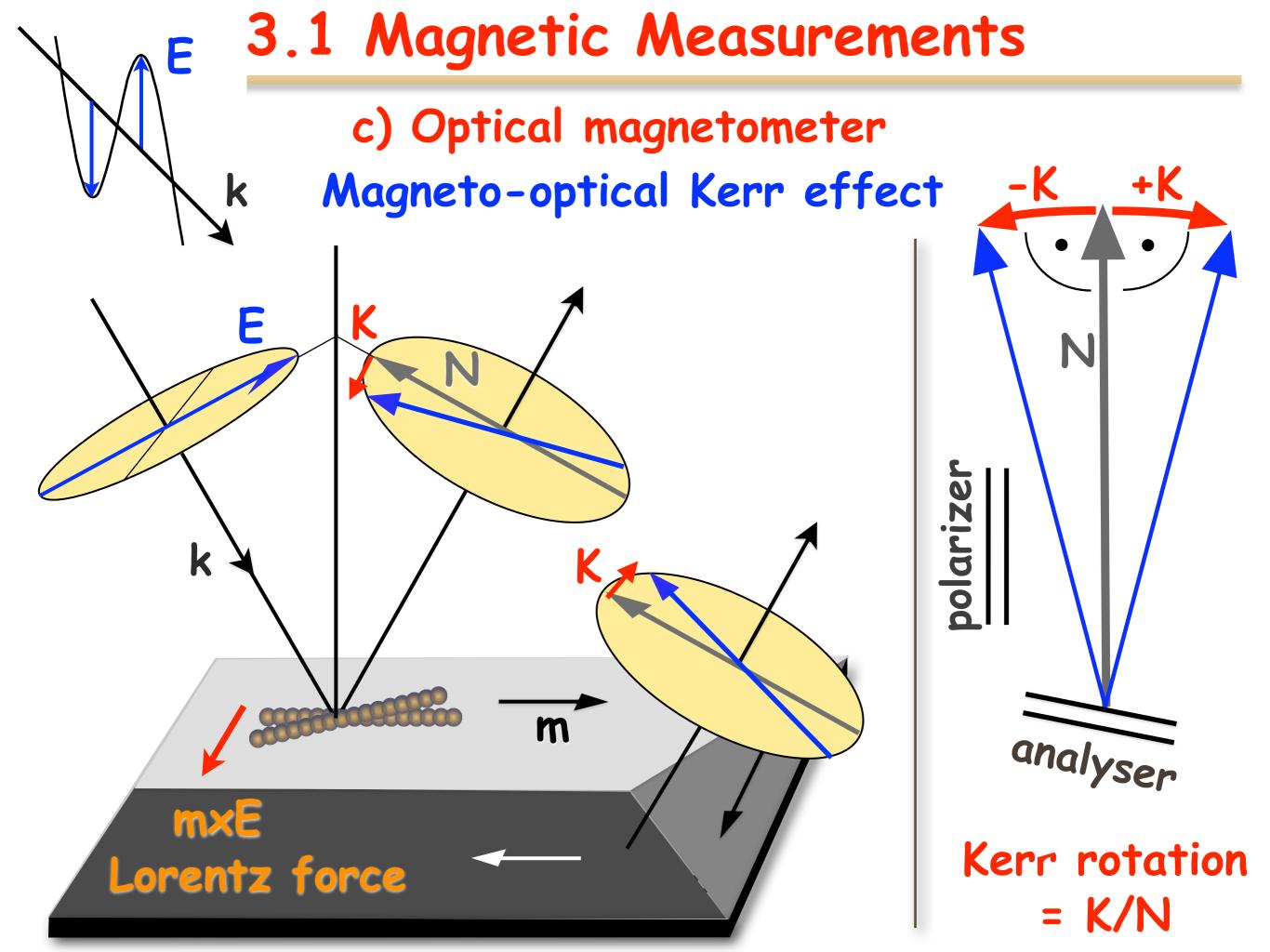
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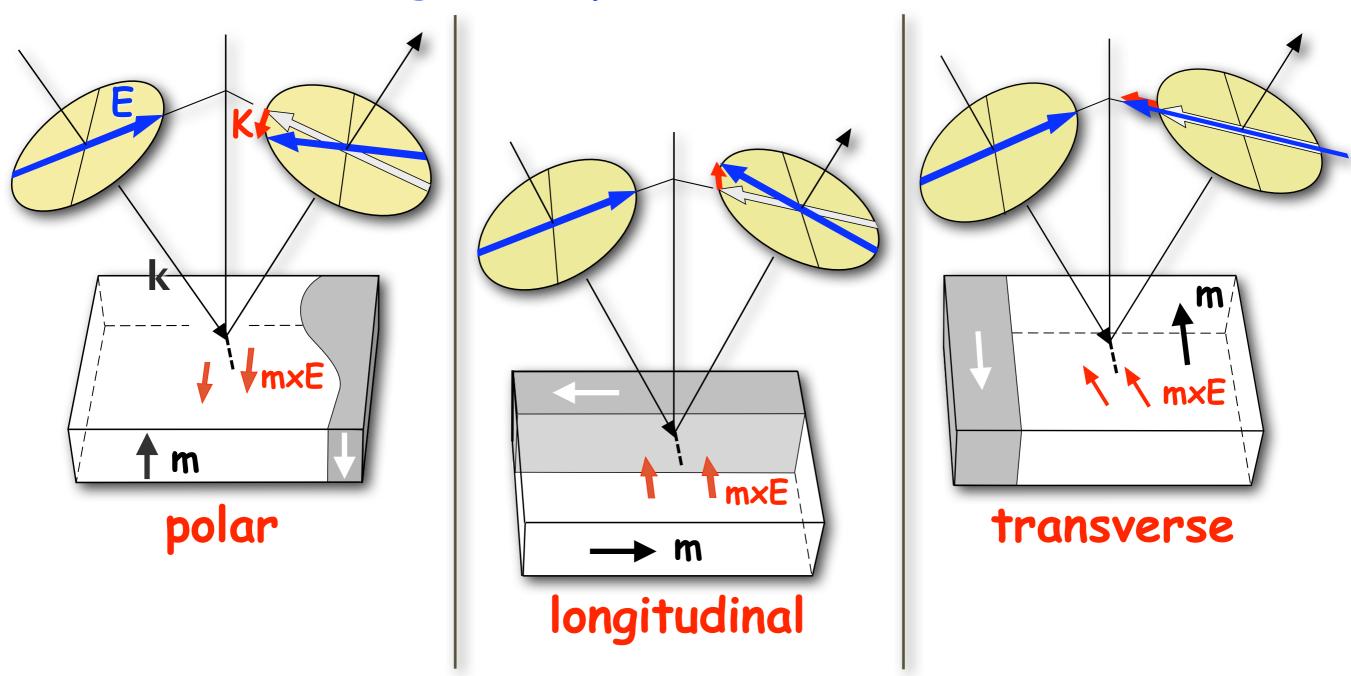
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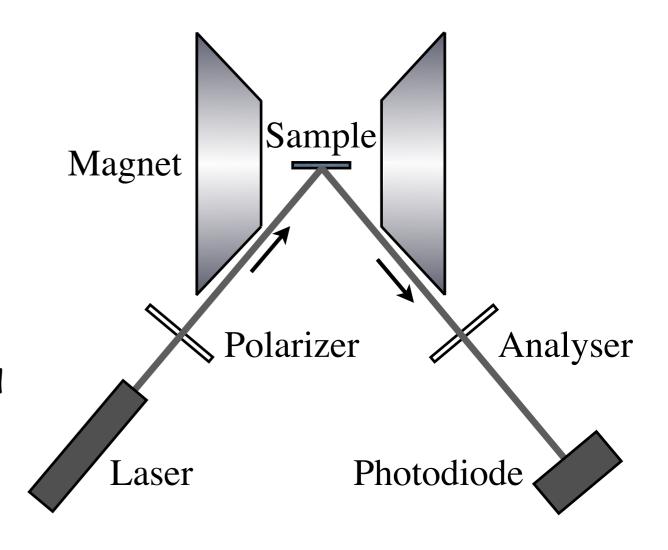
c) Optical magnetometer Magneto-optical Kerr effect



The Kerr effect causes a rotation of light, which is proportional to the magnetization component parallel to the reflected light beam

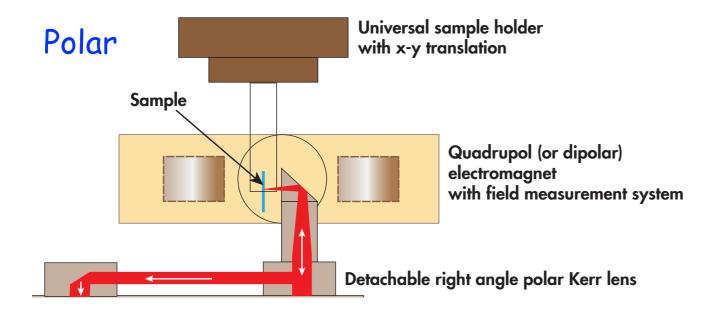
c) Optical magnetometer

- Magneto-optical Kerr effect is linear function of magnetization and therefore well-suited for magnetometry
- For non-transparent material optical magnetometry makes sense only for thin films for which surface magnetization is representative
- Advantages: (i) direct, (ii) quasi-static and dynamic measurements, (iii) Space-resolved measurements are possible by scanning over the surface. (iv) Optical measurements can be performed on-line during preparation or treatment of a material for example inside vacuum chamber
- Noise suppression: feed split-off part of laser light as reference signal into amplifier. If polarization of light is modulated by a spinning analyser or electrooptical device, the magnetic signal can be detected by a lock-in amplifier, thus achieving virtually unlimited sensitivity



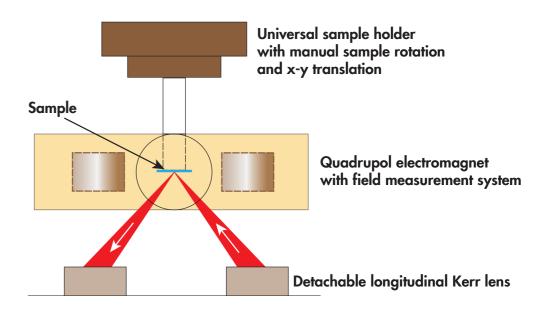
c) Optical magnetometer

Polar Kerr magnetometer (P-MOKE)

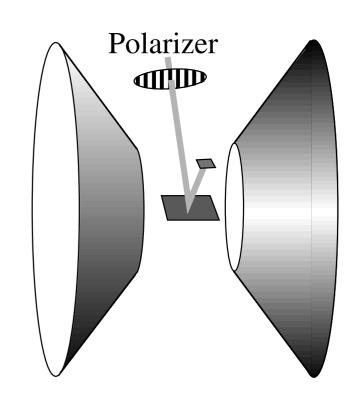


NANOMOKE3® http://www.lot-qd.de

Longitudinal



- Use of transverse Kerr effect (T-MOKE)
 - Polarizer set parallel to the plane of incidence and analyser omitted
 - M-component perpendicular to the plane of incidence causes variation of the reflected intensity, which can be detected electronically
 - Fits nicely into electromagnet



3.

Magnetic Measurements to determine material parameters & properties

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

Principle:

Measurement of mechanical forces on magnetic sample

Two possibilities:

• A uniform field H, acting on uniformly magnetized sample of magnetization M and volume V, generates a mechanical torque $T_{\rm m} = \mu_0 V H \times M$



• Gradient of non-uniform field generates a mechanical force $F_{\rm m} = \mu_0 V \, {\rm grad}(M \cdot H)$



a) Torque magnetometer

Most direct method to measure anisotropy

b) Field gradient mathods

Faraday Balance and Alternating Gradient Magnetometer

Principle:

Measurement of mechanical forces on magnetic sample

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a) Torque magnetometer

Most direct method to measure anisotropy

b) Field gradient mathods

Faraday Balance and Alternating Gradient Magnetometer

a) Torque magnetometer

- Torque measurements offer most direct methods for measuring anisotropies
- Requires uniform, single-crystalline samples, preferably of spherical or disk shape
- Example: crystal with cubic anisotropy:

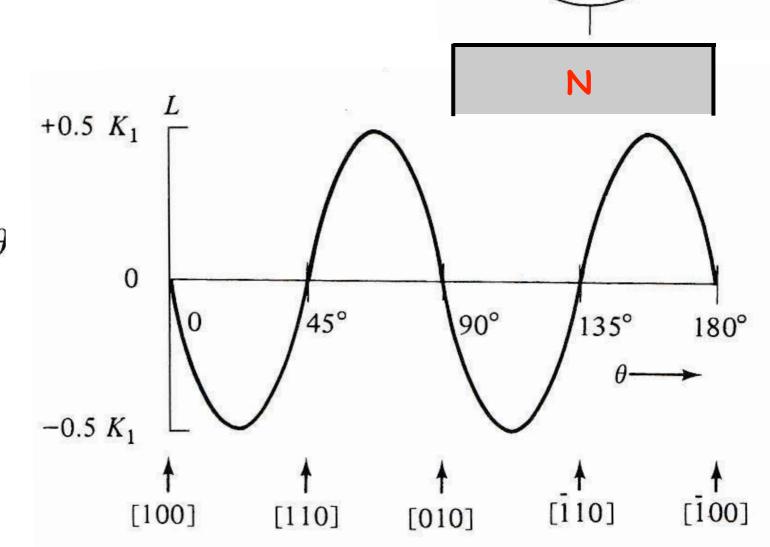
Anisotropy energy:

$$E=K_0+K_1\,\sin^2\!\theta\,\cos^2\!\theta,$$

Torque (assumption: $M_s \parallel H$):

$$L = -\frac{dE}{d\theta} = -K_1 \sin 2\theta \cos 2\theta$$
$$= -\frac{K_1}{2} \sin 4\theta.$$

 Anisotropy constant can be measured by torque measurement



5

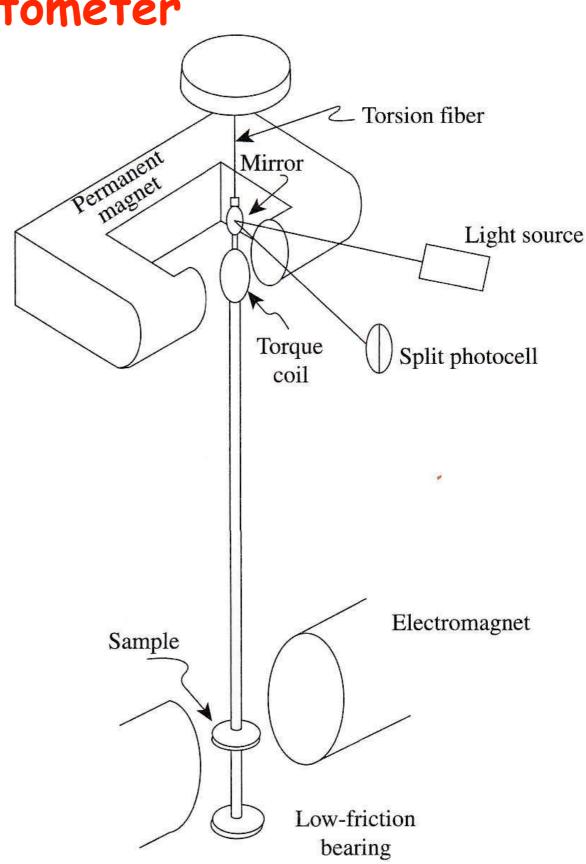
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[010]

a) Torque magnetometer

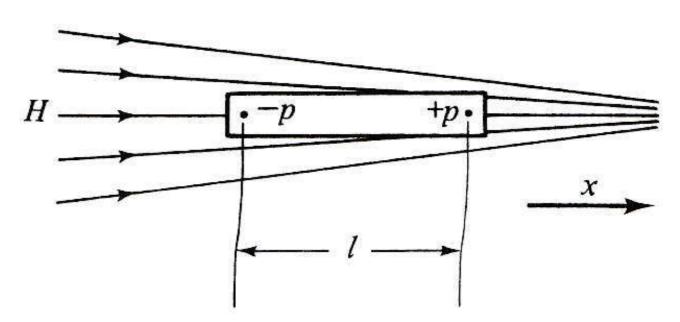
Example: Torque meter with active sensing

- Sample hung from sensitive torsion fiber, placed in electromagnet that can be rotated
- Torque coil, placed in field of permanent magnet. Current through torque coil: coil experiences torque proportional to current
- Sensing circuit (light beam, mirror, photocell)
 provides feedback signal that drives a
 current through the torque coil to balance
 the anisotropy torque of sample
- Value of current through torque coil is proportional to torque on sample



b) Field gradient methods Faraday Balance

- Measures static force on sample in magnetic field gradient:
- A non-spherical body in homogeneous field will rotate till its long axis is parallel to field (compass needle)
- Field gradient: in body of positive susceptibilit χ poles of strength p are produced
- Since field is stronger at north pole than at south pole: net force $F_{\rm x}$ to right, with m = magnetic moment and v = volume of body
- Body will move toward region of greater field strength (to right)



$$F_x = -pH + p\left(H + l\frac{dH}{dx}\right)$$

$$= pl\frac{dH}{dx} = m\frac{dH}{dx} = Mv\frac{dH}{dx}$$

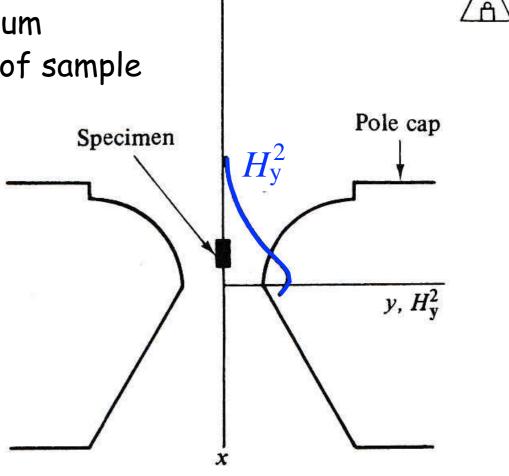
$$= \chi vH\frac{dH}{dx} = \frac{\chi v}{2}\frac{dH^2}{dx}$$

b) Field gradient methods Faraday Balance

- · Measures static force on sample in magnetic field gradient
- Uniform field is generated by electromagnet, and the gradient field is produced by an additional coil-set, optimized for a uniform magnetic gradient along y-axis
- If sample is mounted elastically, it is displaced by force:

$$F_{\rm x} = (\chi - \chi_0)vH_{\rm y}\frac{dH_{\rm y}}{dx} \qquad \begin{array}{l} \chi: \mbox{ susceptibility sample} \\ \chi_0: \mbox{ susceptibility medium} \\ vH_{\rm y}: \mbox{ magn. moment } m \mbox{ of sample} \end{array}$$

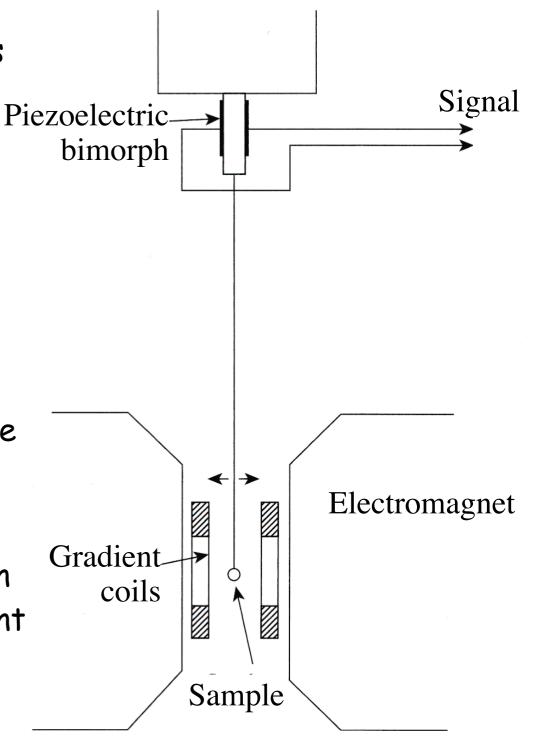
- Force can be detected and compensated by a calibrated electromagnetic counter-force.
 Compensation current is measure of force.
 Only quantity needed: sample volume
- Highly sensitive, can be applied to all kinds of magnetic substances
- In ferromagnetism it is best suited to measure the saturation magnetization with high precision



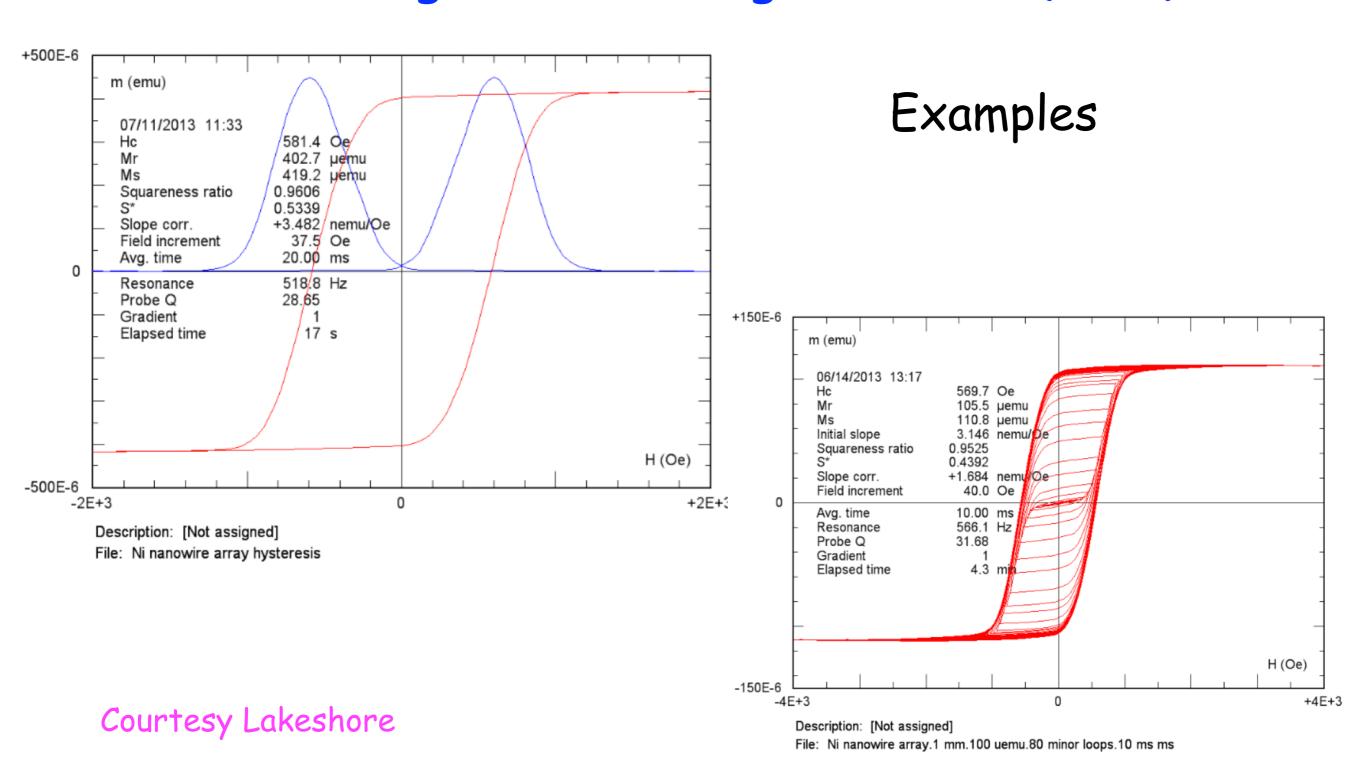
Balance

b) Field gradient methods Alternating Gradient Magnetometer (AGM)

- AGM (or Vibrating Reed Magnetometer) resembles superficially the VSM
- VSM: sample agitated mechanically and electric signal is derived from motion. AGM: magnetically excited signal is recorded
- Sample mounted on elastic cantilever or "reed",
 which is excited into resonant vibration by
 alternating gradient field (produced by gradient
 coils in addition to dc magnet) by chosing resonance
 frequency
- Vibration is recorded by piezoelectric pick-up system: generates voltage proportional to vibration amplitude = proportional to sample magnetic moment
- Sensitivity: $10^{-6} \, \mathrm{emu} = 10^{-9} \, \mathrm{Am^2} \to \mathrm{higher} \, \mathrm{than}$ VSM



b) Field gradient methods Alternating Gradient Magnetometer (AGM)



3.

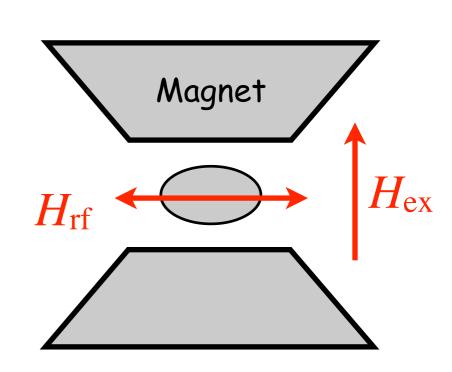
Magnetic Measurements to determine material parameters & properties

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

3.3 Resonance Techniques

Ferromagnetic Resonance (FMR)

- FMR is dynamic measurement method at microwave frequency (GHz-regime, order of Lamor frequency)
 - Because of high-frequency alternating magnetic field: eddy current shielding in metals is nearly complete (penetration depth of field \sim 200 nm)
 - \rightarrow resonance methods are not applicable to bulk metallic samples
 - ightarrow can only be applied to non-conducting oxidic materials, thin films, and powdered materials
- Typical resonance experiment:
 - Sample magnetized in strong static field H_{ex} to enforce uniformly magnetized state
 - To induce resonance phenomenen: alternating field with fixed GHz-frequency is superimposed at right angle to magnetization direction → stimulates precession of magnetization vector
 - The static field amplitude $H_{\rm ex}$ is swept till resonance is achieved at $H_{\rm ex}=H_{\rm res}$



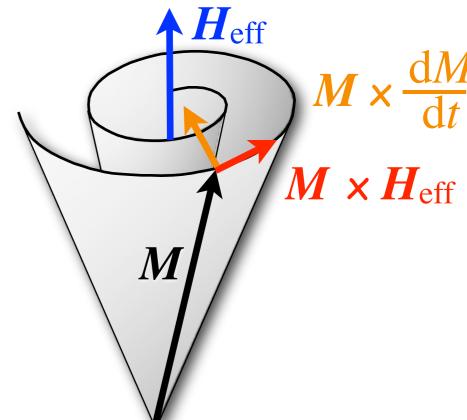
Ferromagnetic Resonance (FMR)

• Based on LLG equation:

$$\frac{\mathrm{d}\boldsymbol{M}}{\mathrm{d}t} = -\gamma_0 \left[\boldsymbol{M} \times \boldsymbol{H}_{\mathrm{eff}} \right] + \frac{\alpha}{M_s} \left[\boldsymbol{M} \times \frac{\mathrm{d}\boldsymbol{M}}{\mathrm{d}t} \right]$$

Desribes (damped) precession of M around effective field $H_{\rm eff}$, caused by gyrotropic reaction of magnetic moment due to its angular momentum





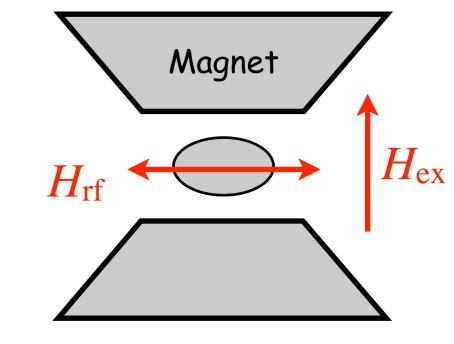
- At higher frequencies, non-uniform precession modes may be excited:
 - If their wavelength is comparable with sample size: magnetostatic modes
 - Resonance phenomena at shorter wavelengths depend on the exchange stiffness constant and are called spin-wave modes
 - Finally, there are surface modes of magnetic resonance which can be excited for example by light instead of an alternating field. Then spectroscopy replaces the standard inductive detection methods

-> Lecture of B. Hillebrands

Ferromagnetic Resonance (FMR)

- FMR experiment:
 - Static field $H_{\rm ex}$ with superimposed microwave field $H_{\rm rf}$ of fixed frequency
 - Static field amplitude $H_{\rm ex}$ is swept till resonance is achieved at $H_{\rm ex} = H_{\rm res}$ (sweeping of field is easier than sweeping microwave frequency)
- Resonance frequency ω_{res} and effective resonance field H_{res} are given by:

$$\omega_{\rm res} = \gamma H_{\rm res}$$
 with $\gamma = \mu_0 ge/2m_{\rm e}$

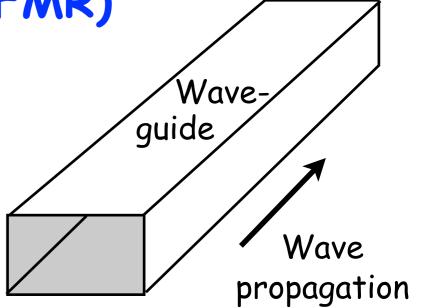


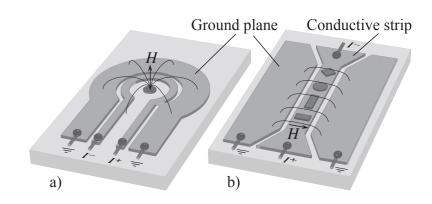
$$H_{\rm res} = \sqrt{\begin{bmatrix} 2K_{\rm u} \\ \overline{\mu_0 M_{\rm s}} + H_{\rm ex} + M_{\rm s} \left(N_{\rm b} - N_{\rm a}\right) \end{bmatrix} \begin{bmatrix} 2K_{\rm u} \\ \overline{\mu_0 M_{\rm s}} + H_{\rm ex} + M_{\rm s} \left(N_{\rm c} - N_{\rm a}\right) \end{bmatrix}}$$
 Anisotropy External Demagnetizing field field

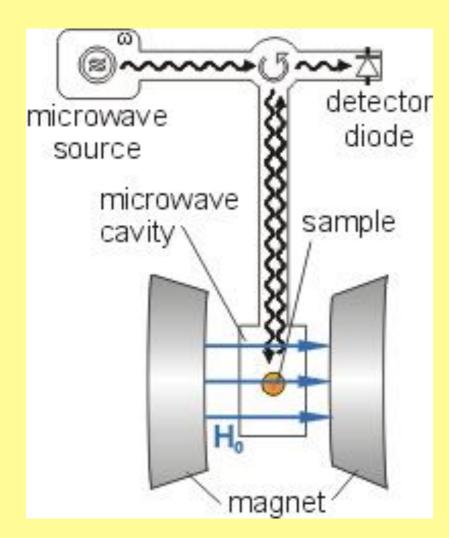
• If $M_{\rm s}$ and $N_{\rm i}$ are known \to anisotropy $K_{\rm u}$ can be derived from measuring $H_{\rm res}$

Ferromagnetic Resonance (FMR)

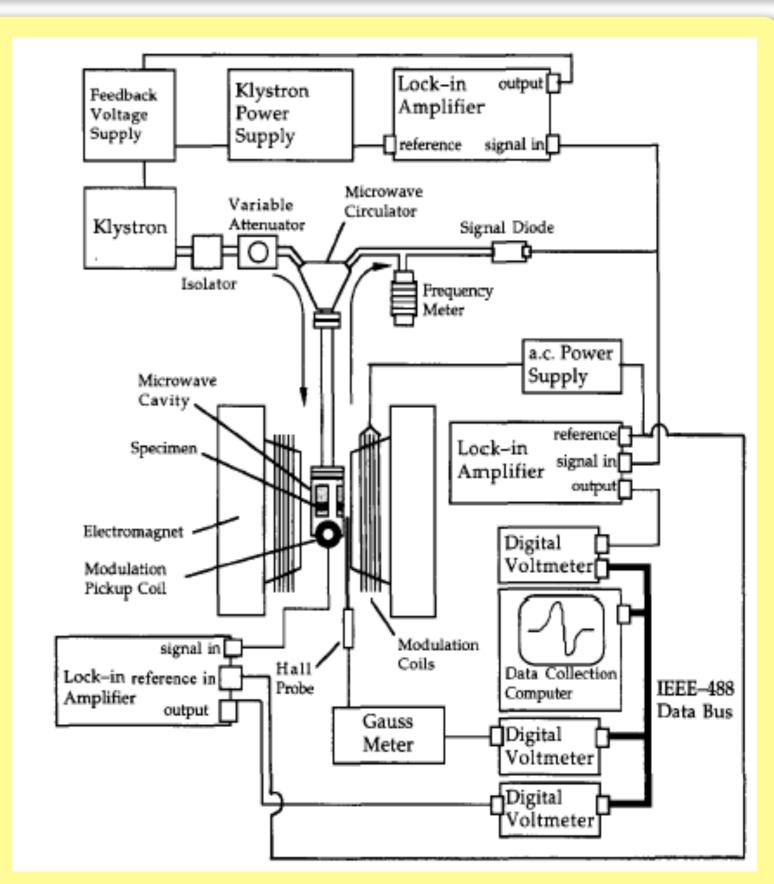
- FMR experiment:
 - Microwave field is generated by Klystron or Gunn diode and conducted to sample by wave guide (hollow metal tube)
 - Sample centered in microwave cavity (closed hollow metal structure), located in electromagnet
 - → Microwave frequency fixed and determined by klystron and cavity. Alternativly sample can be placed on micro-stripline







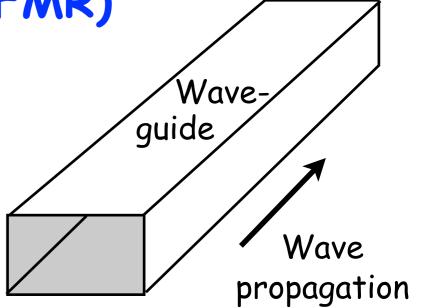
Courtesy Wolfgang Kuch

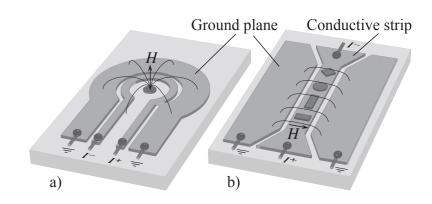


Courtesy Zbigniew Celinski

Ferromagnetic Resonance (FMR)

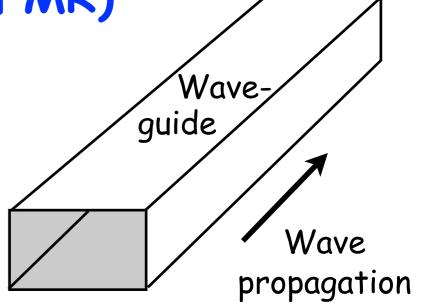
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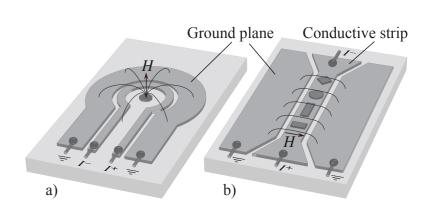




Ferromagnetic Resonance (FMR)

- FMR experiment:
 - Microwave field is generated by Klystron or Gunn diode and conducted to sample by wave guide (hollow metal tube)
 - Sample centered in microwave cavity (closed hollow metal structure), located in electromagnet
 - → Microwave frequency fixed and determined by klystron and cavity. Alternativly sample can be placed on micro-stripline
 - Incident microwave signal couples to sample and is partially absorbed in dependence of field strength H_{ex}
 - If resonance condition is fulfilled o max. absorption of microwave power by sample
 - Crystal detector measures reflected microwave signal. This signal is input into lock-in amplifier where it is compared with reference signal
 - Output of lockin vs. external field: corresponds to derivative of absorption curve, i.e the change of absorbed intensity I as function of $H_{\rm ex}$: ${\rm d}I/{\rm d}H_{\rm ex}$

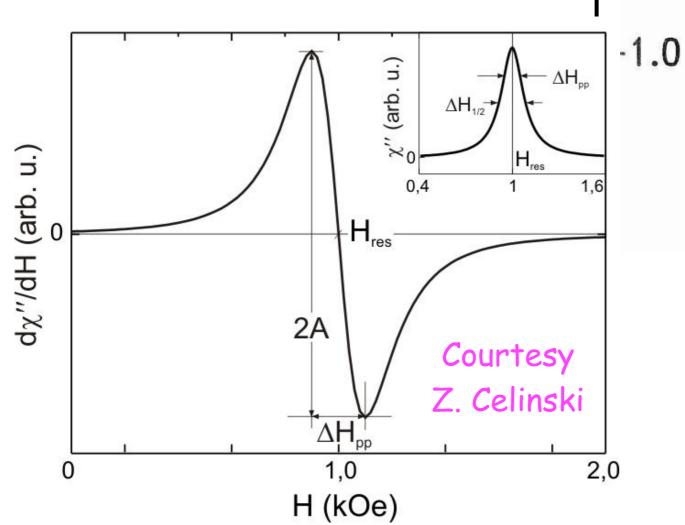


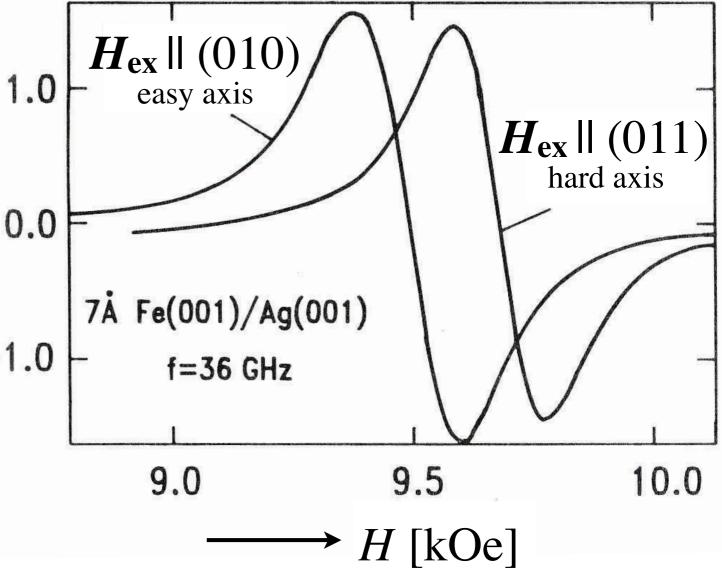


Ferromagnetic Resonance (FMR)

 $\mathrm{d}I/\mathrm{d}H_{\mathrm{ex}}$

- Resonance field $H_{\rm res}$ and half power line width ΔH can be determined
- $H_{\rm res} \rightarrow$ magnetic anisotropy
- $\Delta H \rightarrow \text{relaxation}$
- Intensity $\rightarrow M_{\rm s}$





B. Heinrich et al., PRL **59**, 1756 (1987)

Spinwave Resonance
Light Scattering experiments

Spinwave Resonance

Light Scattering experiments

-> Lecture of B. Hillebrands

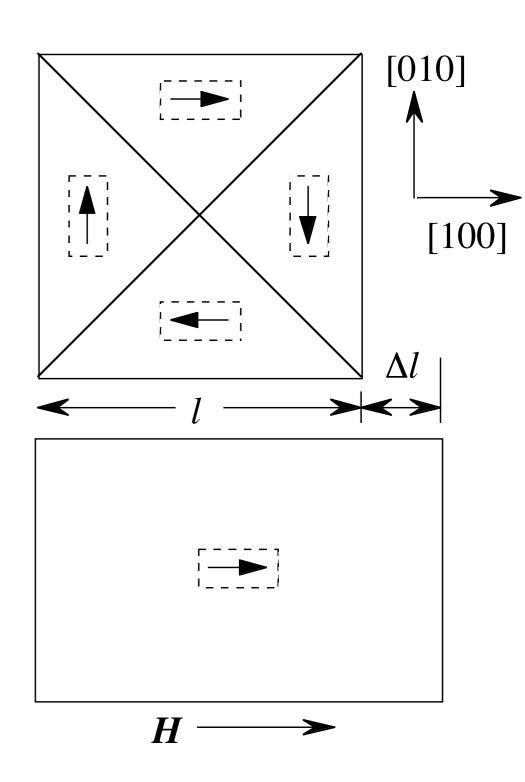
3.

Magnetic Measurements to determine material parameters & properties

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

Magnetostriction

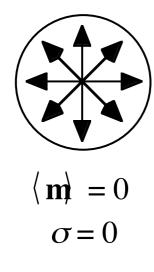
- Example: cubic crystal (iron) with 4 domain phases in ground state \rightarrow no net-magnetization
- Each domain elongates crystal along M-direction
 → cubic lattice gets tetragonally distorted
- Application of magnetic field, saturation \rightarrow elongation of total crystal
- Relative length change $\Delta l / l = \lambda_s$ $\lambda_s =$ magnetostriction coefficient
- $\lambda_s > 0$: elongation in magnetization direction, $\lambda_s < 0$: compression
- Note: 180°-domains are elongated along same axis
- λ for iron: 20·10⁻⁶ \rightarrow very small effect

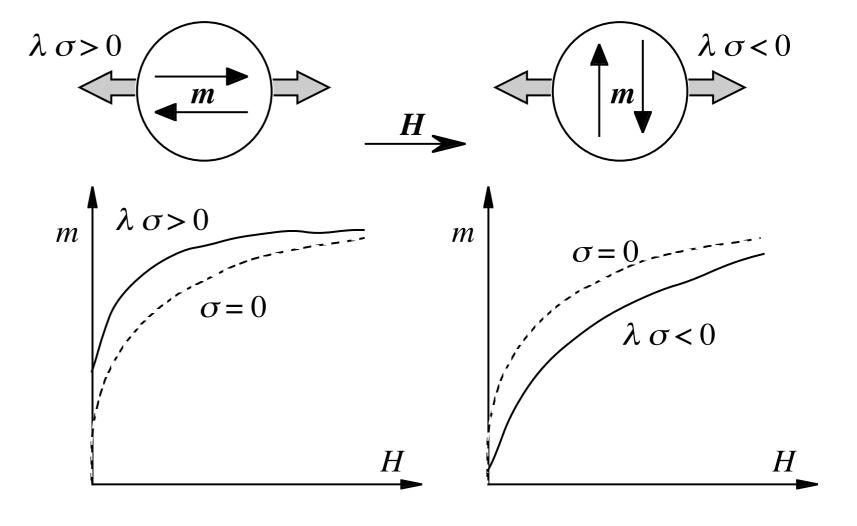


Magnetostriction measurement

- Saturation magnetostriction constants can be determined both directly or indirectly:
 - Indirect methods: stress sensitivity of a suitable magnetic property is analysed, more suitable for thin films and wires

Example: magnetization curve and resonance measurements, if performed as function of external stress, can be evaluated in terms of magneto-elastic coefficients



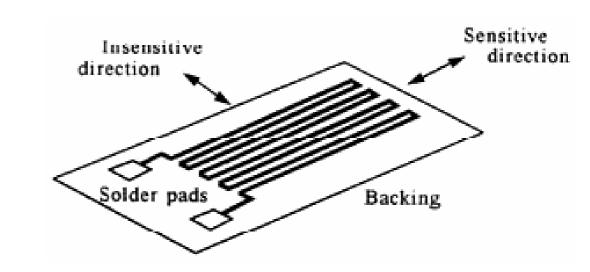


Magnetostriction measurement

- Saturation magnetostriction constants can be determined both directly or indirectly:
 - Direct measurements: evaluate elongation of a magnet depending on the magnetization direction, preferred for bulk samples of sufficient size

Strain Gauges

- · Plastic foil on which structured metal films act as sensors, cemented on sample
- Based on (small) change of el. resistance by elongation, measured with bridge circuit
- Strain gauge can be applied locally on favourable small region of single crystal or even on grain in a coarse-grained sample. Active area down to 1 mm²
- It is always advisable to apply strain gauges on both sides of sample, and to connect them in series to avoid influence from sample bending induced by one-sided heating by the measuring current

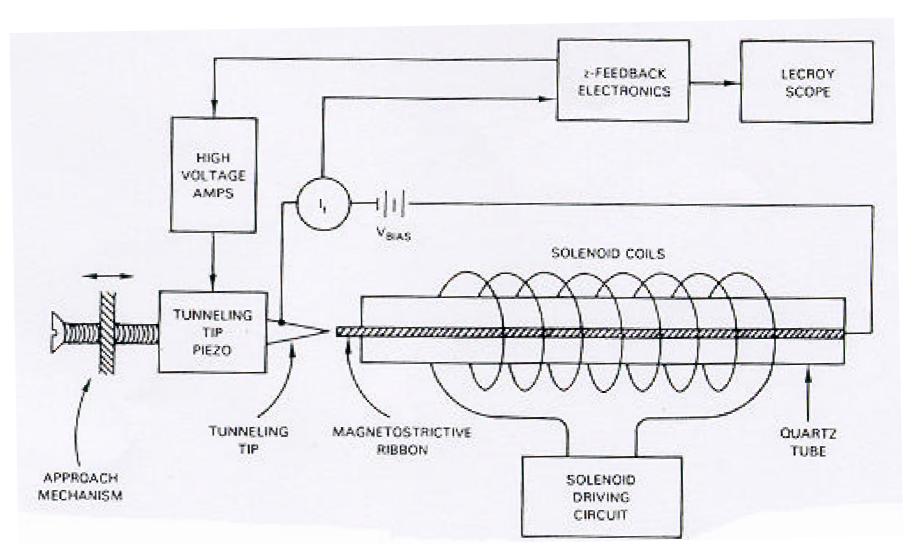


Magnetostriction measurement

- Saturation magnetostriction constants can be determined both directly or indirectly:
 - Direct measurements: evaluate elongation of a magnet depending on the magnetization direction, preferred for bulk samples of sufficient size

Dilatometers

- Capacitive sensors, optical interferometers, tunnelling sensor, piezo sensor...
- With normal samples
 of centimetre
 dimension a
 resolution in the
 nanometre range is
 required



Magnetostriction measurement

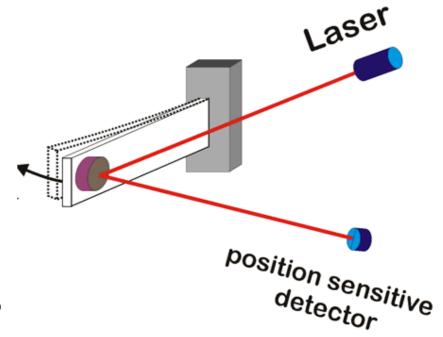
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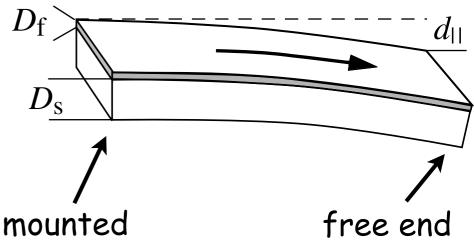
Cantilever for films

- Magnetostrictive bending of a sample-substratecomposite in magnetic field is optically detected as measuring signal by reflected laser beam, a quadrant detector and lock-in technique
- Sample esposed to rotating saturation field
- Deflection difference $d_{
 m f}$ of free end of cantilever for longitudinal and transverse magnetization:

$$d_{\rm f} = d_{\parallel} - d_{\perp} = \frac{3D_{\rm f}L^2}{D_{\rm s}^2} \frac{E_{\rm f}(1+\nu_{\rm s})}{E_{\rm s}(1+\nu_{\rm f})} \cdot \frac{3}{2}\lambda_{\rm s}\sin^2\vartheta$$

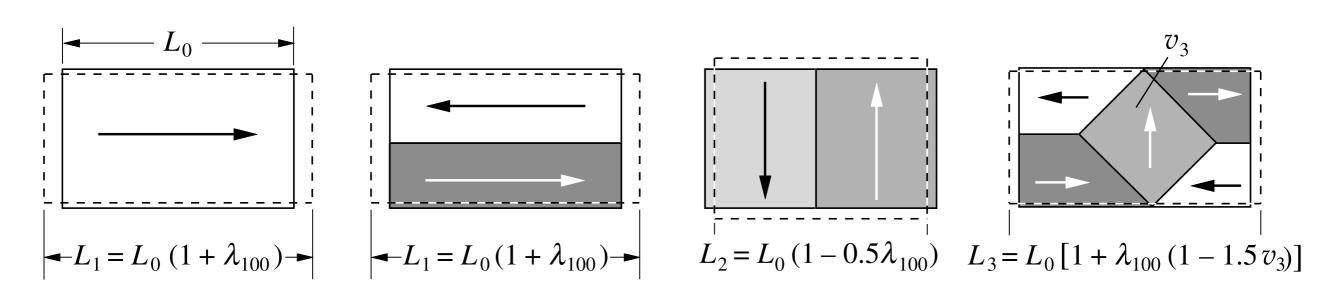
 $E_{\rm x}$ and $\nu_{\rm x}$: Young's moduli and Poisson's ratios of film and substrate, θ : magnetization angle ($\theta=0$ for magnetization along cantilever)





Magnetostriction measurement, remark

 Every direct determination of magnetostriction constant requires measurement of length change between two different saturated states — usually parallel and perpendicular to measuring direction. Experiment with field applied along only one axis of crystal yields no useful information on magnetostriction constants, because then only some arbitrary demagnetized state and the saturated states are compared



3.

Magnetic Measurements to determine material parameters & properties

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

3.5 Domain Methods

Principle:

Under favourable circumstances material constants may be derived directly from observed domains. Such approach requires an equilibrium situation for which a reliable theoretical treatment is possible.

To qualify as suitable domain structure for quantitative evaluation, a pattern must fulfil a number of requirements:

- It must be sufficiently simple to permit a complete analysis.
- It must contain at least one feature (such as an angle or a characteristic length) which can reach its optimum value independent of its environment.
- This feature must be sensitive to an interesting material parameter.

3.5 Domain Methods

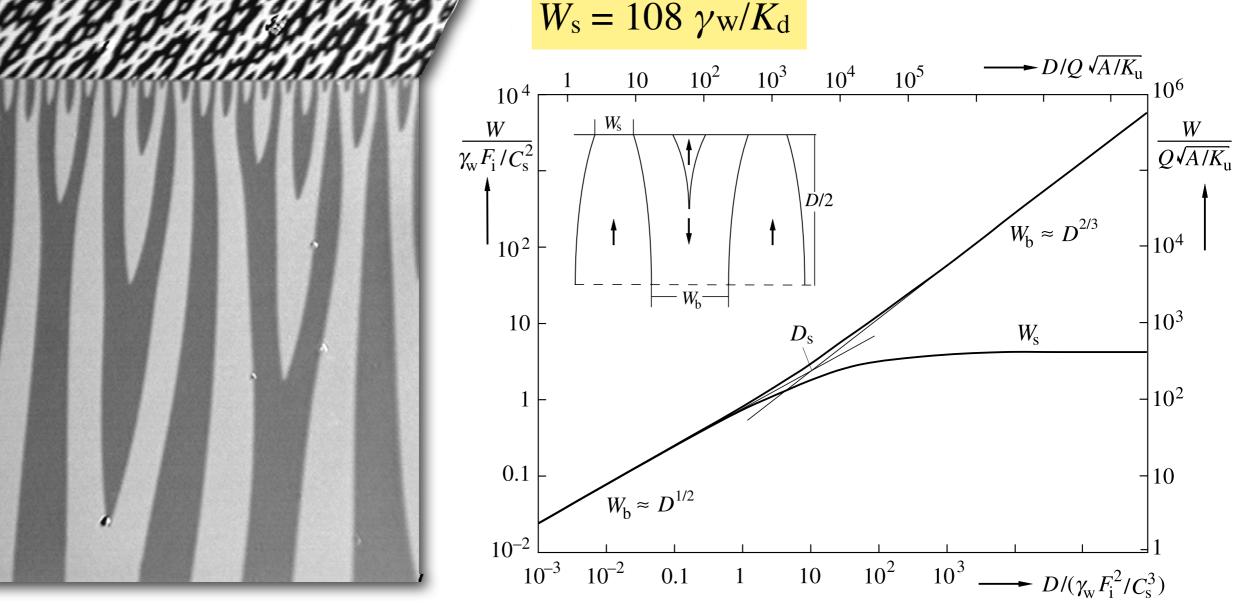
Example: Surface domain width in bulk uniaxial crystals

NdFeB, top- and side views

20 μm

For sufficiently thick crystals: surface domain width $W_{\rm s}$ constant, independent of sample dimensions, depends only on wall energy γ_{W} and stray field energy constant $K_d = \mu_0 M_S^2/2$:

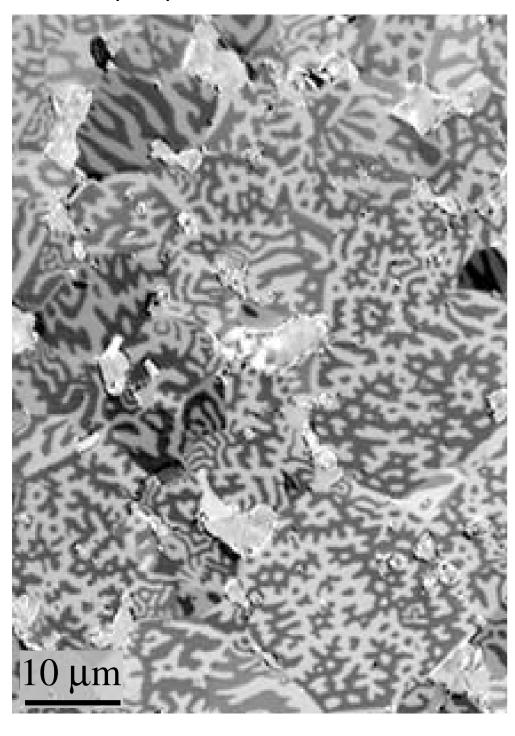
$$W_{\rm s} = 108 \ \gamma_{\rm W}/K_{\rm d}$$



3.5 Domain Methods

Example: Surface domain width in bulk uniaxial crystals

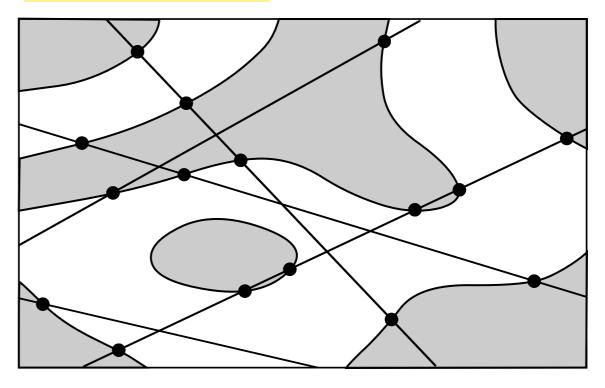
NdFeB magnet, c-axis perpendicular



For sufficiently thick crystals: surface domain width $W_{\rm s}$ constant, independent of sample dimensions, depends only on wall energy $\gamma_{\rm W}$ and stray field energy constant $K_{\rm d} = \mu_0 \, M_{\rm S}^2 \, / 2$:

$$W_{\rm s} = 108 \ \gamma_{\rm W}/K_{\rm d}$$

$$\gamma w = \pi \sqrt{A/K_u}$$

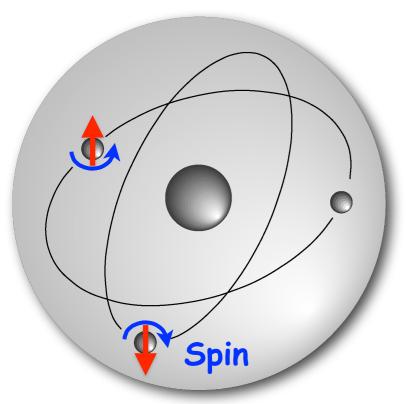


$$\frac{\text{Domain}}{\text{width}} = \frac{2 \cdot \text{Total test line length}}{\pi \cdot \text{Number of intersections}}$$

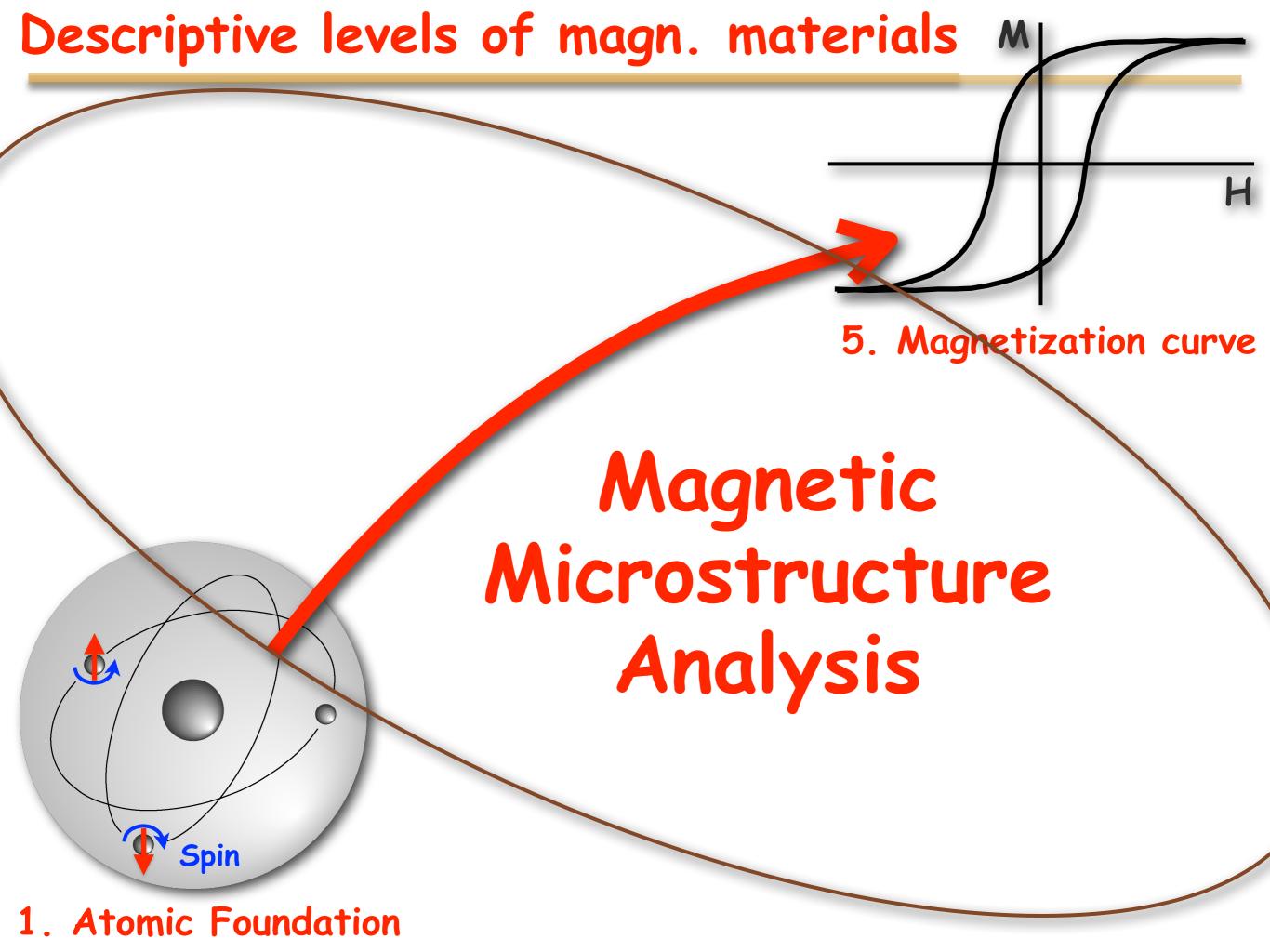
4.
Domain scale
measurements
(Magnetic Imaging)

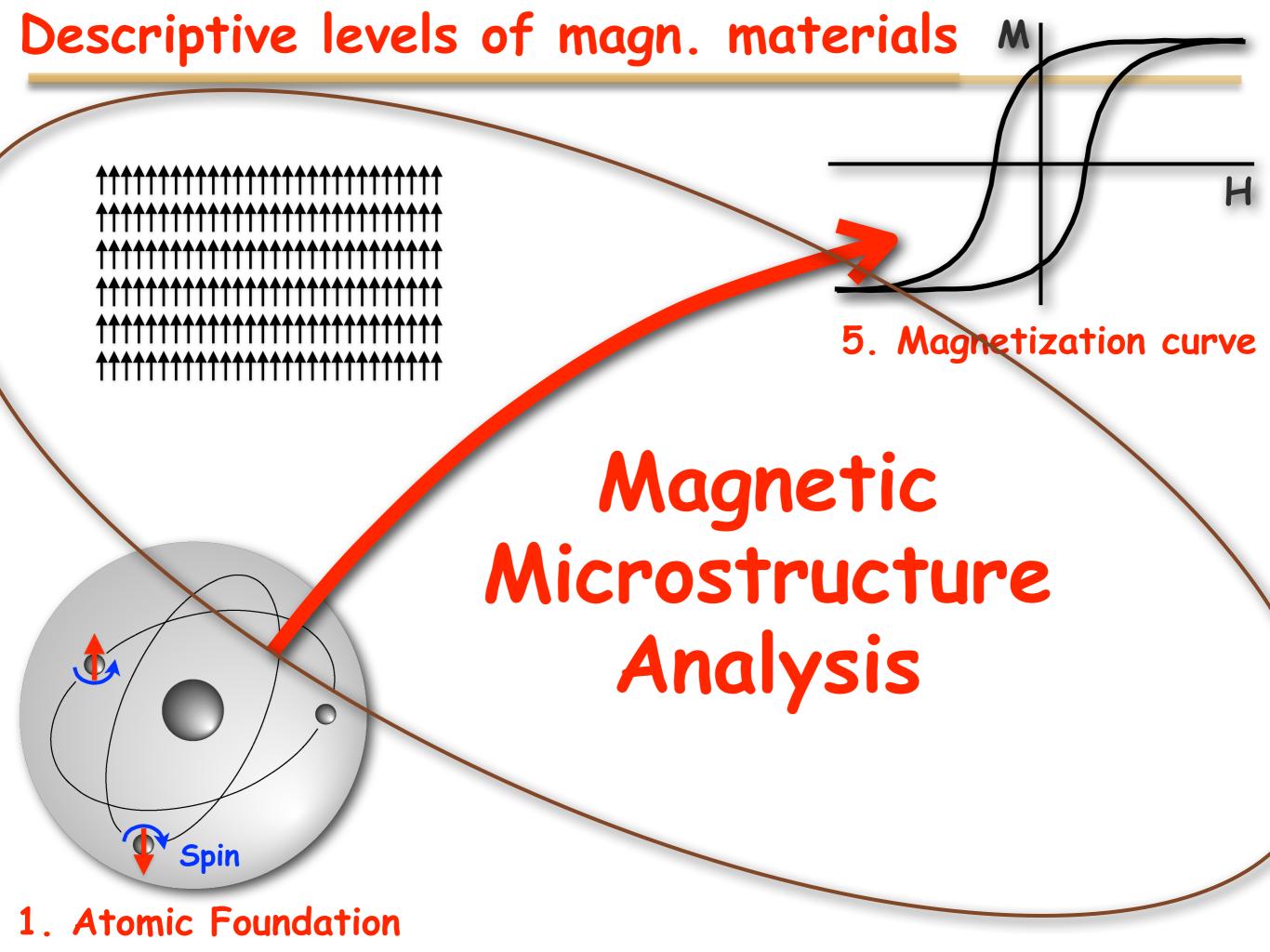
Descriptive levels of magn. materials M

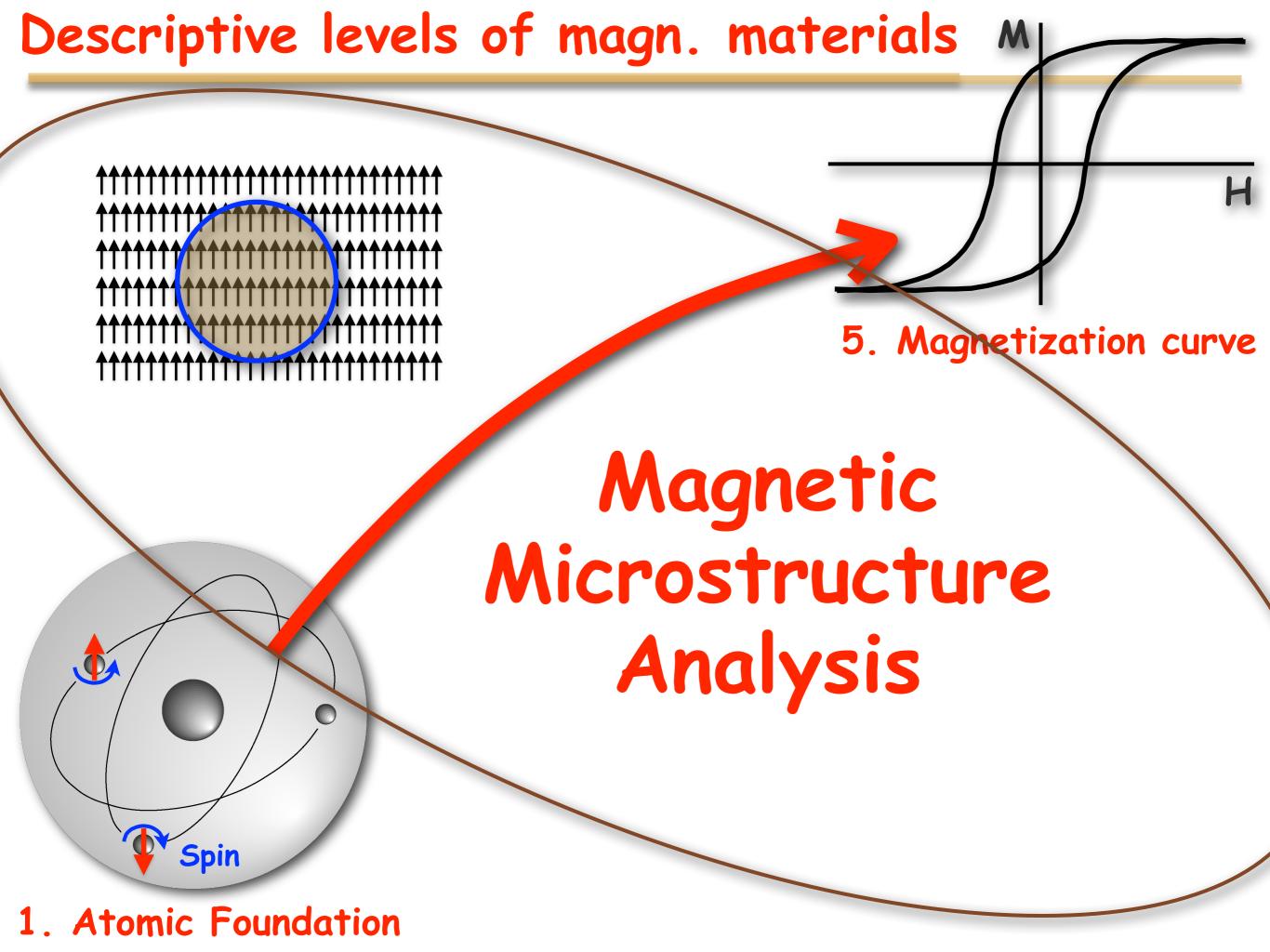
5. Magnetization curve

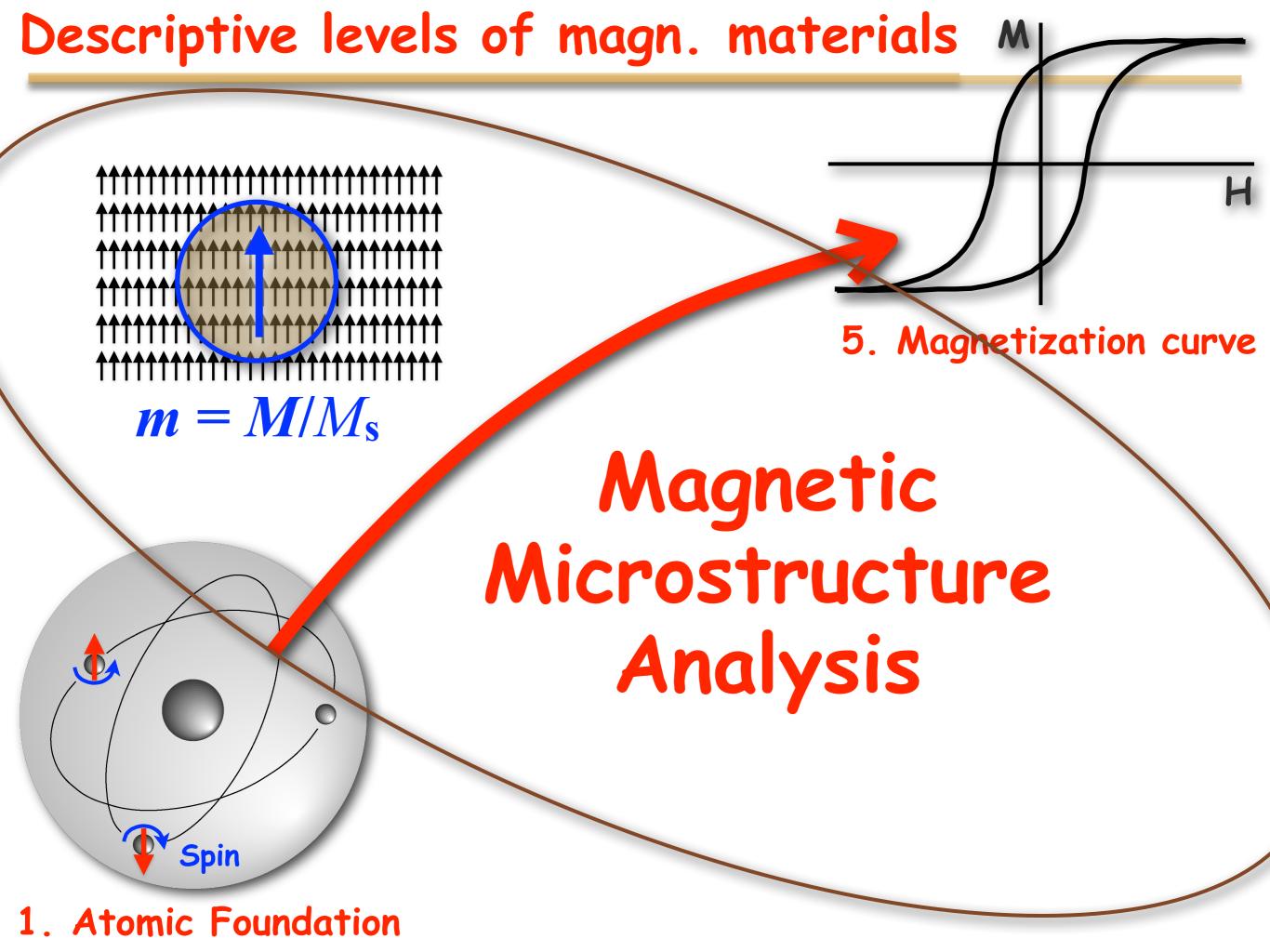


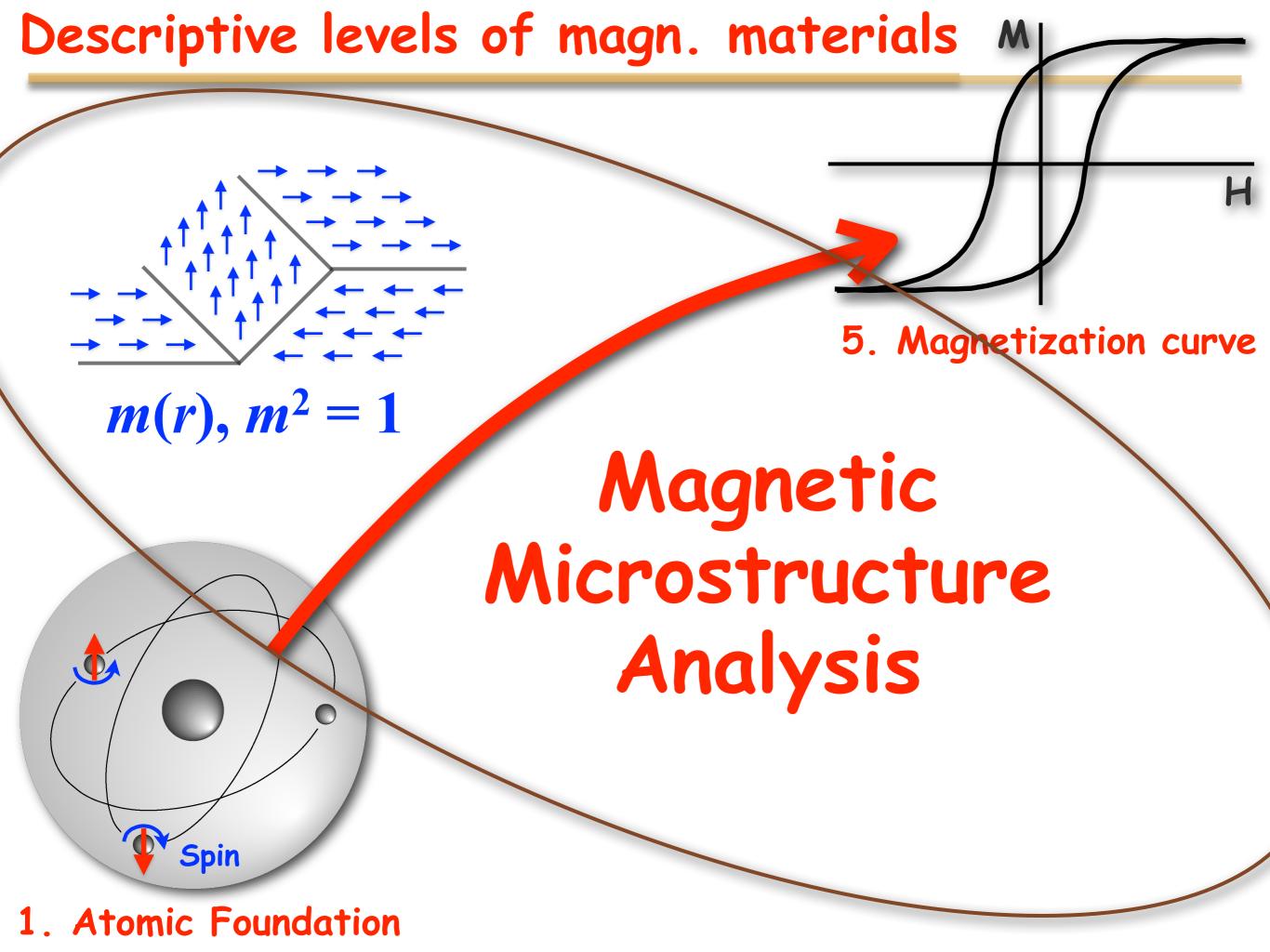
1. Atomic Foundation

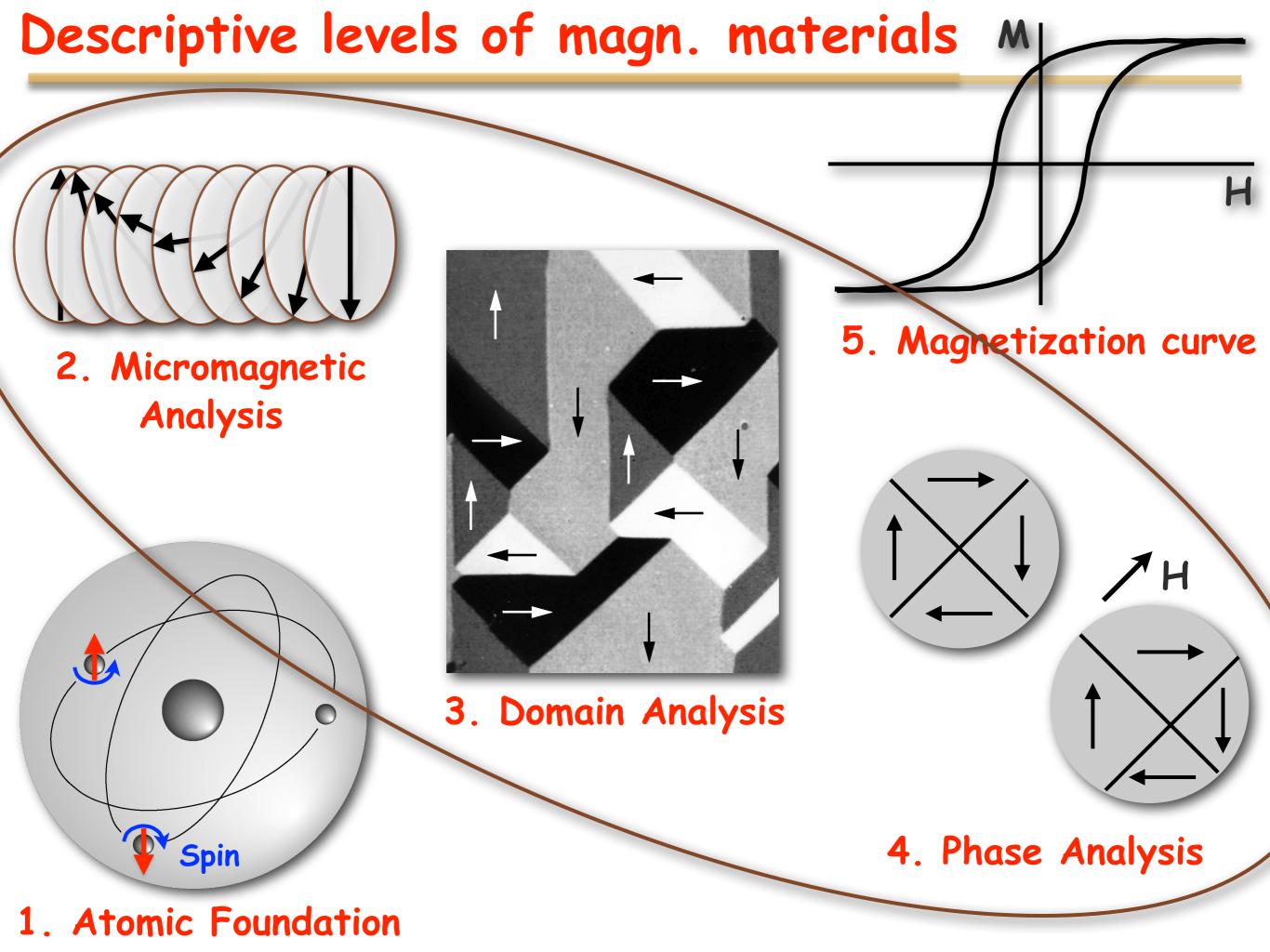












Sensitivity of imaging methods

$$\mathbf{B} = \mu_0 (\mathbf{H} + \mathbf{M})$$
 $(\mathbf{H} = \mathbf{H}_{ext} + \mathbf{H}_{stray})$
 $\operatorname{div} \mathbf{B} = 0$
 $\operatorname{div} \mathbf{H}_{stray} = -\operatorname{div} \mathbf{M}$

• Sensitive to H_{stray}

- Bitter technique
- Magnetic force microscopy
- Hall probe microscopy

Sensitive to M

- Magneto-optical microscopy
- X-ray spectroscopy
- Polarized electrons (SEMPA, SPT)

· Sensitive to B

- Transmission electron microscopy

Sensitive to distortions

- X-ray, neutron scattering

Sensitivity of imaging methods

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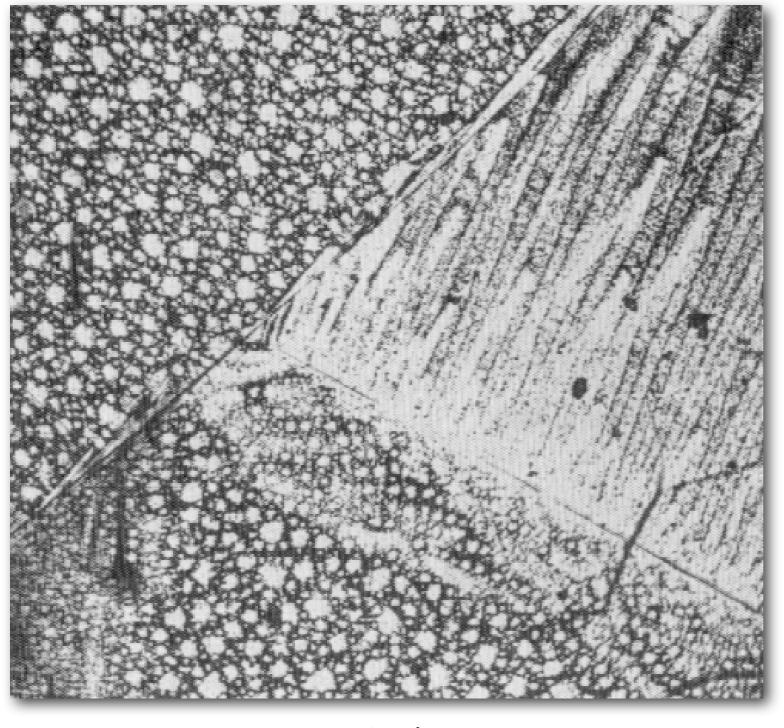
Sensitive to H_{stray}

· Sensitive to M

- Sensitive to B
- Sensitive to distortions

- 1. Bitter technique
- 2. Magnetic force microscopy
- 3. Hall probe microscopy
- Magneto-optical microscopy
- X-ray spectroscopy
- Polarized electrons (SEMPA, SPT)
- Transmission electron microscopy
- X-ray, neutron scattering

History: first imaging of domains by F. Bitter, 1931)

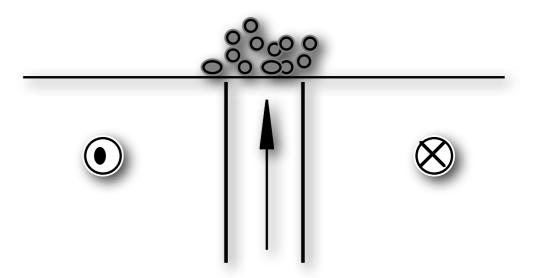




Cobalt FeSi

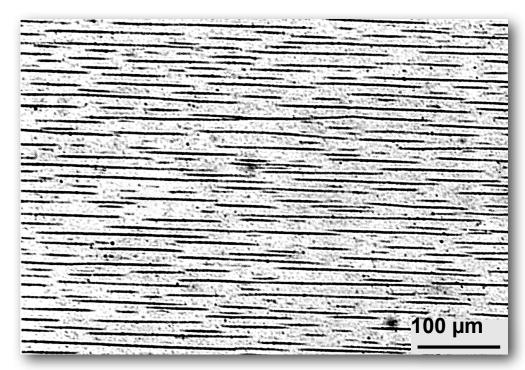
Principle

- · Magnetic colloid: Magnetite particles (diameter about 10 nm) in water
- · Accumulation in stray field at sample surface



Sensitivity

- Reversible agglomeration in weak magnetic field
 - → Increase of volume, elongated shape
 - → Large susceptibility
 - → Large sensitivity to stray fields in order of a few 100 A/m

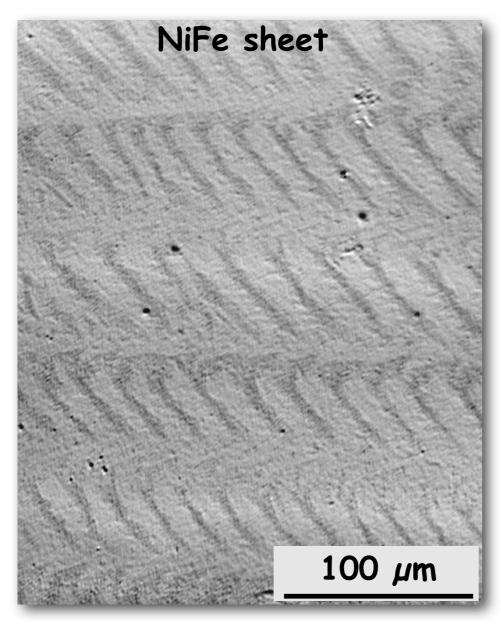


Agglomeration in magnetic field (560 A/m)

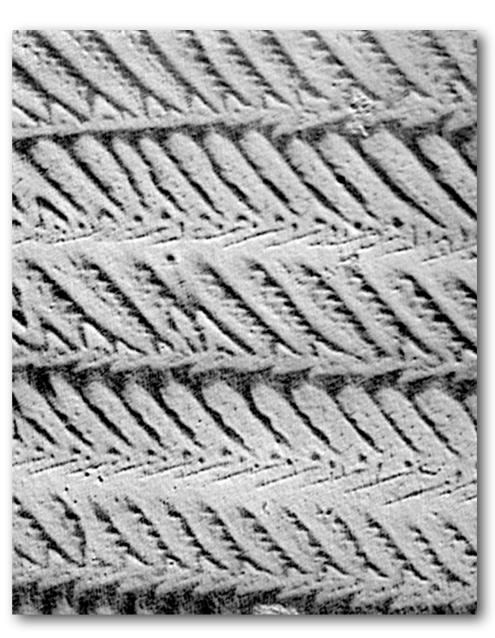
Sensitivity

Increase of sensitivity in weak perpendicular field

→ Domain imaging in soft magnetic materials



Without auxiliary field



With perpendicular field

● 1.5 kA/m

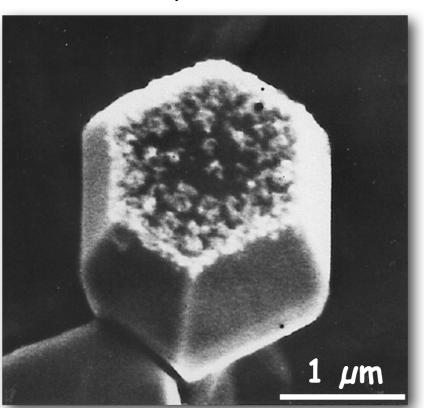
Dry colloid technique

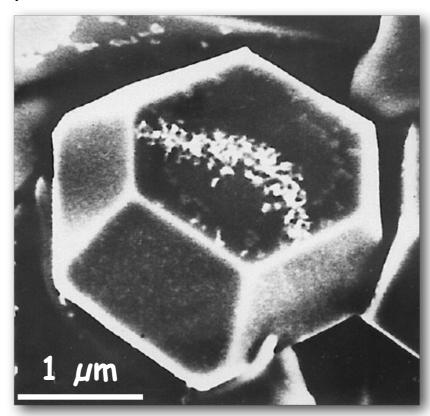
Allowing colloid to dry on surface

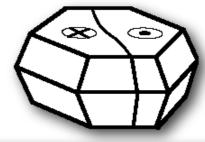
Adding agent

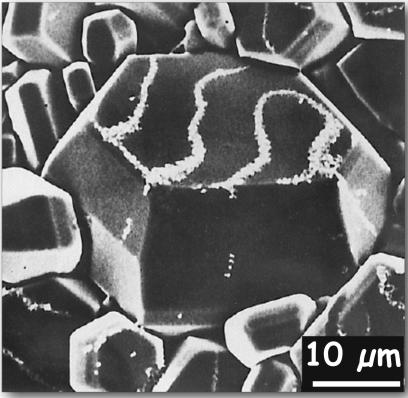
- → Strippable film
- → Imaging in electron microscope

Ba-Ferrite particles (courtesy K. Goto, Sendai)









Dry colloid technique:

Static domain observation on rough, 3-dimensional surfaces at high resolution of some 10 nm

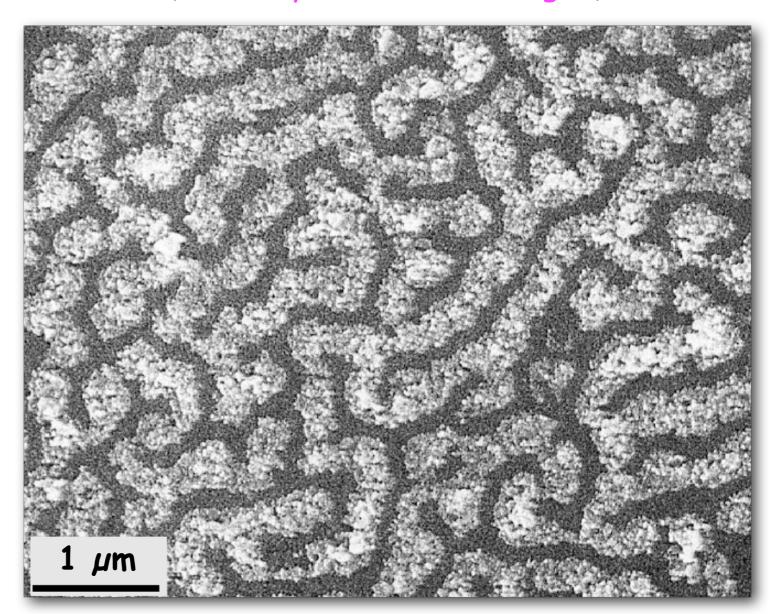
Dry colloid technique

Allowing colloid to dry on surface Adding agent

- → Strippable film
- → Imaging in electron microscope

CoCr recording medium

(courtesy J. Simsová, Prague)

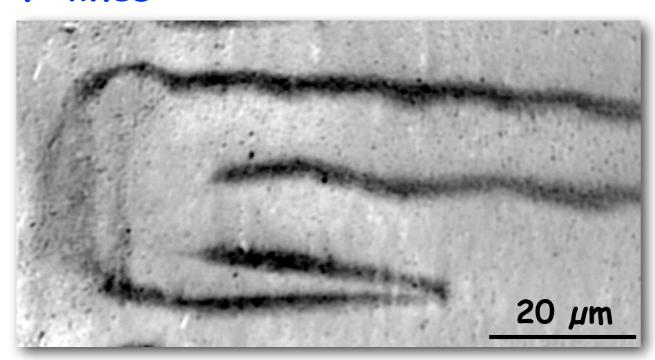


Dry colloid technique:

Static domain observation on rough, 3-dimensional surfaces at high resolution of some 10 nm

V-lines

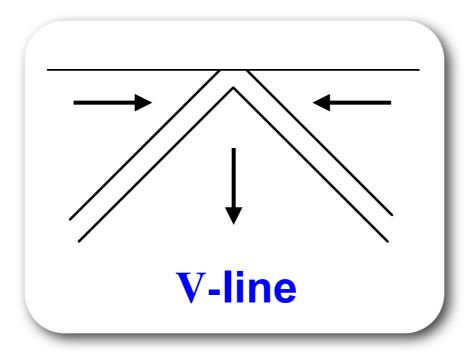
Visible and invisible features



V-line

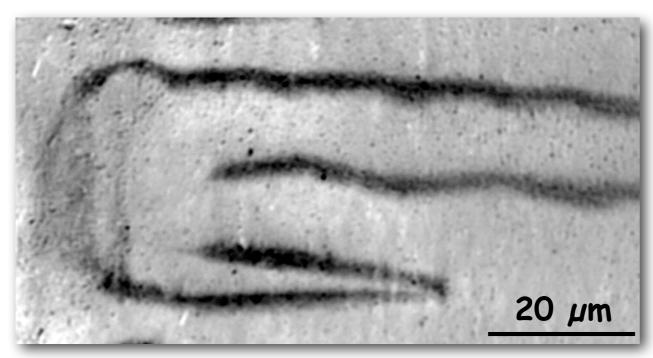
Bitter image

Kerr image



V-lines

Visible and invisible features

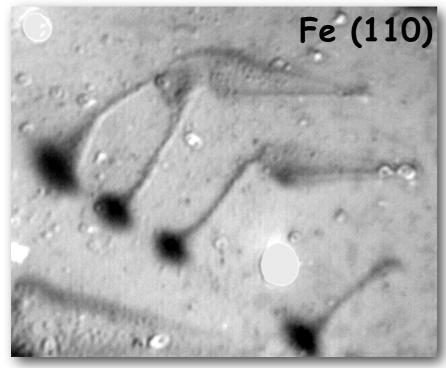


V-line

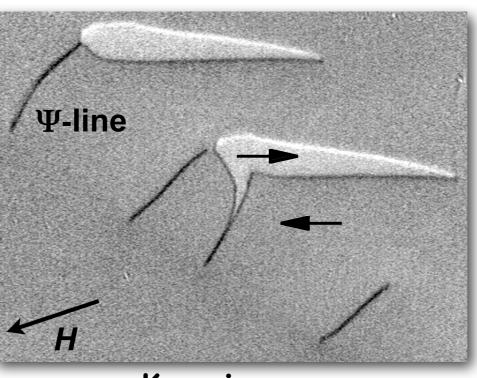
Bitter image

Kerr image

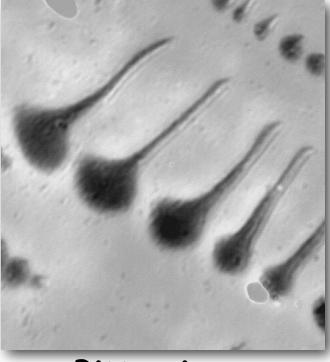
Ψ -lines



Bitter image

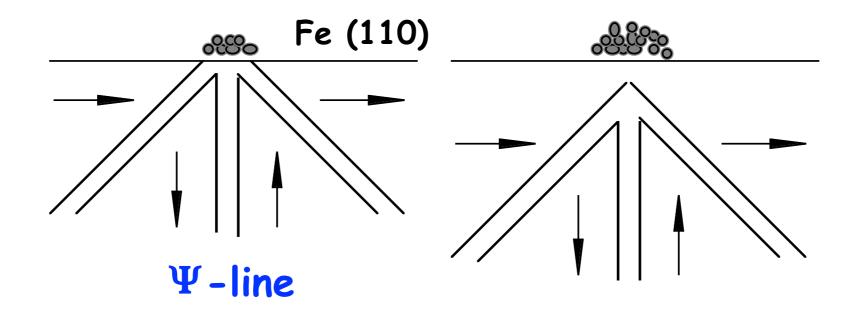


Kerr image

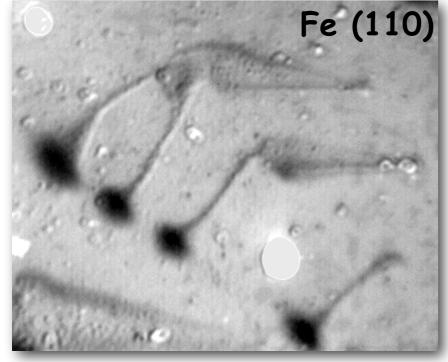


Bitter image

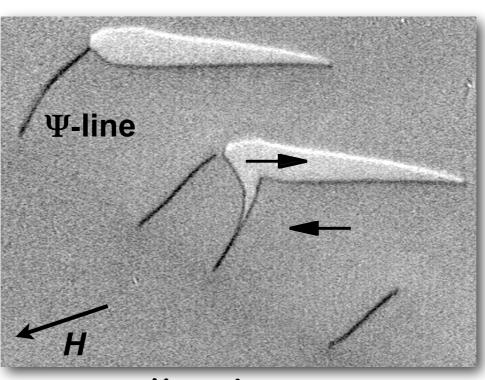
Visible and invisible features



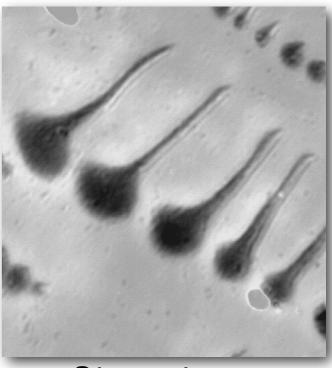
Ψ -lines



Bitter image



Kerr image



Bitter image

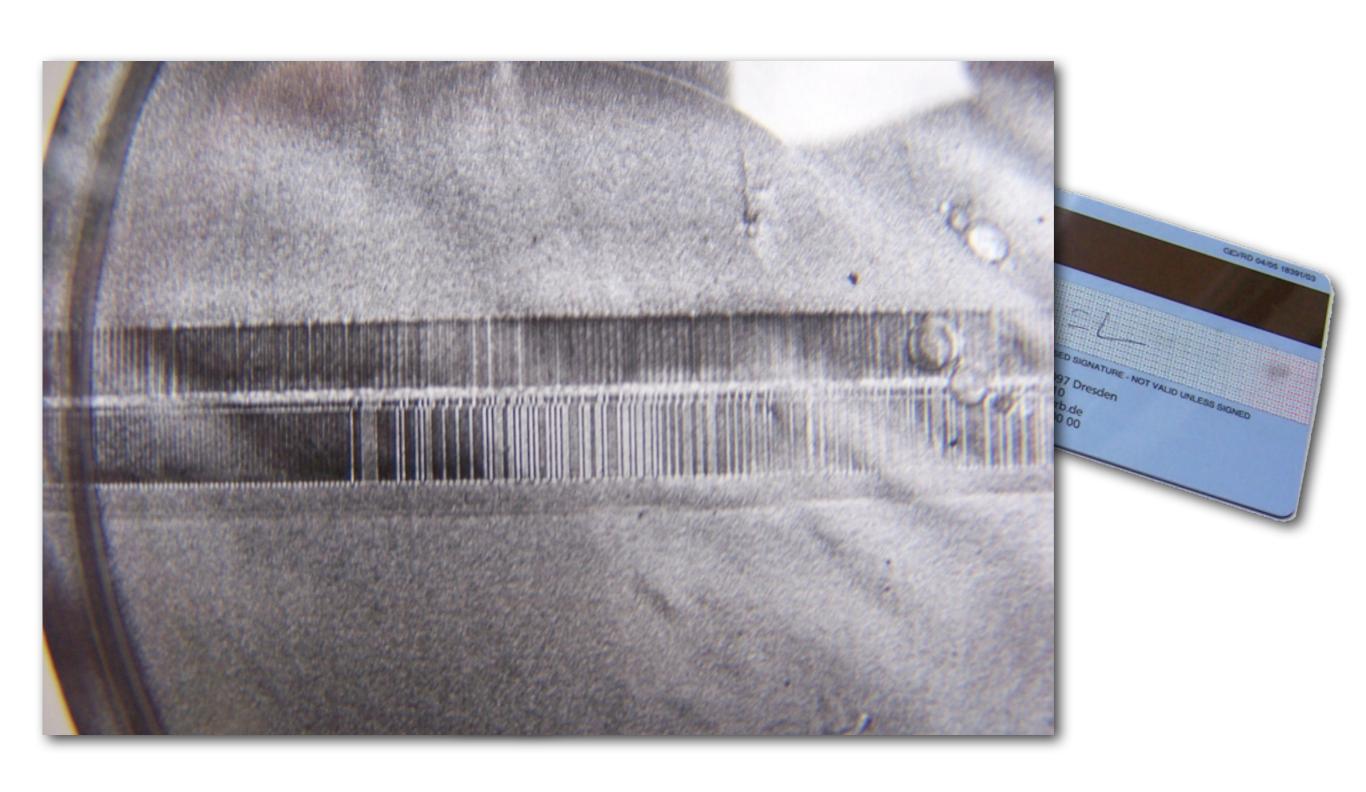
Toner powder emulsion

Laser printer toner + water + household detergent



Toner powder emulsion

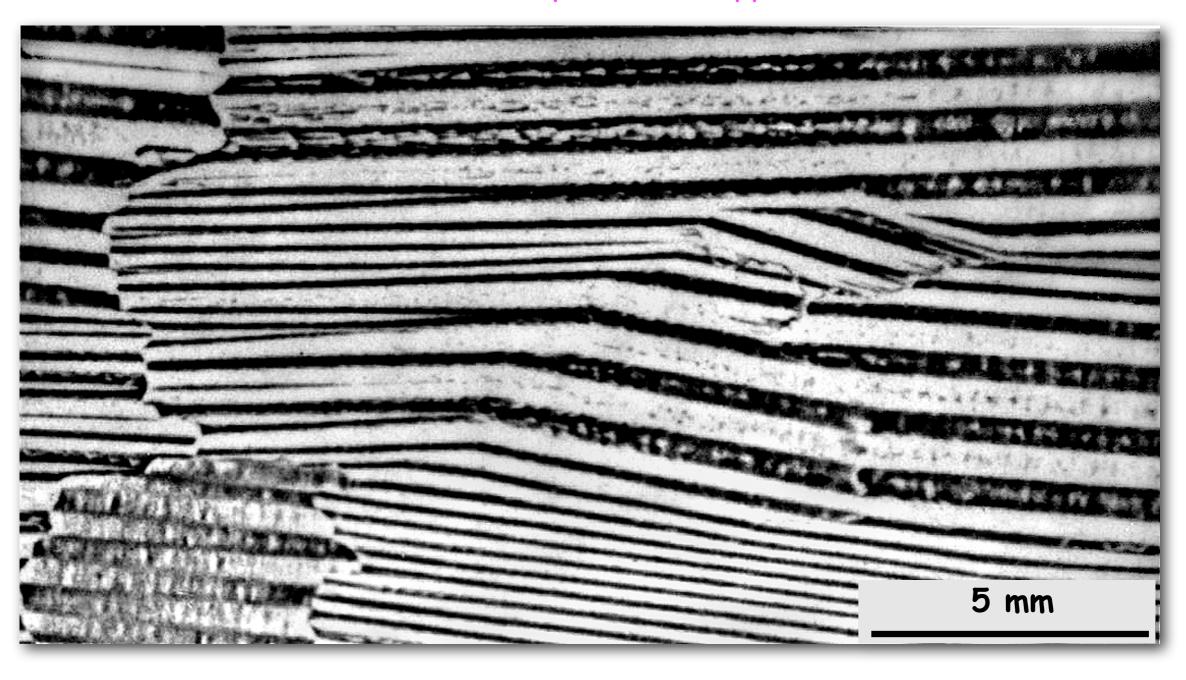
Laser printer toner + water + household detergent



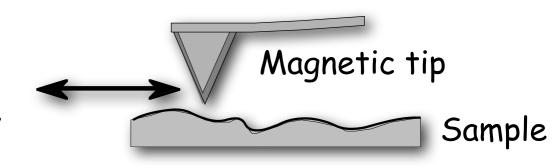
Toner powder emulsion

Laser printer toner + water + household detergent

Transformer steel (courtesy S. Arai, Nippon steel)



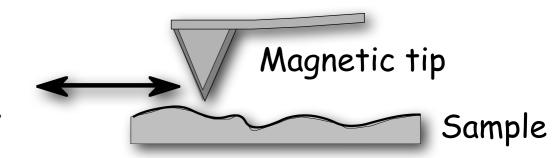
- Spin-off of scanning tunnelling microscope
- Tip-shaped probe at free end of cantilever
 (= flexible beam). Tip position detected (e.g.) by
 optical interference between tip of a fibre and
 cantilever



2 modes:

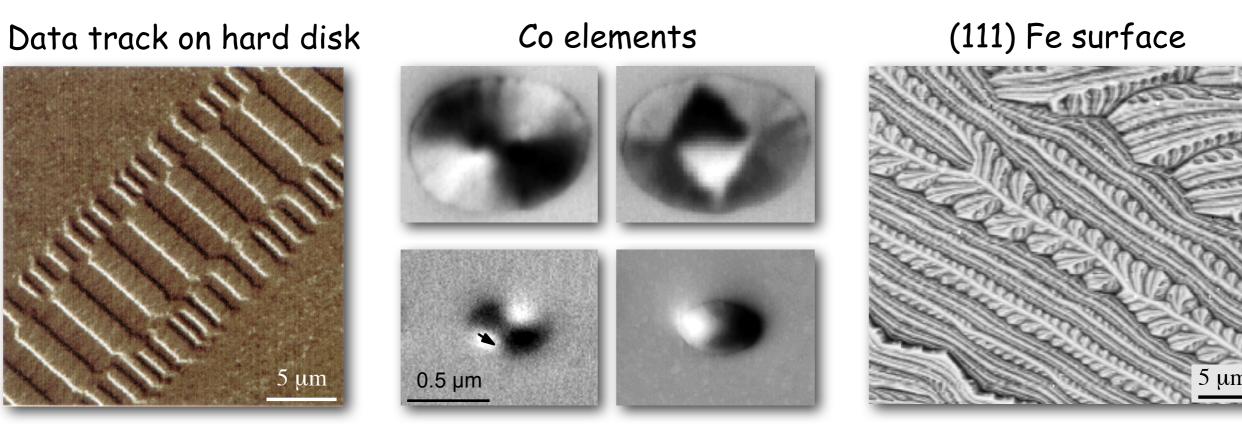
- Static mode: MFM is run at constant force (equivalent to constant deflection of the cantilever) and the height necessary to obtain this state is used as the imaging information
- Dynamic mode: Cantilever is operated at frequency close to its mechanical resonance, and change in resonance amplitude or shift in phase due to stray field interaction are detected. Since a magnetic force gradient is equivalent to an additional contribution to the spring constant of the cantilever, profiles of constant force gradient are recorded this way

- · Spin-off of scanning tunnelling microscope
- Tip-shaped probe at free end of cantilever
 (= flexible beam). Tip position detected (e.g.) by
 optical interference between tip of a fibre and
 cantilever



Courtesy: J. Miltat

- 2 modes:
 - Static mode: MFM is run at constant force (equivalent to constant deflection of



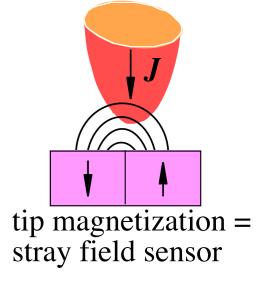
Courtesy: A. Fernandez

Conventional interpretation of MFM: $F = -\partial E_{\text{inter}}/\partial z$; $\partial F/\partial z = -\partial E_{\text{inter}}^2/\partial z^2$

$$E_{\text{inter}} = -\int_{\text{tip}} \mathbf{J}_{\text{tip}} \cdot \mathbf{H}_{\text{sample}} dV = -\int_{\text{sample}} \mathbf{J}_{\text{sample}} \cdot \mathbf{H}_{\text{tip}} dV$$

$$H_{\text{tip}} = -\operatorname{grad} \bar{\Phi}_{\text{tip}}$$
, partial integration

$$\Phi_{\text{tip}}$$
 = tip potential



Alternative interpretation *Hubert, Rave, Tomlinson:* Phys. Stat. Sol. B204, 817 (1997)

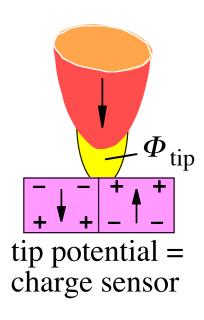
$$E_{\text{inter}} = \int_{\text{sample}}^{\sigma_{\text{sample}}} \Phi_{\text{tip}} dS + \int_{\text{sample}}^{\rho_{\text{sample}}} \Phi_{\text{tip}} dV$$
surface sample

$$O_{\text{sample}} = n \cdot J_{\text{sample}}$$
 (surface charge)

$$\rho_{\text{sample}} = -\operatorname{div} \boldsymbol{J}_{\text{sample}}$$
 (volume charge)

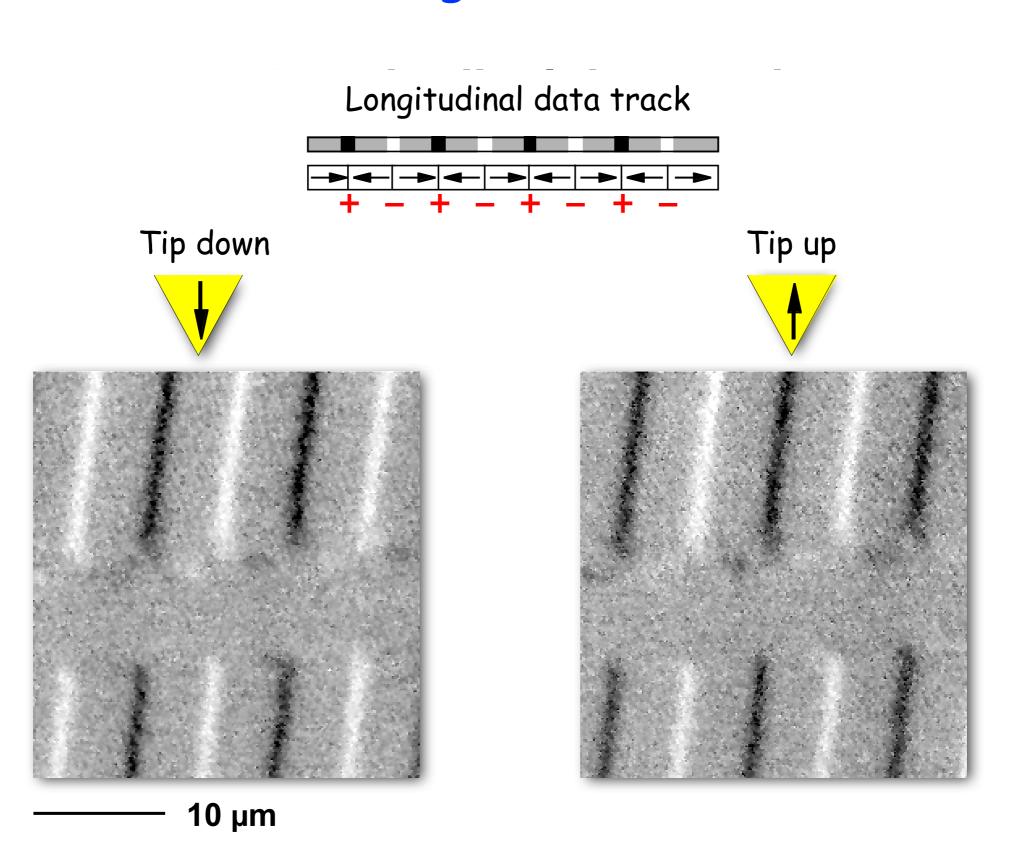
Force
$$F = -\frac{\partial E_{\text{inter}}}{\partial z} = -\int (\frac{\partial \sigma}{\partial z} \Phi + \sigma \frac{\partial \Phi}{\partial z}) dS - \int (\frac{\partial \rho}{\partial z} \Phi + \rho \frac{\partial \Phi}{\partial z}) dV$$
for weak interaction
$$\approx -\int \sigma \frac{\partial \Phi}{\partial z} dS - \int \rho \frac{\partial \Phi}{\partial z} dV$$

Force gradient
$$\frac{\partial F}{\partial z} = -\frac{\partial E_{\text{inter}}^2}{\partial z^2} \approx -\int \sigma \frac{\partial^2 \Phi}{\partial z^2} dS - \int \rho \frac{\partial^2 \Phi}{\partial z^2} dV$$



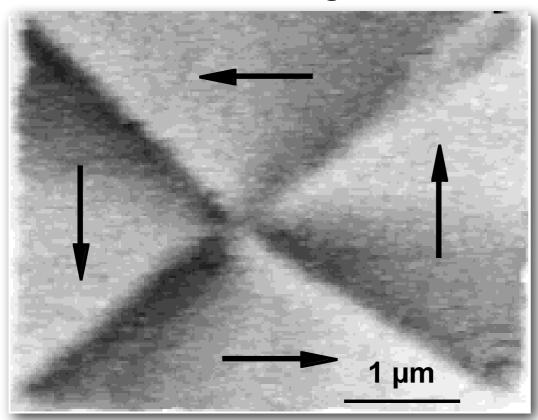
In the limit of weak interaction: MFM is Charge Microscopy

Charge contrast

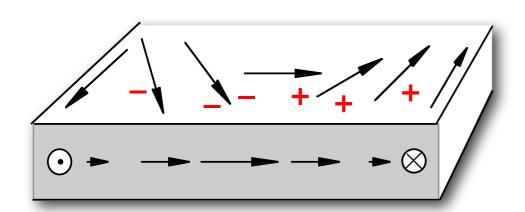


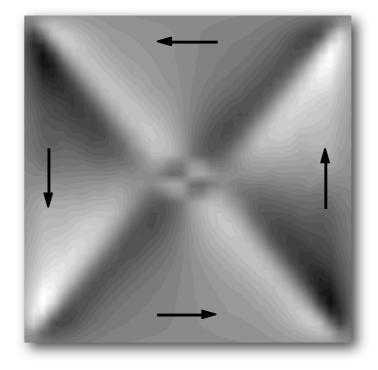
Charge contrast

MFM image

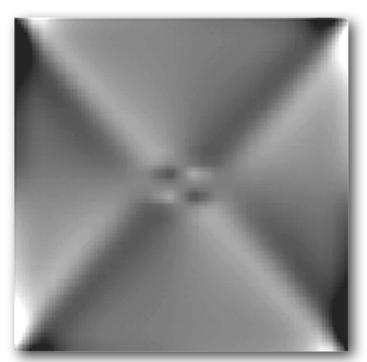


FeTnN element (30 nm) (courtesy J. Miltat)





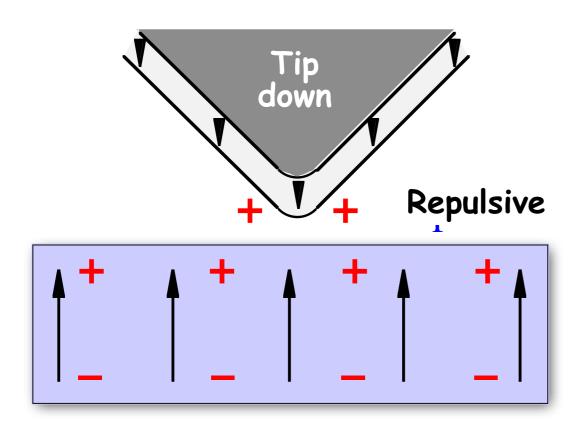
Simulated MFM image

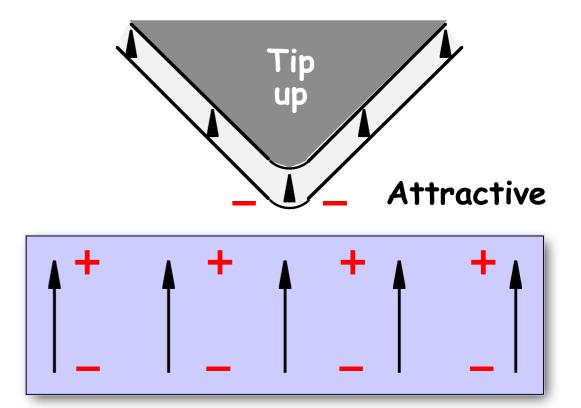


Simulated charge distribution

A. Hubert, W. Rave, S. Tomlinson: Phys. Stat. Sol. B 204, 817 (1997)

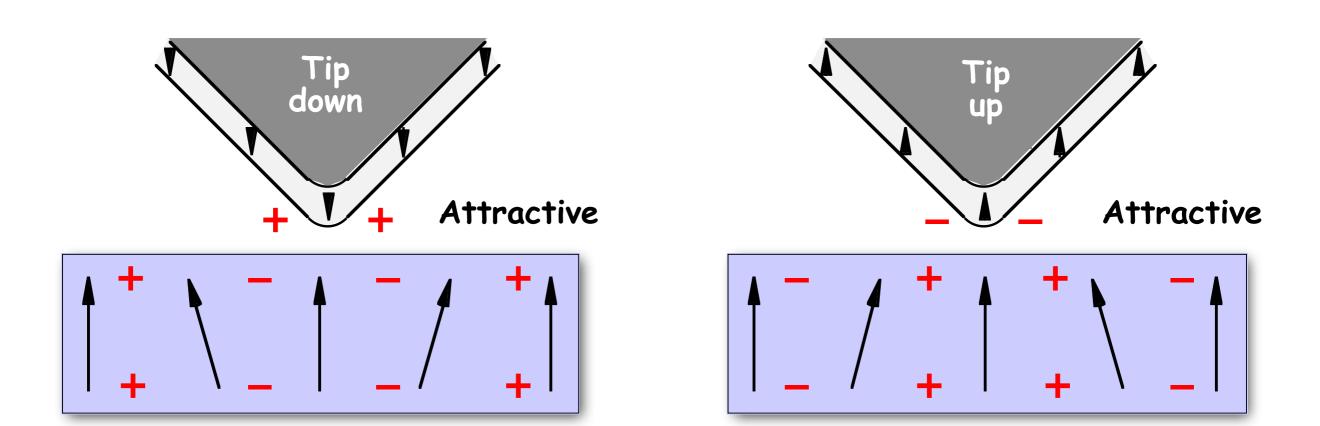
Charge contrast





Charge contrast is inverted when tip polarity is inverted

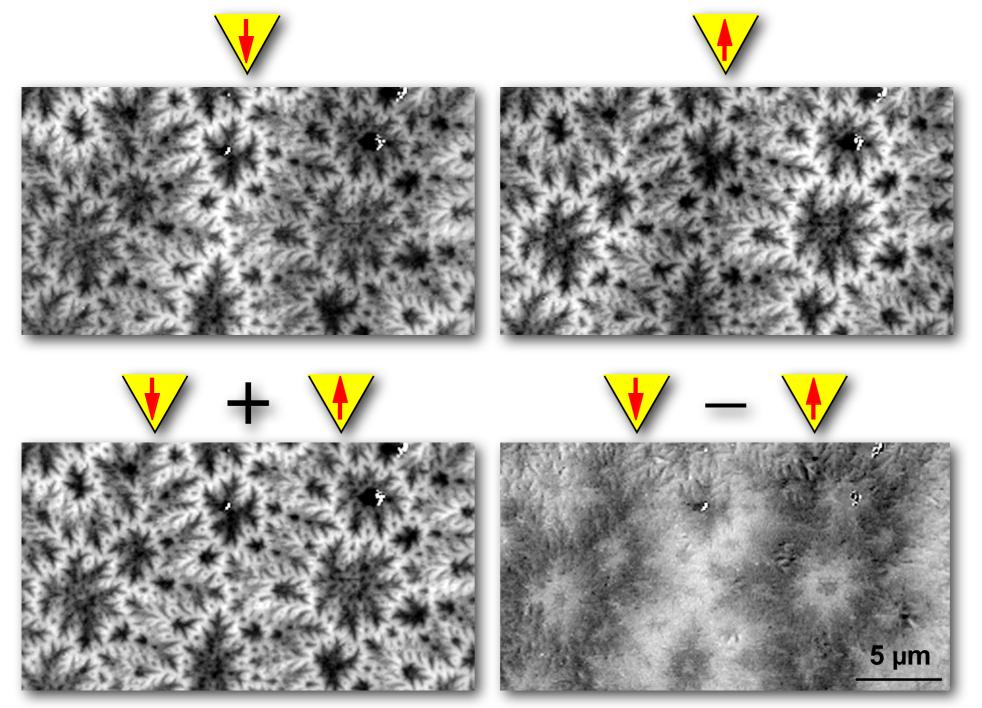
Induced charges: susceptibility contrast



- → Tip induces charges of opposite polarity in each case
- → Always attractive interaction (independent of tip polarity)
- → Strength of attraction depends on local susceptibility

Charge & susceptibility contrast

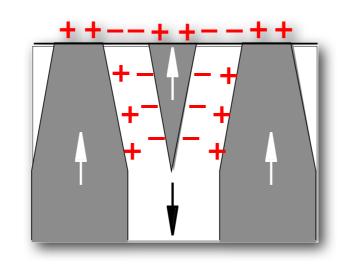
- · Charge contrast in inverted by inversion of tip magnetization,
- Susceptibility contrast: not inverted
- $\cdot \rightarrow$ Separation of charge and susceptibility contrast by difference and sum images



Co crystal

Charge & susceptibility contrast

E. Zueco et al.: JMMM 190, 42 (1998)







Weaker attraction





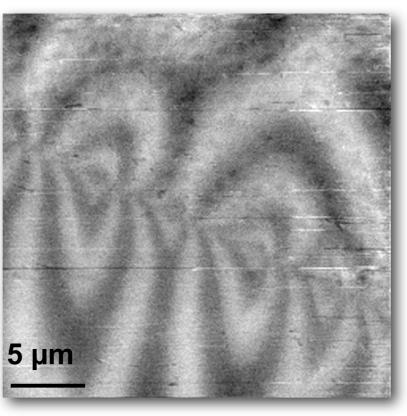




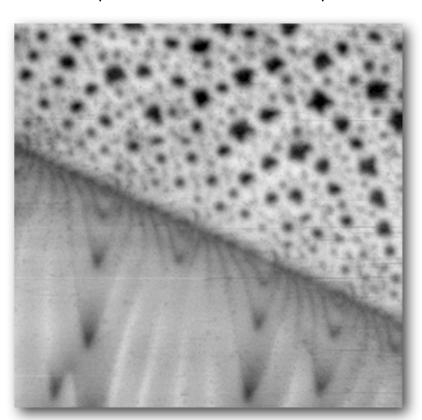
NdFeB twin boundary



Kerr image



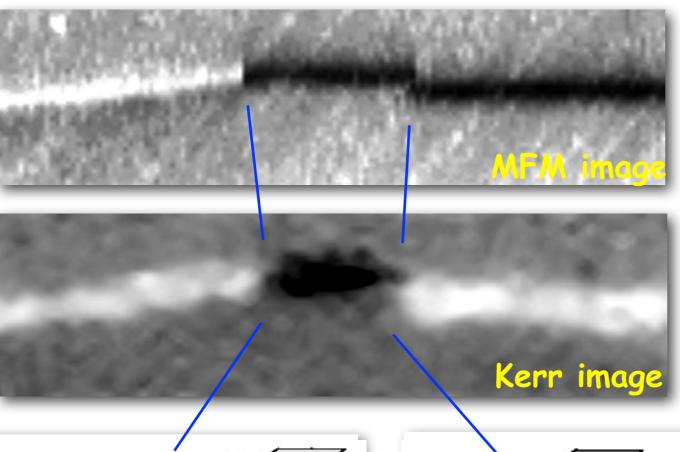
MFM: charge contrast



Susceptibility contrast

Fe whisker

Depth sensitivity

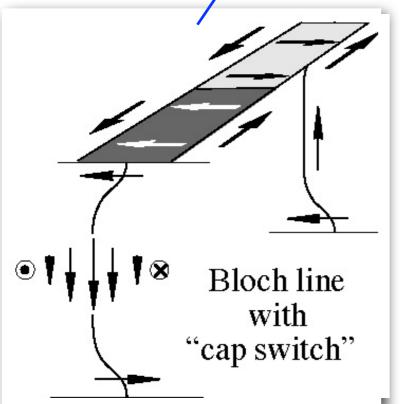


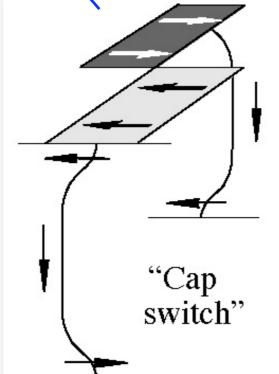
MFM:

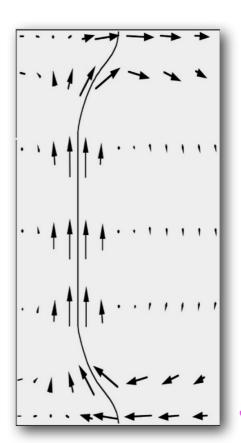
sensitive to interior magnetization of the wall

Kerr:

sensitive to surface magnetization





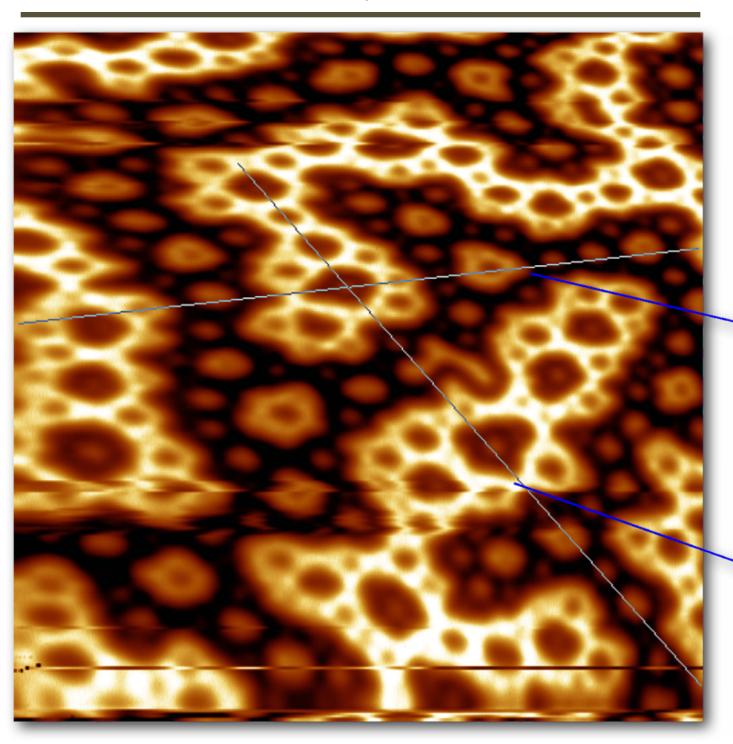


Asymmetric vortex wall

E. Zueco et al., JMMM 196, 115 (1999)

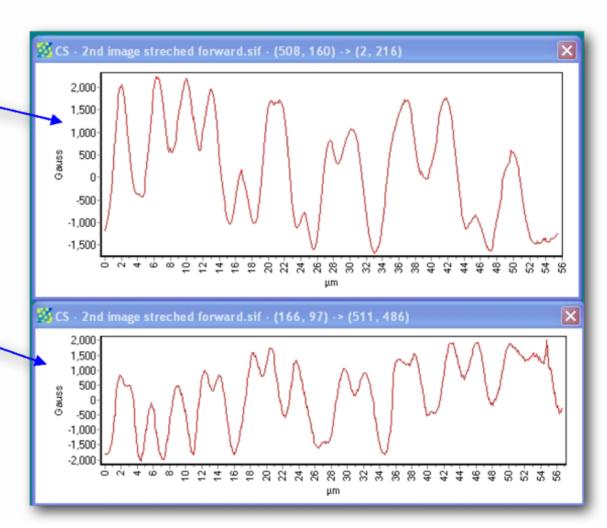
3. Hall-Probe Microscopy

56 μm



NdFeB crystal

Micro-Hallprobe is scanned across surface



Together with J. McCord and U. Wolff, IFW

Sensitivity of imaging methods

$$\mathbf{B} = \mu_0 (\mathbf{H} + \mathbf{M})$$
 $(\mathbf{H} = \mathbf{H}_{ext} + \mathbf{H}_{stray})$
 $\operatorname{div} \mathbf{B} = 0$
 $\operatorname{div} \mathbf{H}_{stray} = -\operatorname{div} \mathbf{M}$

• Sensitive to H_{stray}

· Sensitive to M

- · Sensitive to B
- Sensitive to distortions

- 1. Bitter technique
- 2. Magnetic force microscopy
- 3. Hall probe microscopy
- Magneto-optical microscopy
- X-ray spectroscopy
- Polarized electrons (SEMPA, SPT)
- Transmission electron microscopy
- X-ray, neutron scattering

Sensitivity of imaging methods

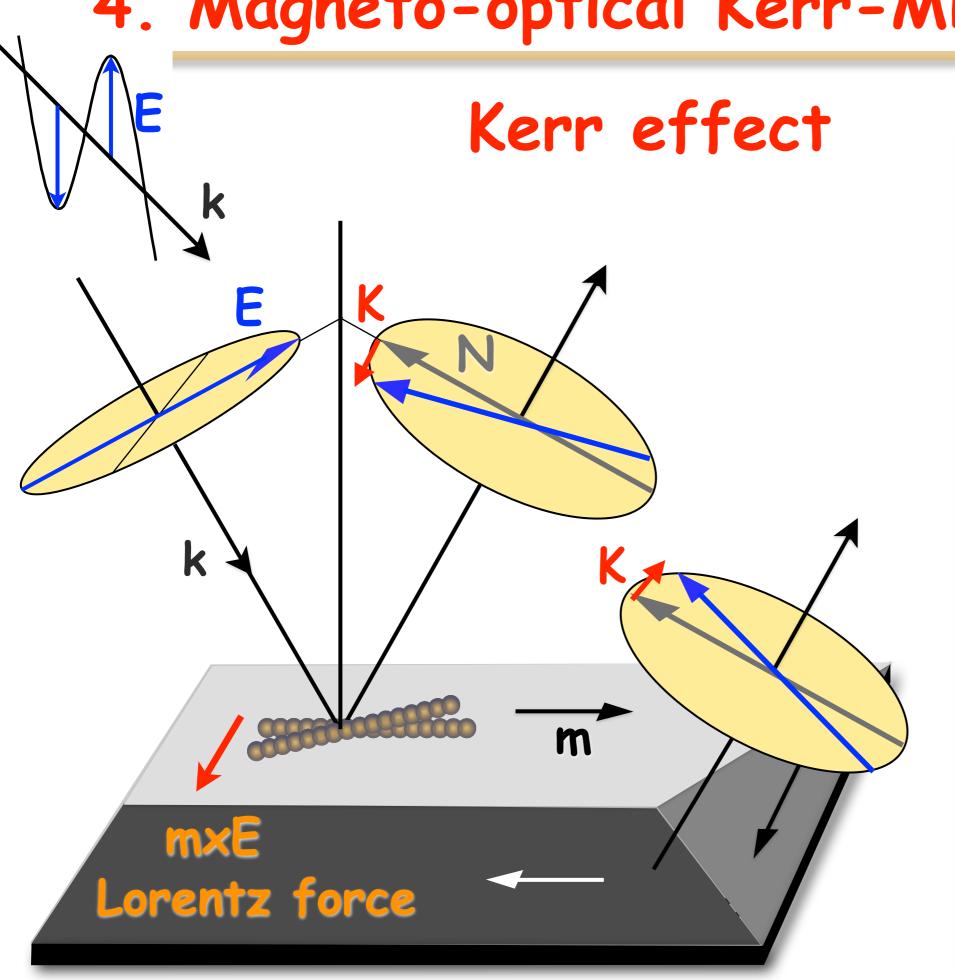
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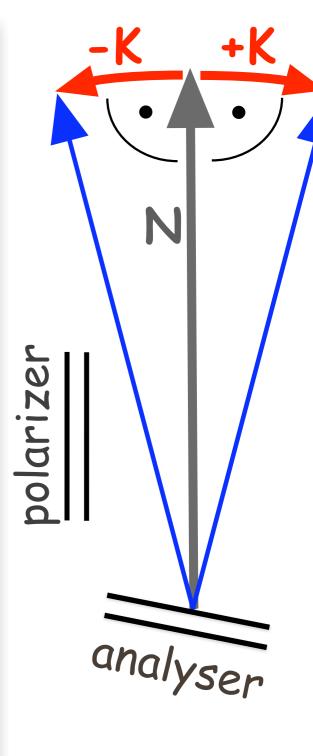
• Sensitive to H_{stray}

· Sensitive to M

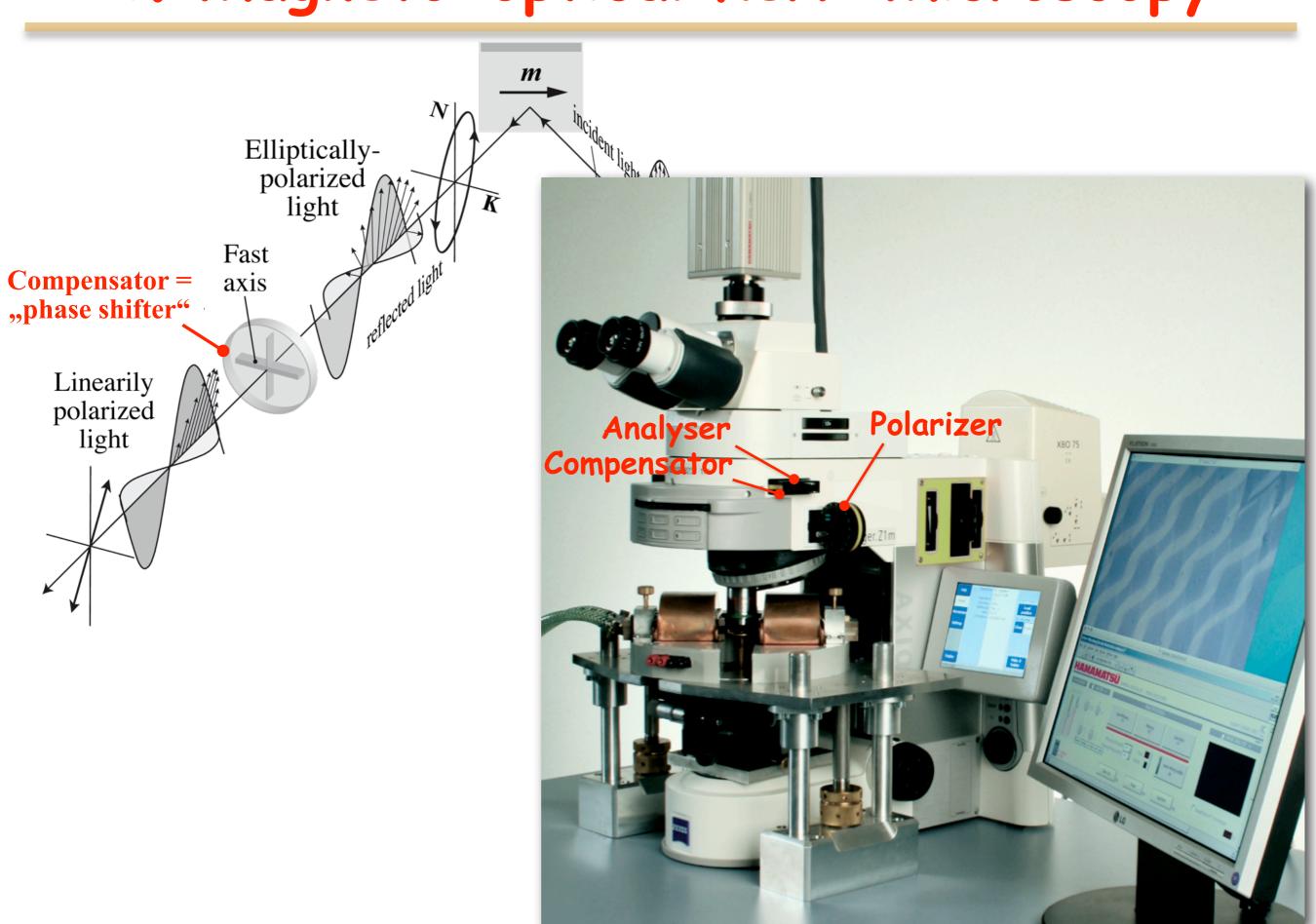
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- 1. Bitter technique
- 2. Magnetic force microscopy
- 3. Hall probe microscopy
- 4. Magneto-optical microscopy
- 5. X-ray spectroscopy
- 6. Polarized electrons (SEMPA, SPT)
- Transmission electron microscopy
- X-ray, neutron scattering

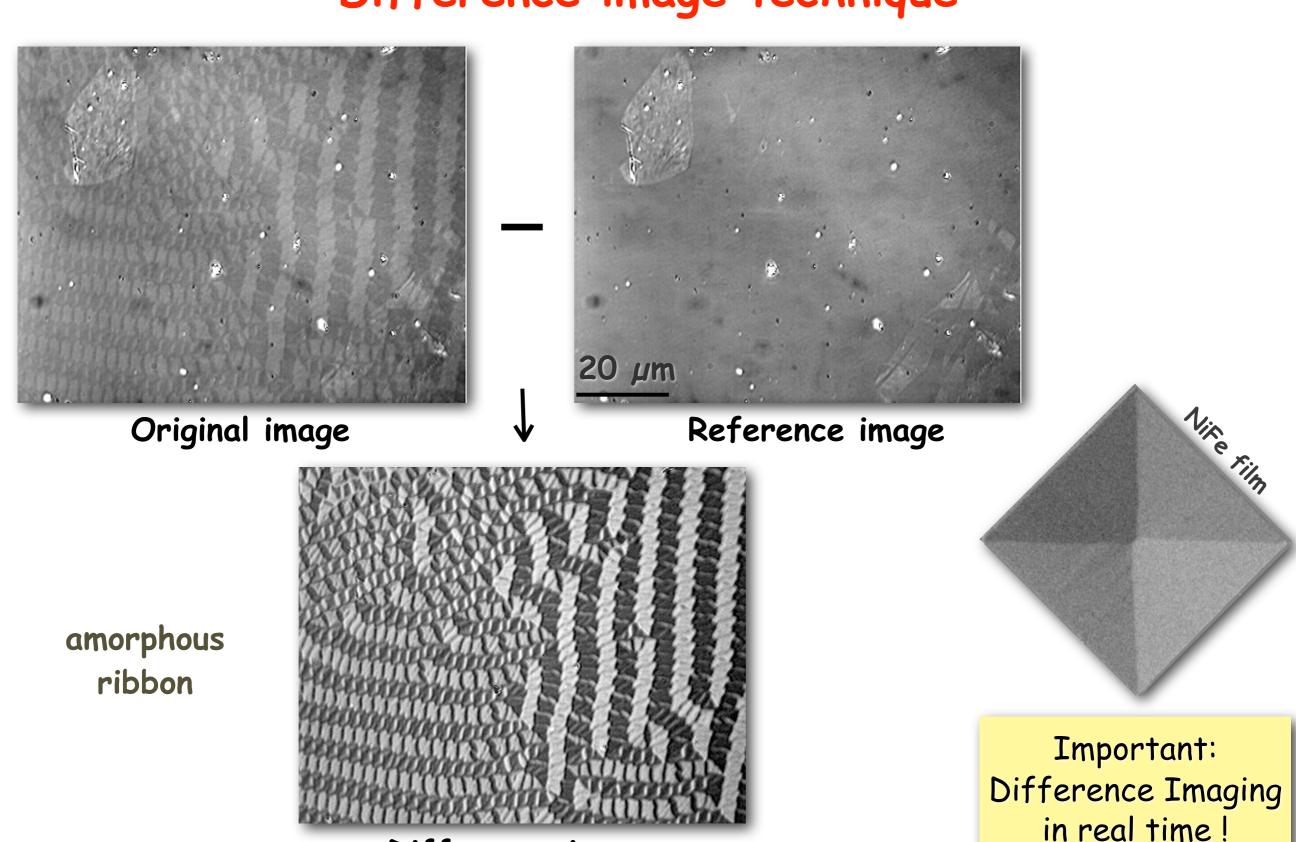




Kerr rotation = K/N 4. Magneto-optical Kerr-N copy m Ellipticallypolarized light **Fast** reflected light **Compensator** = axis "phase shifter" Linearily polarized light

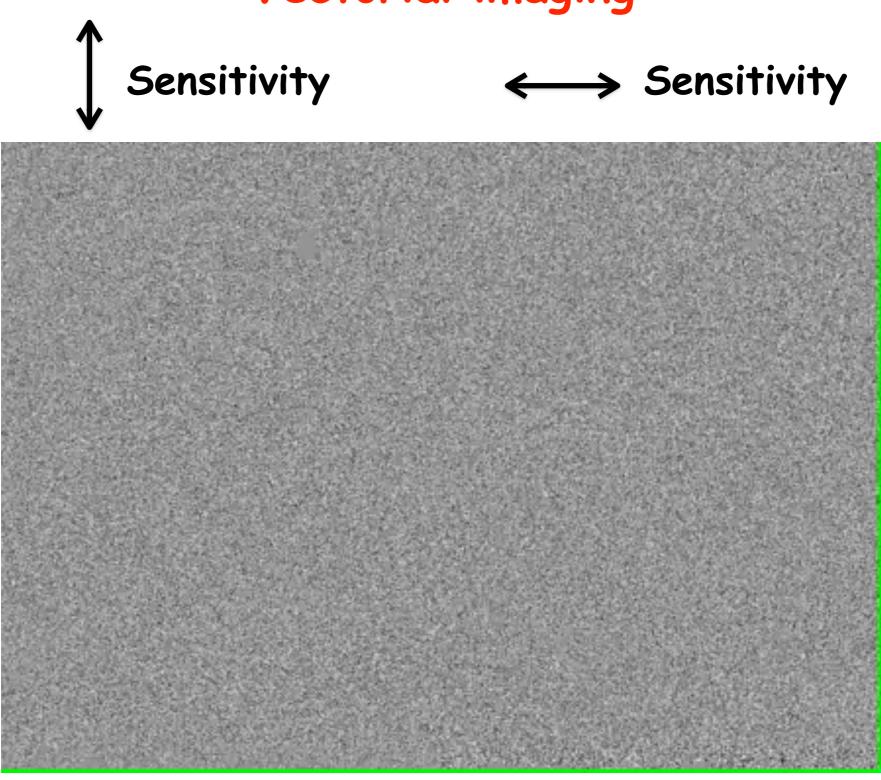


Difference image technique



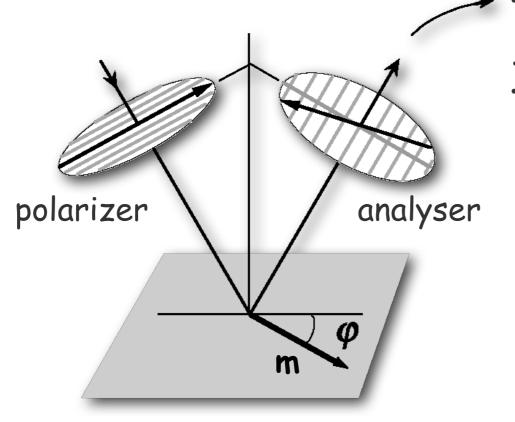
Difference image

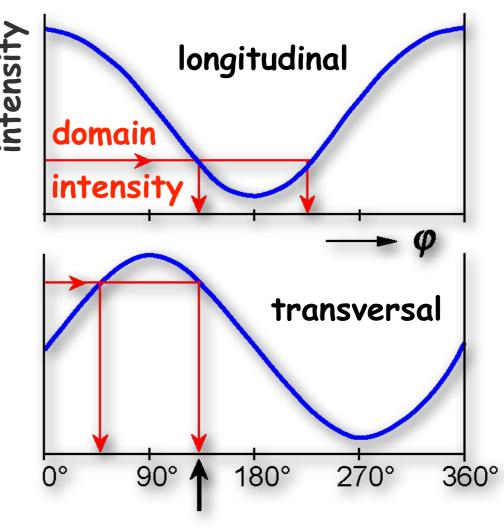
Vectorial imaging



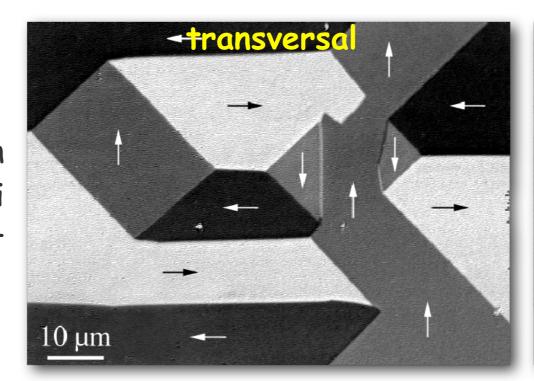
Courtesy J. McCord, Kiel http://www.tf.uni-kiel.de/matwis/nmm/en/movies/laminated

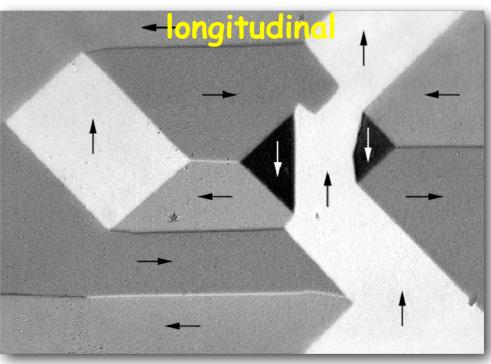
Quantitative Kerr microscopy





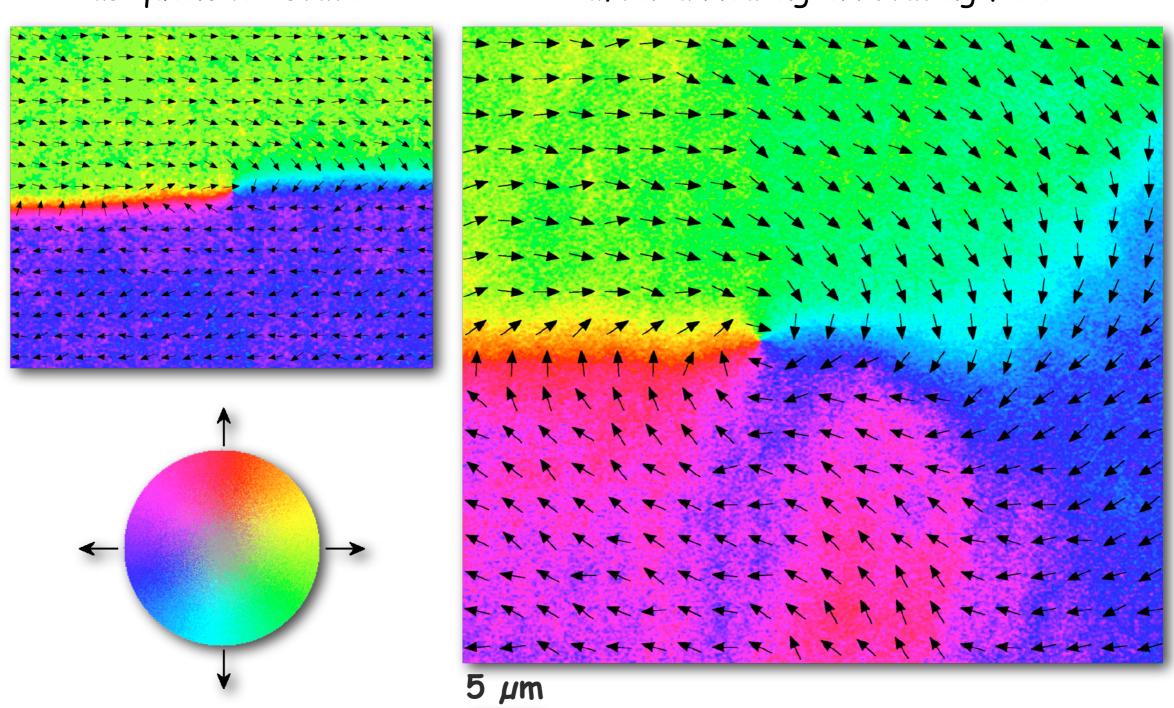
Domains on (100)-FeSi sheet





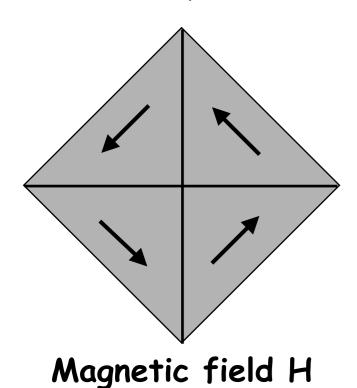
Quantitative Kerr microscopy

Domains in magnetostriction-free amorphous ribbon as-quenched state after annealing in rotating field



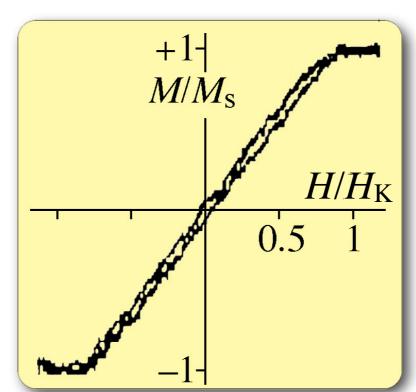
MOKE-Magnetometry and domains

Permalloy (NiFe) film 207 nm thick

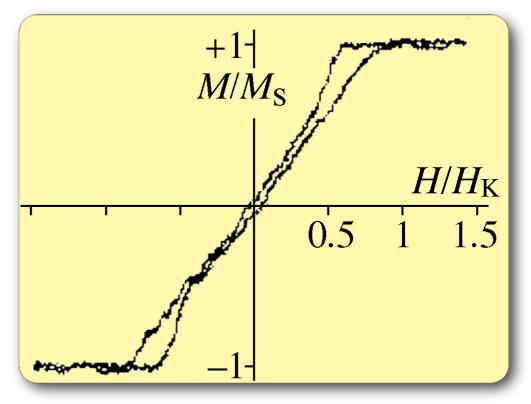


of hw

 $H_{\text{max}} = H_{\text{K}}$



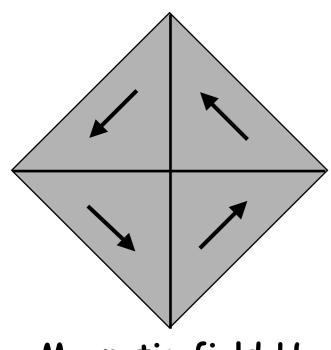
 $H_{\text{max}} > H_{\text{K}}$



MOKE M(H) loops

MOKE-Magnetometry and domains

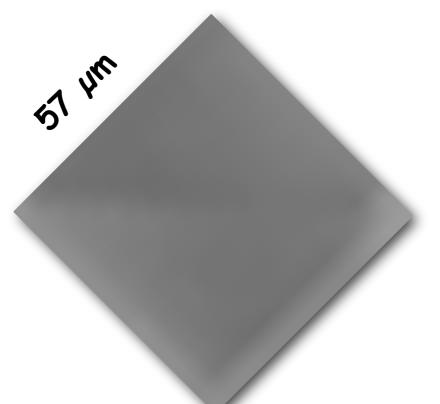
Permalloy (NiFe) film 207 nm thick



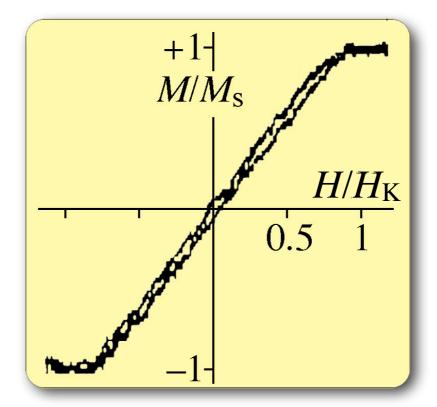
Magnetic field H



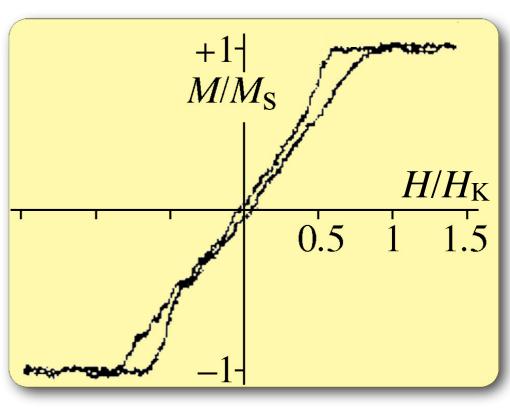
MOKE M(H) loops



 $H_{\text{max}} = H_{\text{K}}$

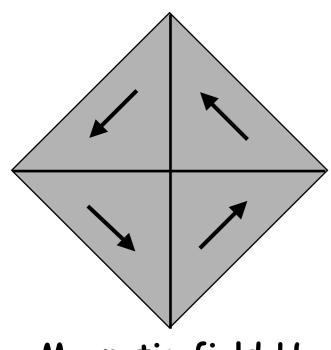


 $H_{\rm max} > H_{\rm K}$



MOKE-Magnetometry and domains

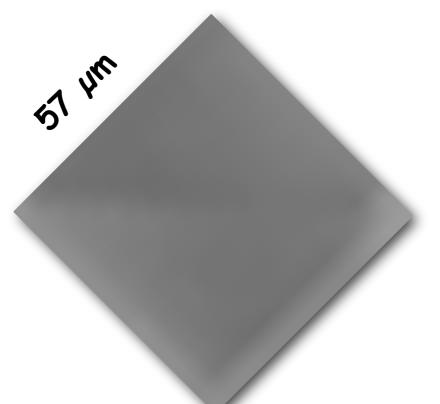
Permalloy (NiFe) film 207 nm thick



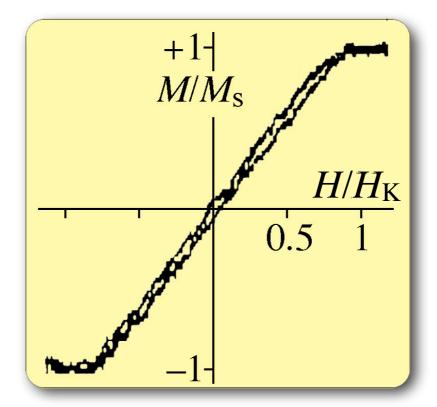
Magnetic field H



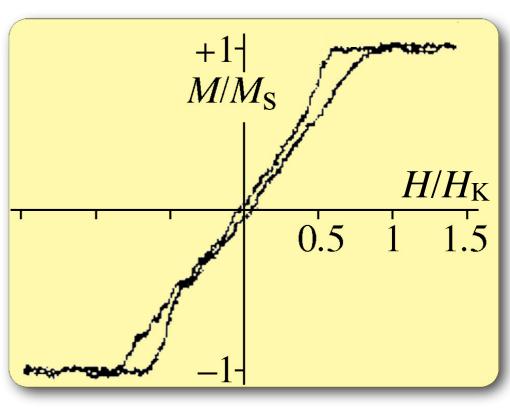
MOKE M(H) loops



 $H_{\text{max}} = H_{\text{K}}$



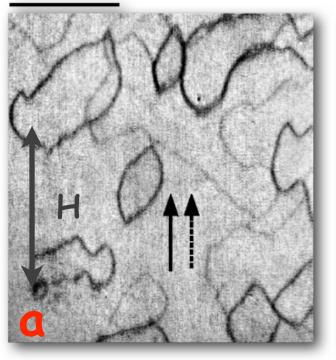
 $H_{\rm max} > H_{\rm K}$



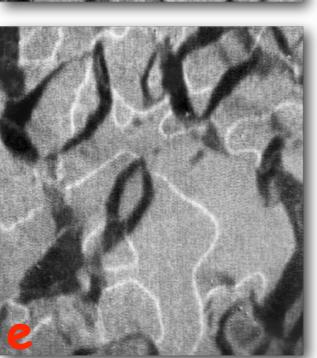
Depth sensitivity of Kerr microscopy

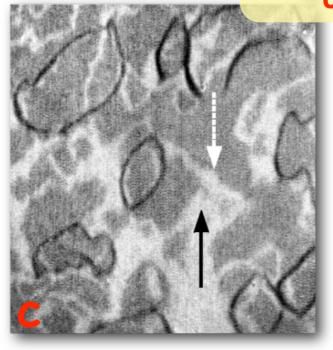
Information depth in metals: ~20 nm

20 μm



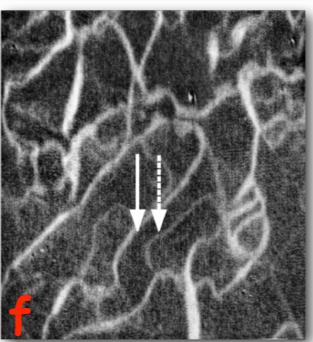






pinned

layer



NiFe (3 nm)

free

layer

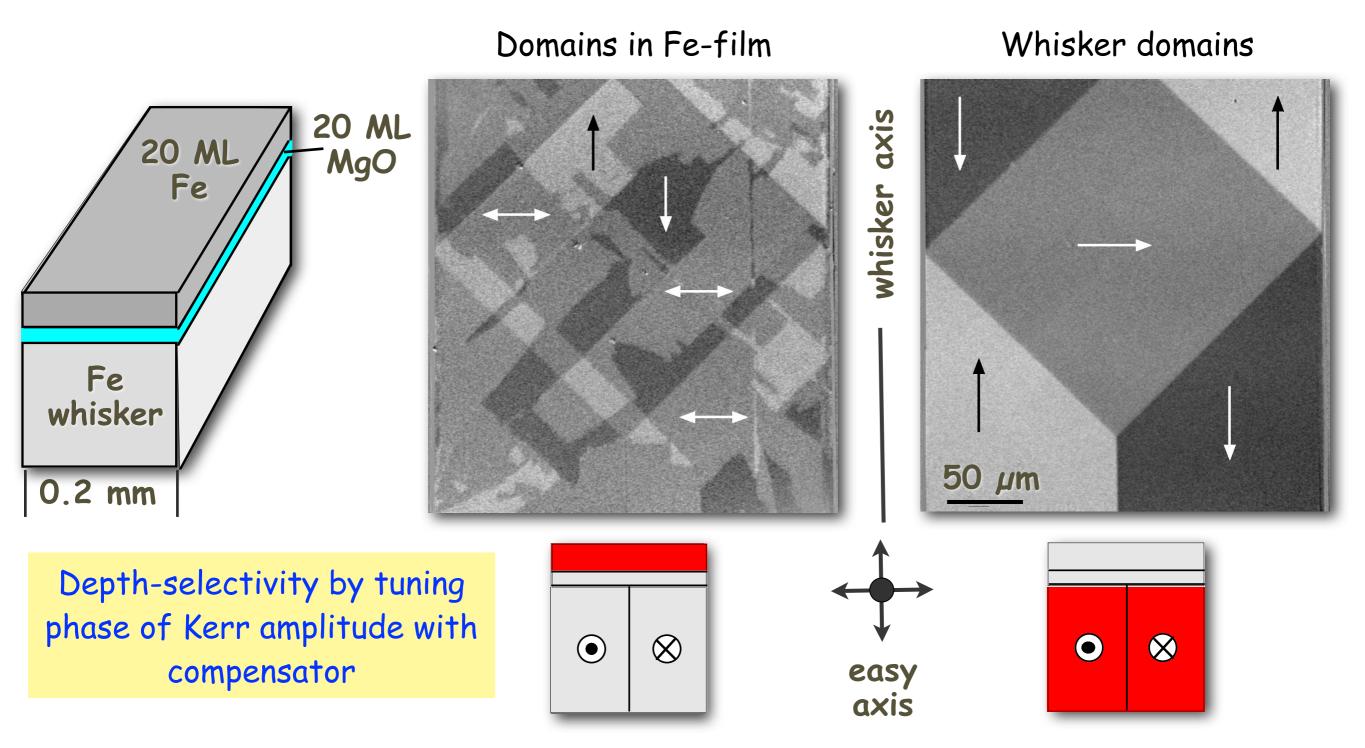
Ru (3 nm)

NiFe (10 nm)

FeMn

Sample: S. Parkin, IBM

Layer-selective Kerr microscopy

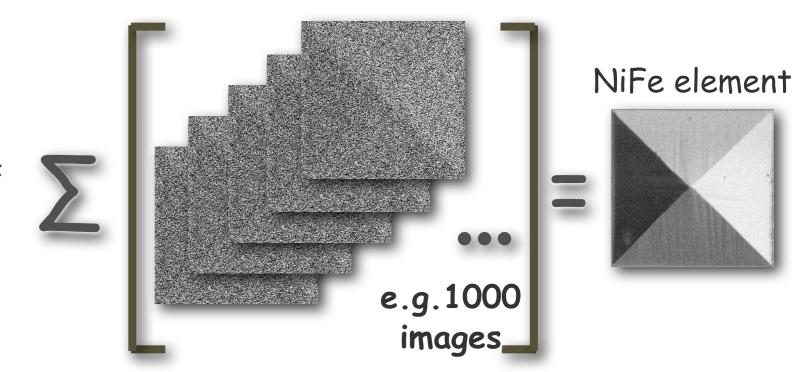


R. S., R. Urban, D. Ullmann, H. L. Meyerheim, B. Heinrich, L. Schultz, J. Kirschner, PRB 65, 144405 (2003)

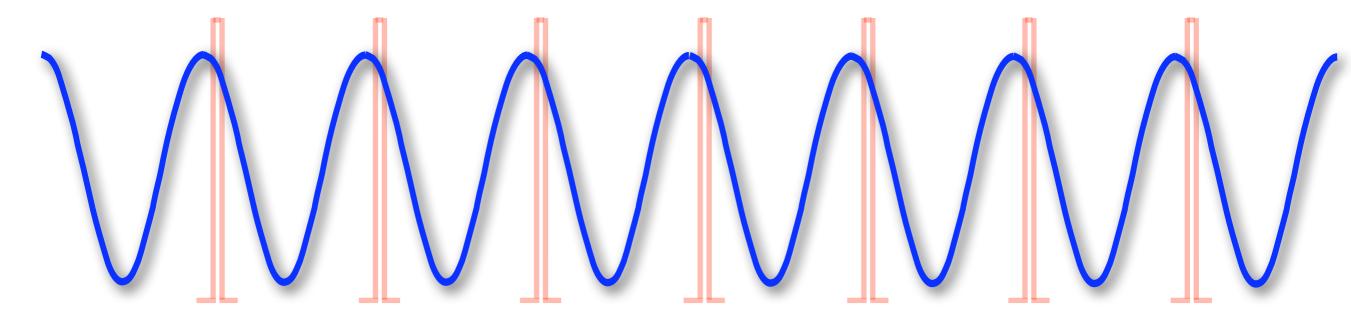
Time-resolved (stroboscopic) imaging

illumination intensity and repetition rate are limited

- → no single-shot imaging possible
- → accumulation of large number of independent events necessary (at fixed time delay)
- → requires repetitive magnetization processes!!



probing with defined time delay

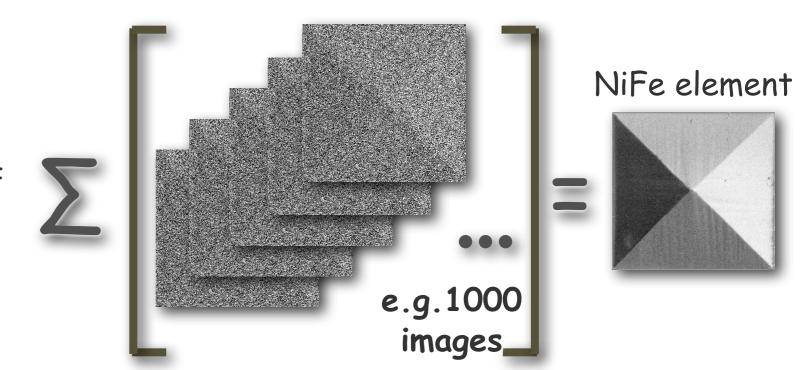


periodic magnetic field excitation

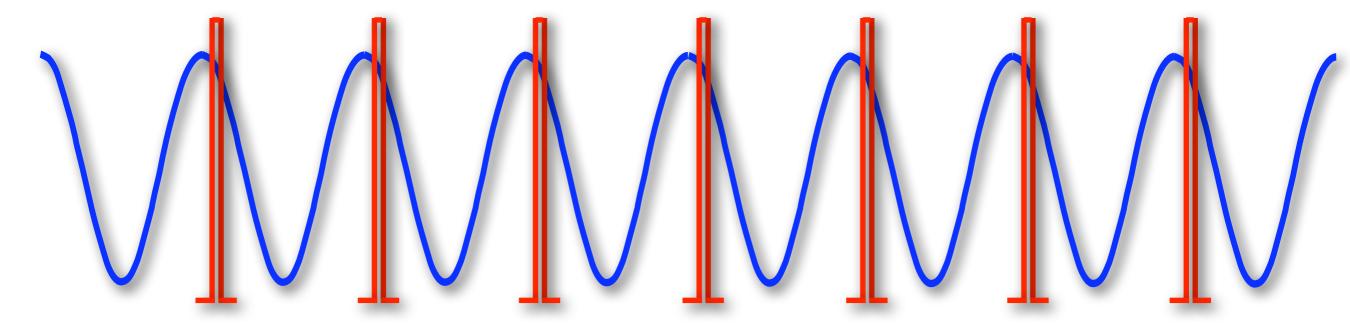
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probing with defined time delay

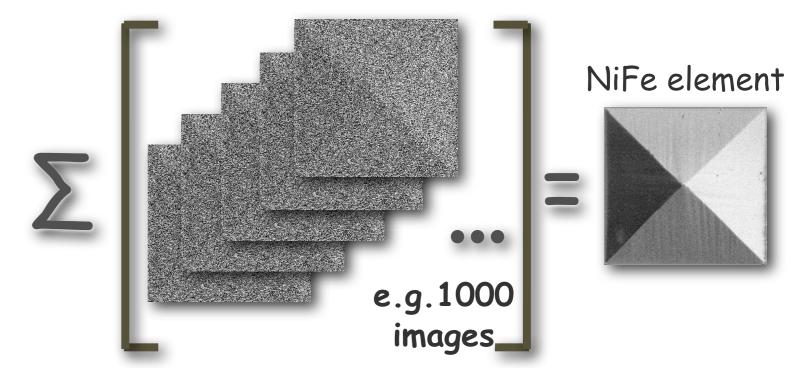


periodic magnetic field excitation

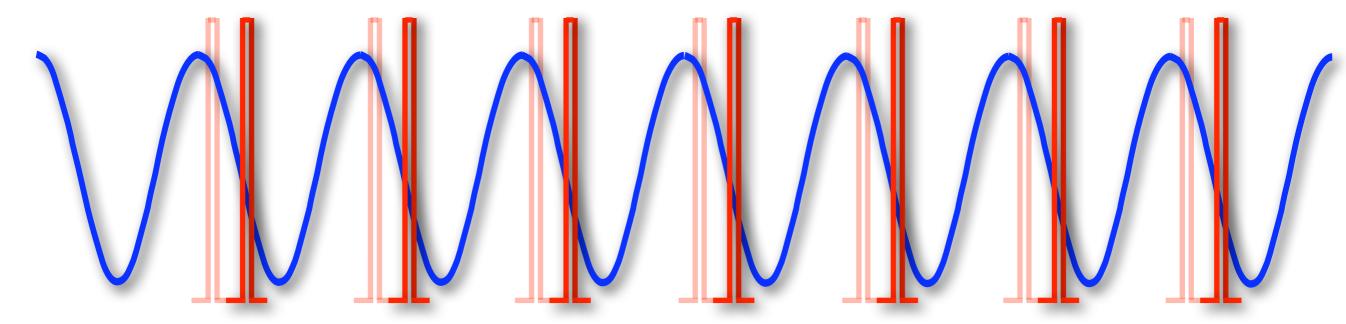
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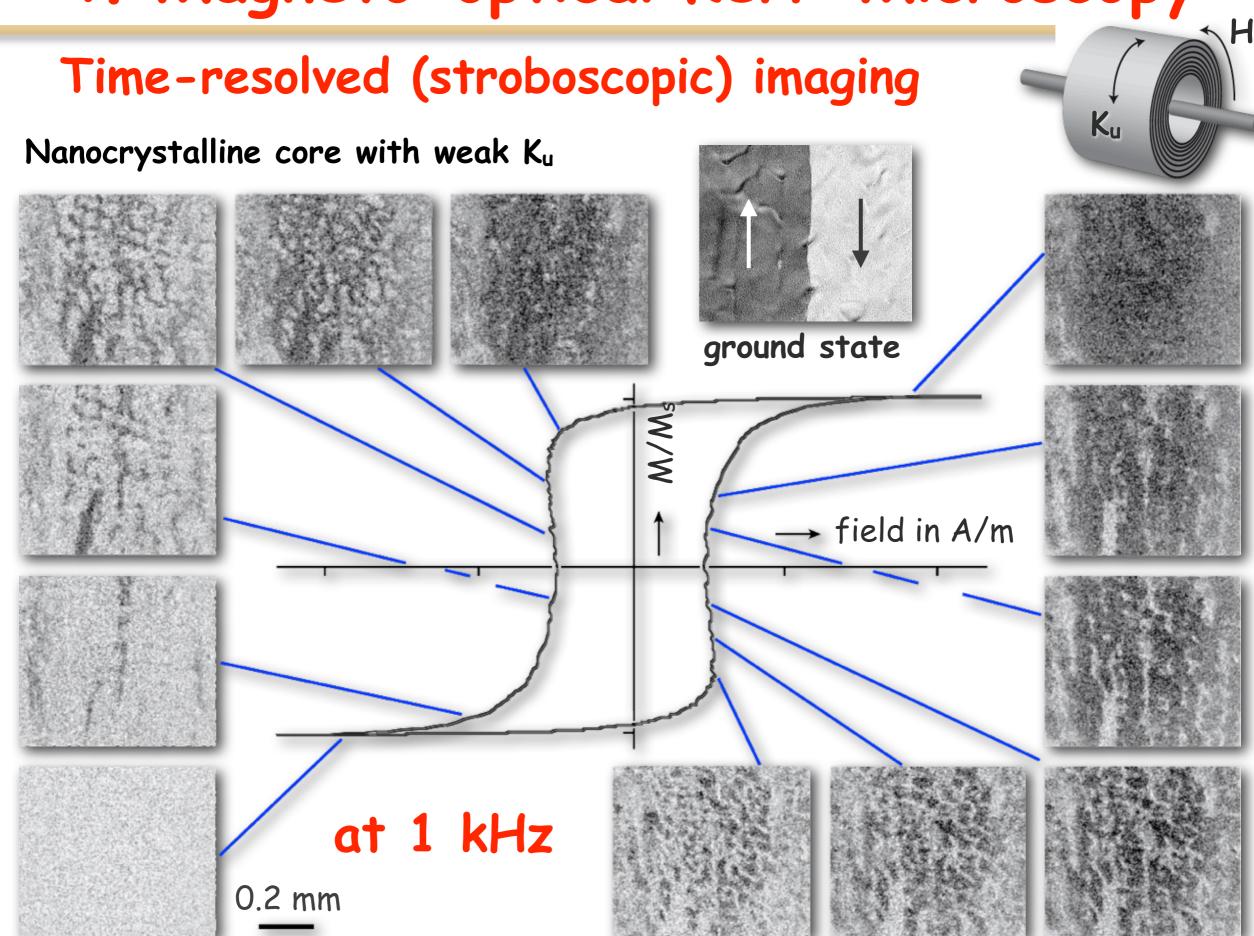
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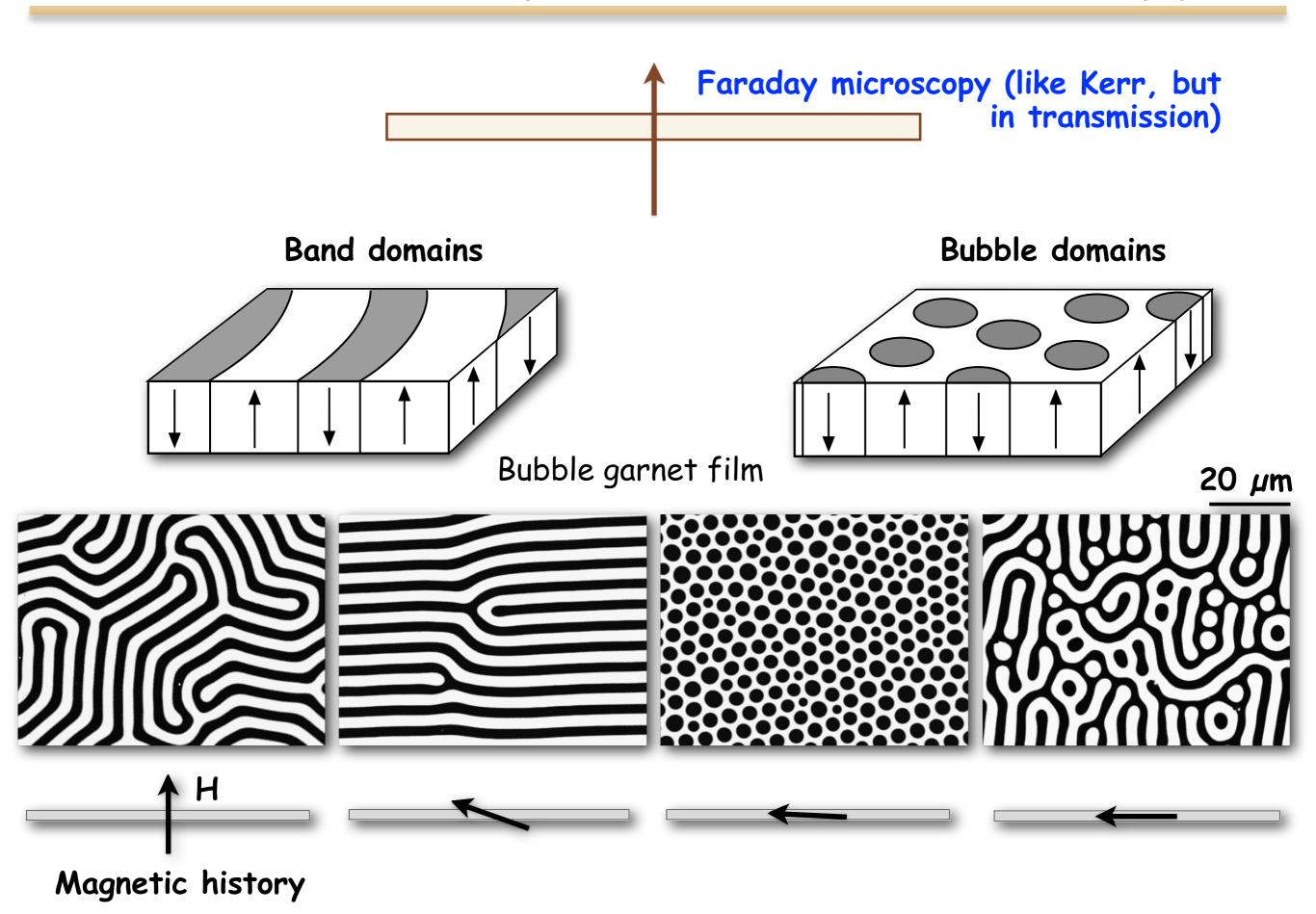


probing with defined time delay

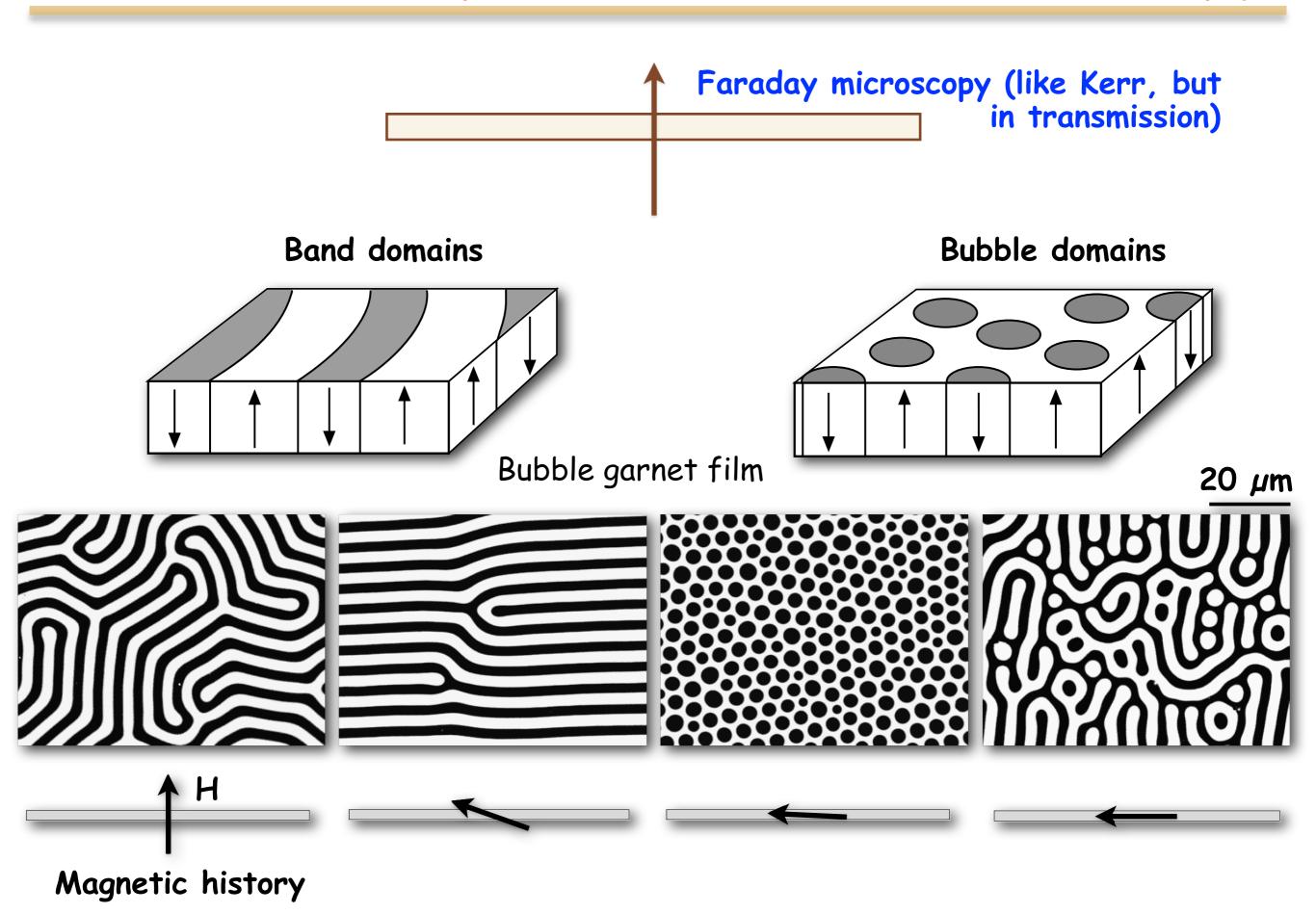


periodic magnetic field excitation

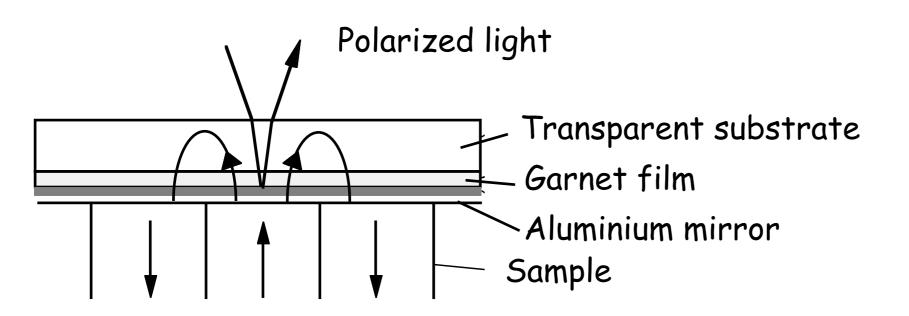


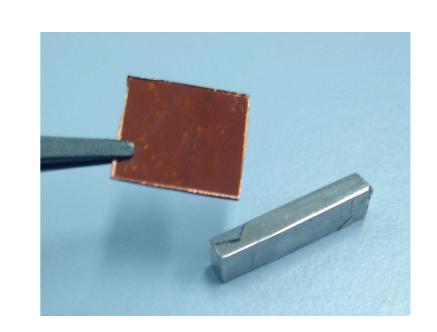


4. Magneto-optical Faraday-Microscopy



Indicator film technique: stray field imaging



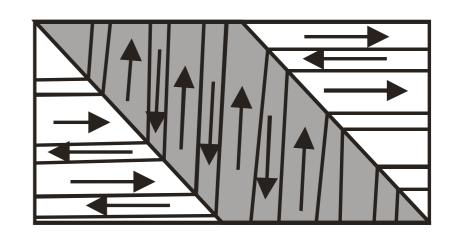


Metallographic contrast



With indicator film





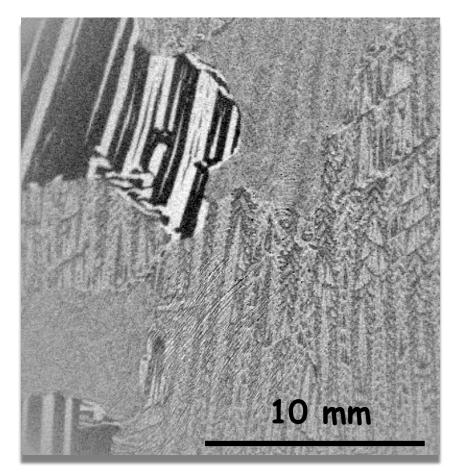
200 μm

Bulk NiMnGa single crystal

(shape memory material, does not show direct Kerr contrast)

Indicator film technique: stray field imaging

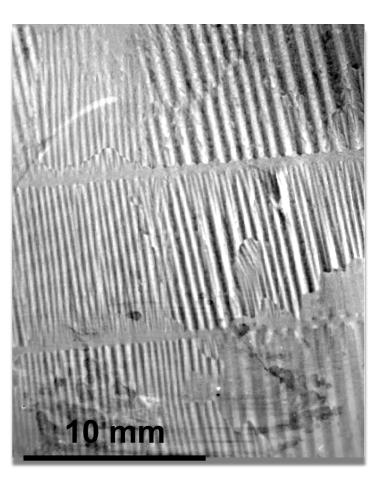
Grain oriented electrical steel:



Direct Kerr contrast (sample polished)



MOIF contrast (sample polished)

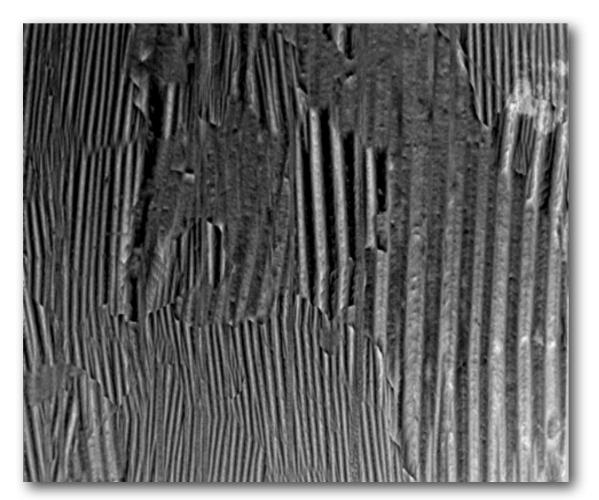


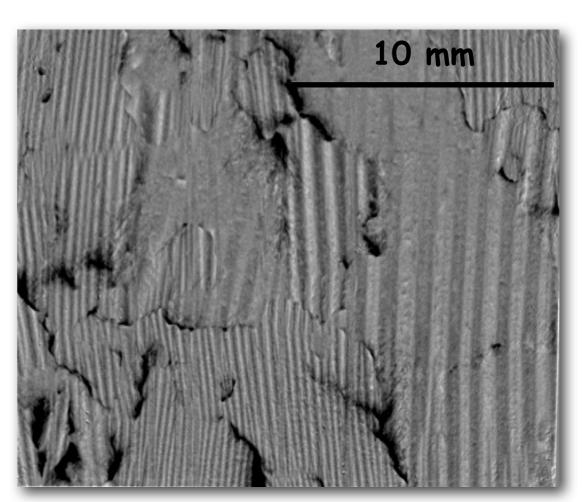
MOIF contrast (with insulation coating)

Domain contrast even through coating

Indicator film technique: stray field imaging

Grain oriented electrical steel:



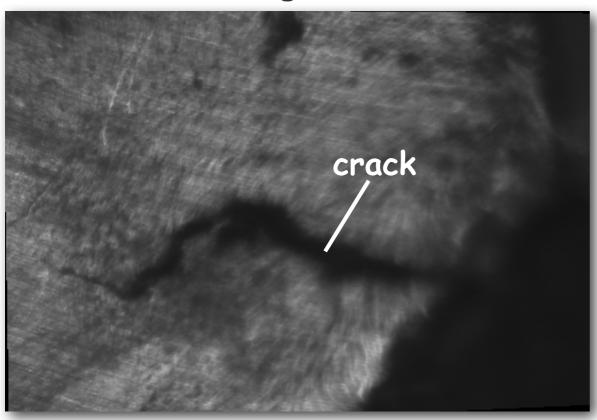


MOIF contrast (with insulation coating)

Magnetic Pole contrast at grain boundaries

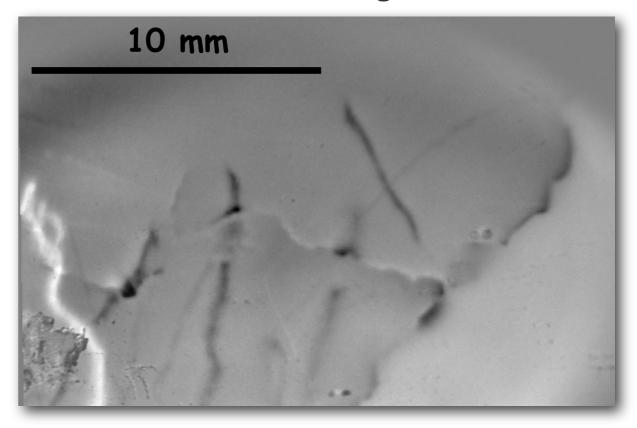
Indicator film technique: stray field imaging

Direct image of surface



Rail track with crack

MOIF image

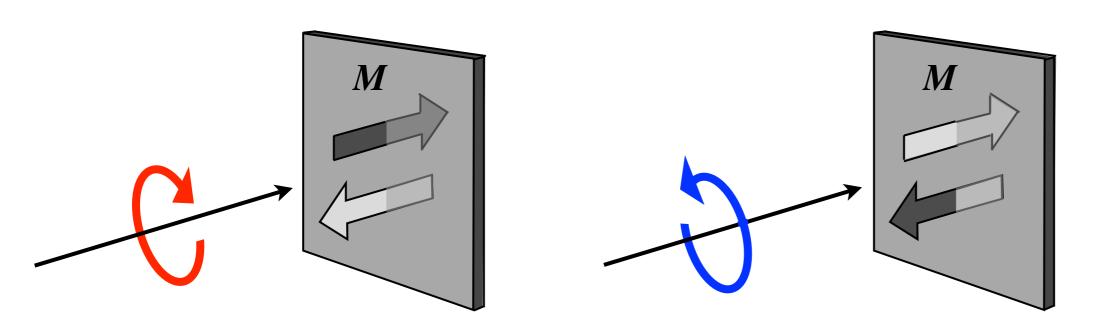


Imaging of defects for non-destructive testing

Together with G. Y. Tian, Chengdu

X-Ray Magnetic Circular Dichroism (XMCD)

XMCD: Absorption of circularly polarized x-rays depends on orientation of magnetization M with respect to helicity of the X-rays, change of sign by reversing M



X-Ray Magnetic Circular Dichroism (XMCD)

XMCD: Absorption of circularly polarized x-rays depends on orientation of magnetization M with respect to helicity of the X-rays, change of sign by

reversing **M**

Physical origin: If energy of absorbed photon exceeds binding energy of an inner core level (e.g. $p_{1/2}$ and $p_{2/3}$ states, separated by spin-orbit coupling)

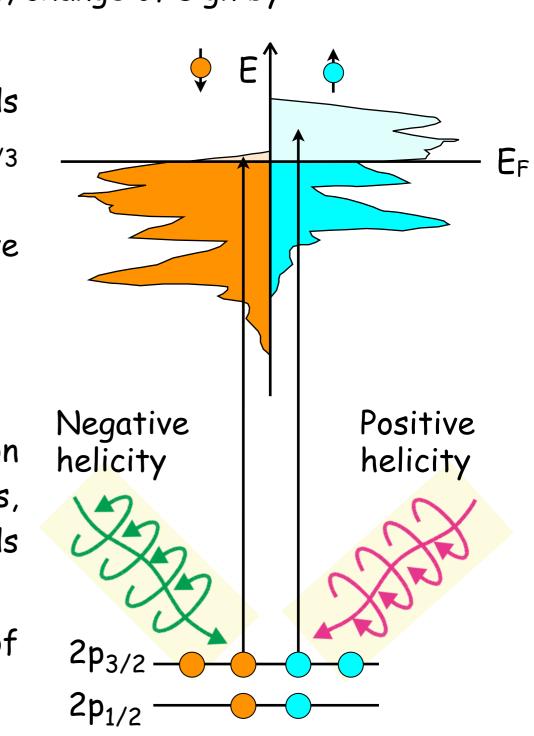
→ Transition into unoccupied spin-split states above Fermi level (e.g. into 3d band)

Initial states are well defined inner-core levels

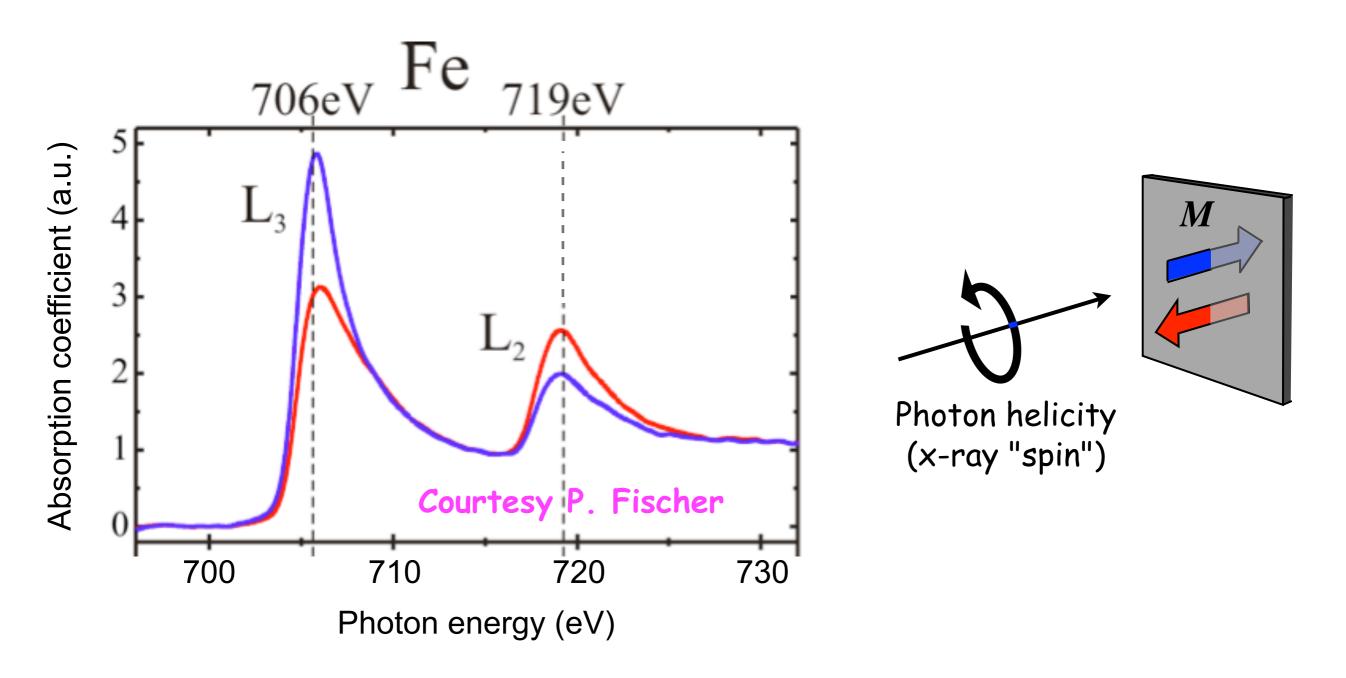
→ XMCD is element selective

Fermi's golden rule: transition probability of absorption process is related to density of unoccupied states, which are different for minority and majority bands due to exchange interaction

 \rightarrow X-MCD signal is proportional to magnetic moment of absorbing atom \rightarrow Sensing of magnetization of sample

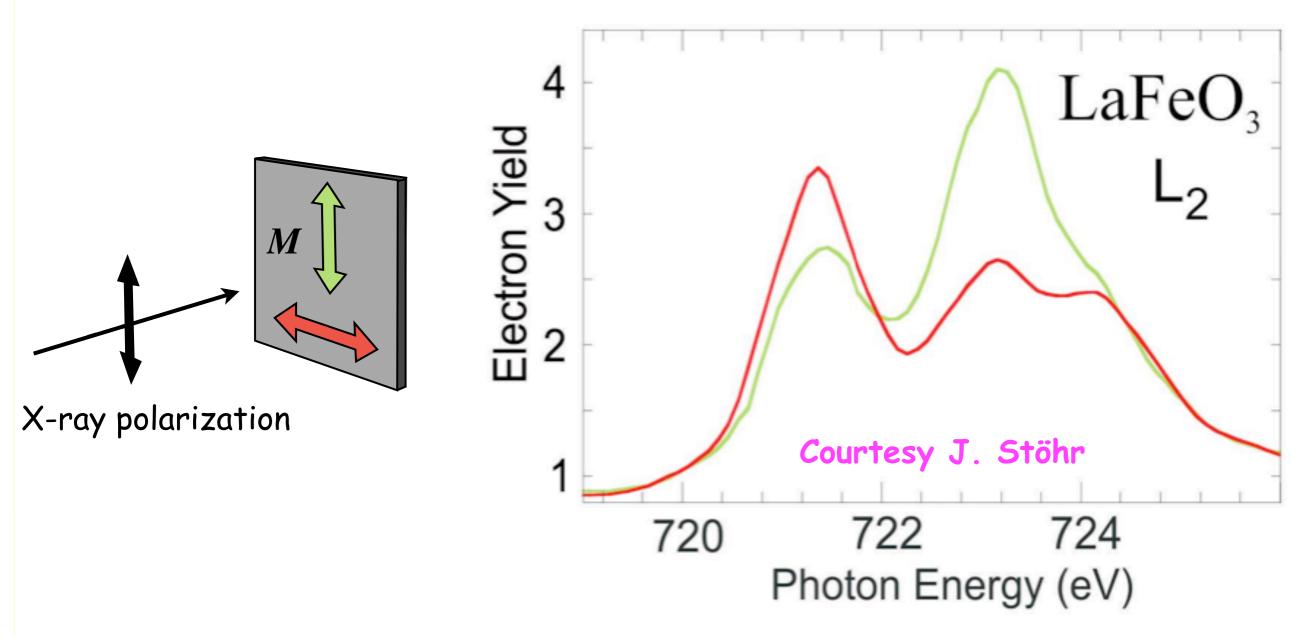


X-Ray Magnetic Circular Dichroism (XMCD)



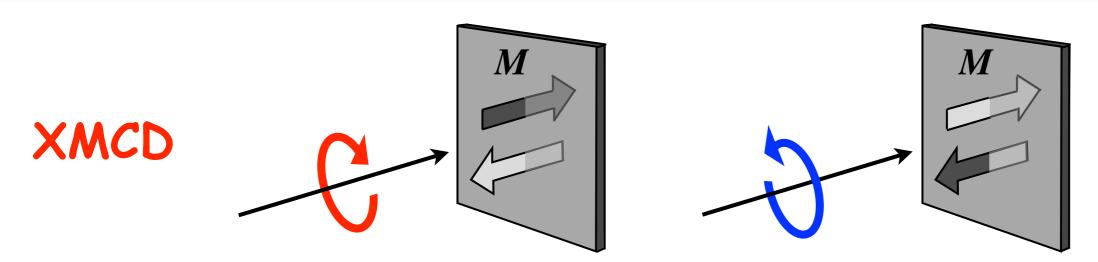
XMCD effect is localized around L_2 (transition from $2p_{1/2}$ core level to unoccupied 3d states) and L_3 (transition from $2p_{3/2}$ core level) absorption edges, which are separated by the spin-orbit coupling

X-Ray Magnetic Linear Dichroism (XMLD)

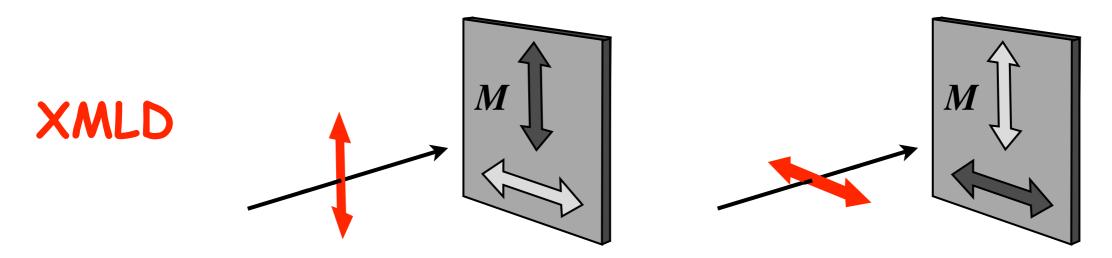


Oxides are usually antiferromagnetic: studied with X-Ray Magnetic Linear Dichroism (XMLD) spectroscopy

The XMLD effect is large only in cases where the absorption edge exhibits multiplet structure



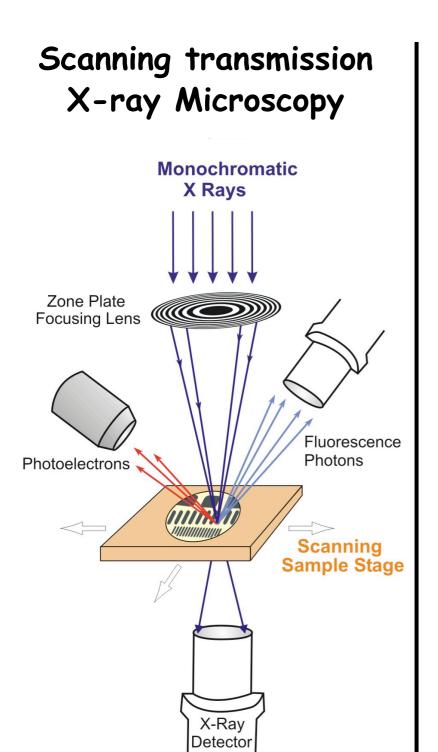
XMCD detects the difference in absorption for the projection of the sample's magnetization onto the propagation direction of circularly polarized X rays. XMCD distinguishes between magnetization parallel and antiparallel to the light propagation direction

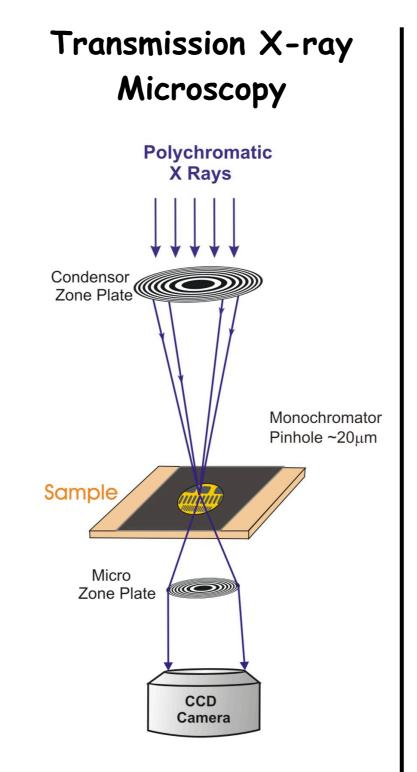


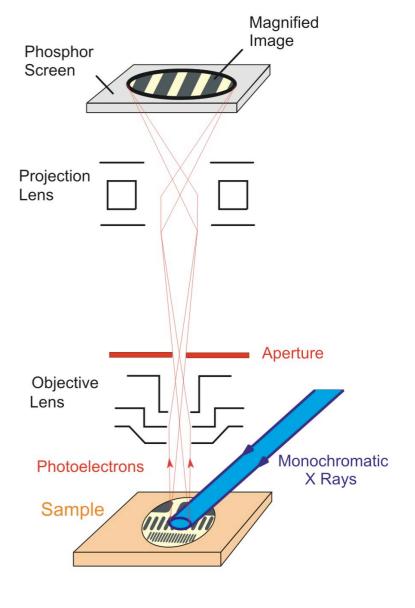
XMLD detects the difference in absorption of the axis of magnetization aligned parallel or perpendicular to the E-field of the X-rays.

XMLD distinguishes between the sample being magnetized parallel or perpendicular to the light polarization direction

X-Ray microscopy methods

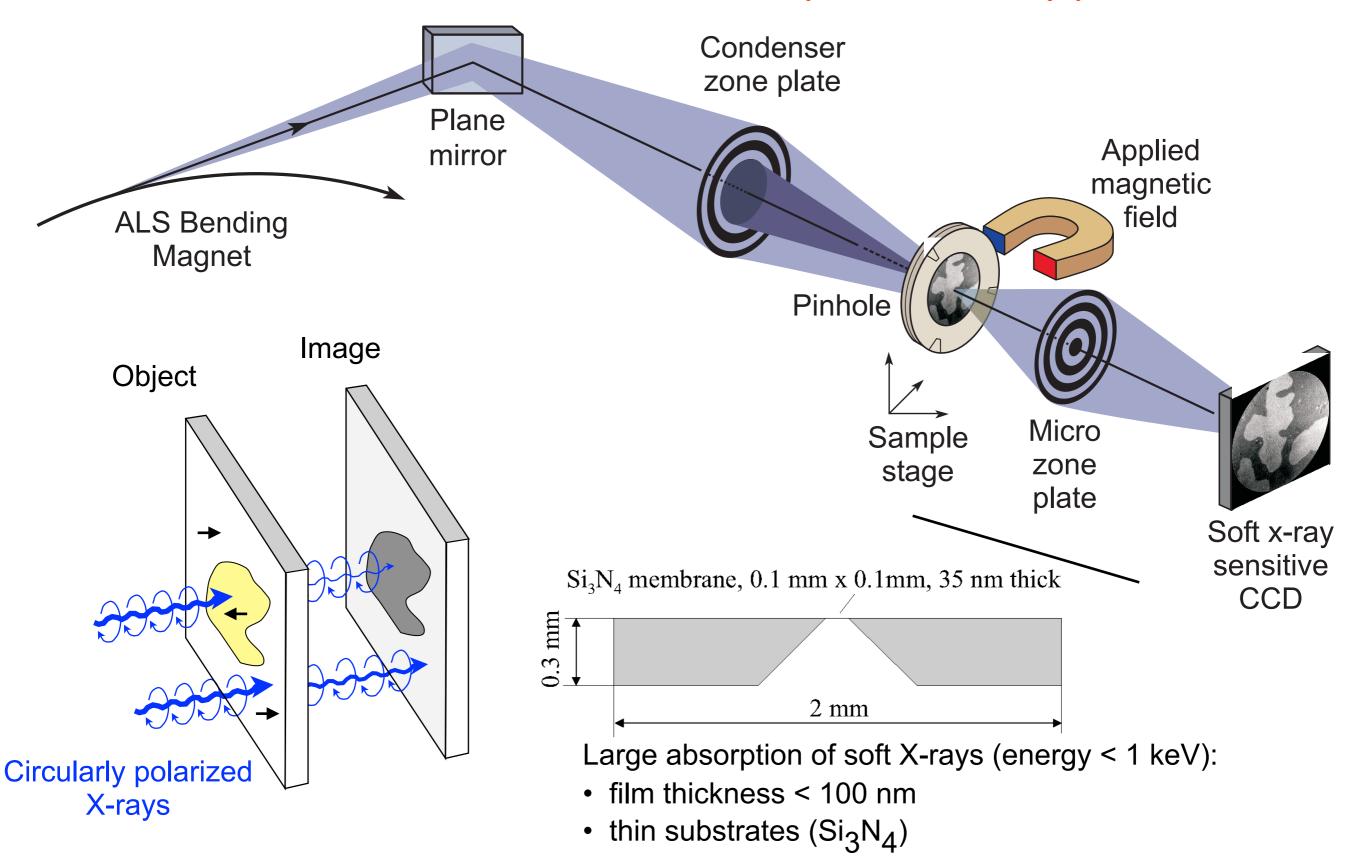






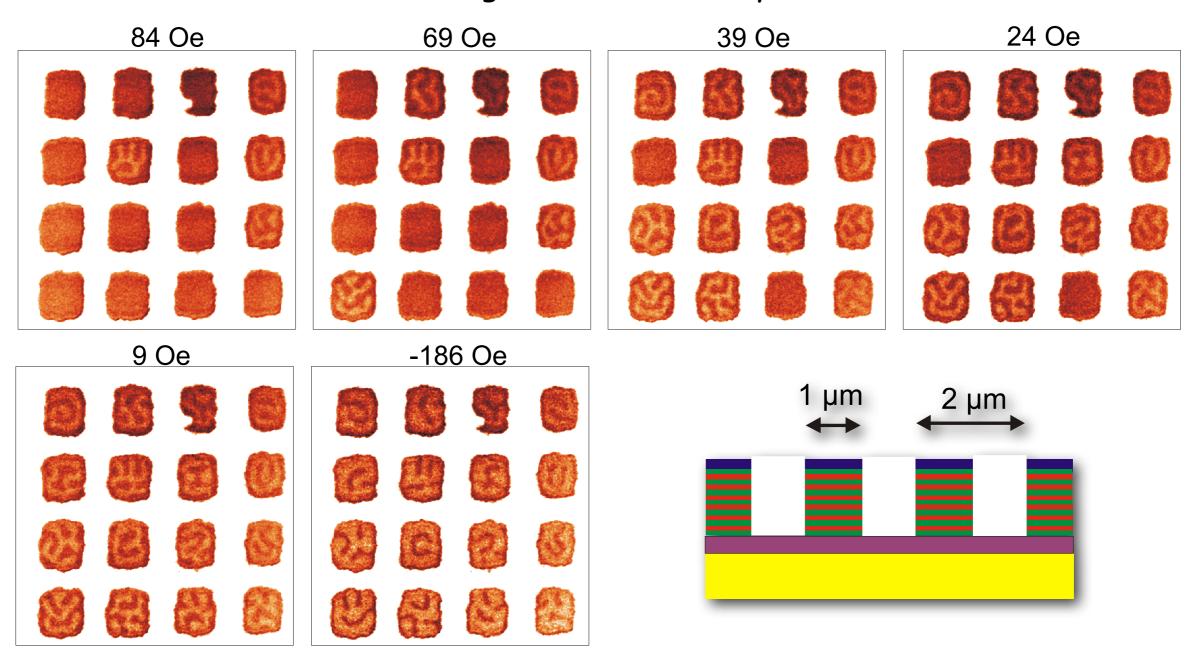
Resolution in 20 nm range

5.1 Transmission X-Ray microscopy



5.1 Transmission X-Ray microscopy

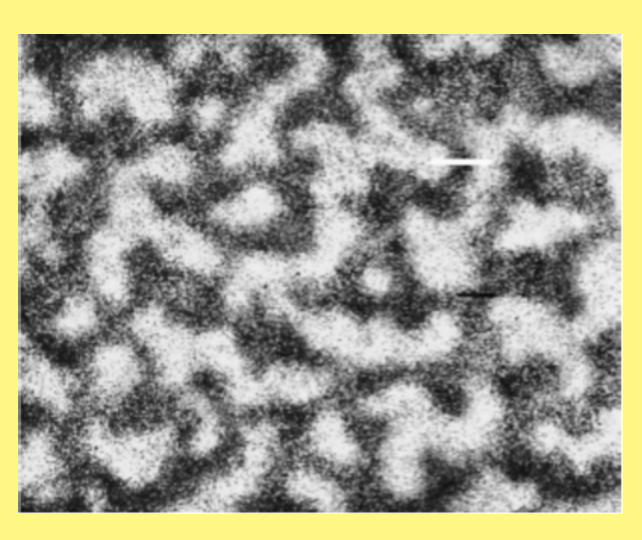
Switching of Fe/Gd multilayered dots

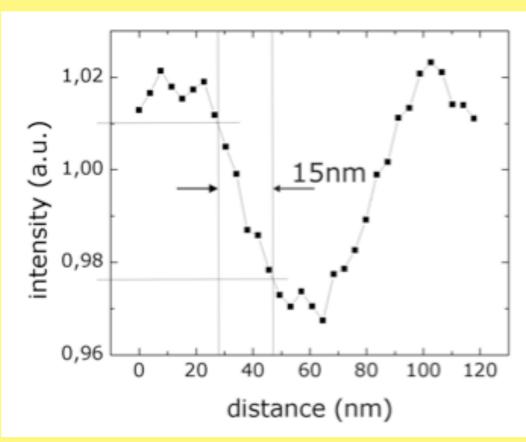


Courtesy P. Fischer, Th. Eimüller

5.1 Transmission X-Ray microscopy

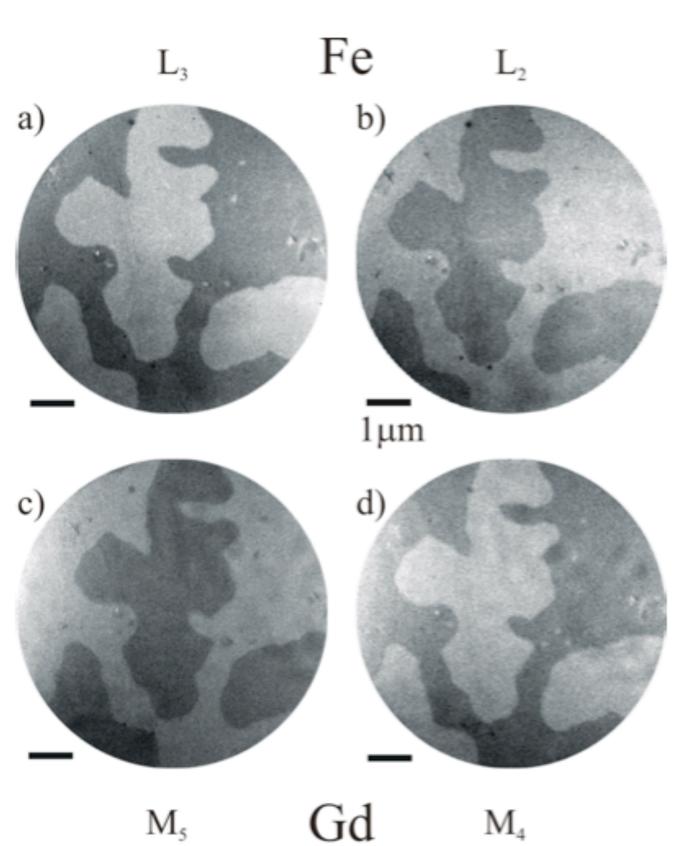
Intensity profile across the boundary of a magnetic domain in an amorphous GdFe layer showing a lateral resolution of less than 15 nm





Courtesy P. Fischer

5.1 Transmission X-Ray microscopy

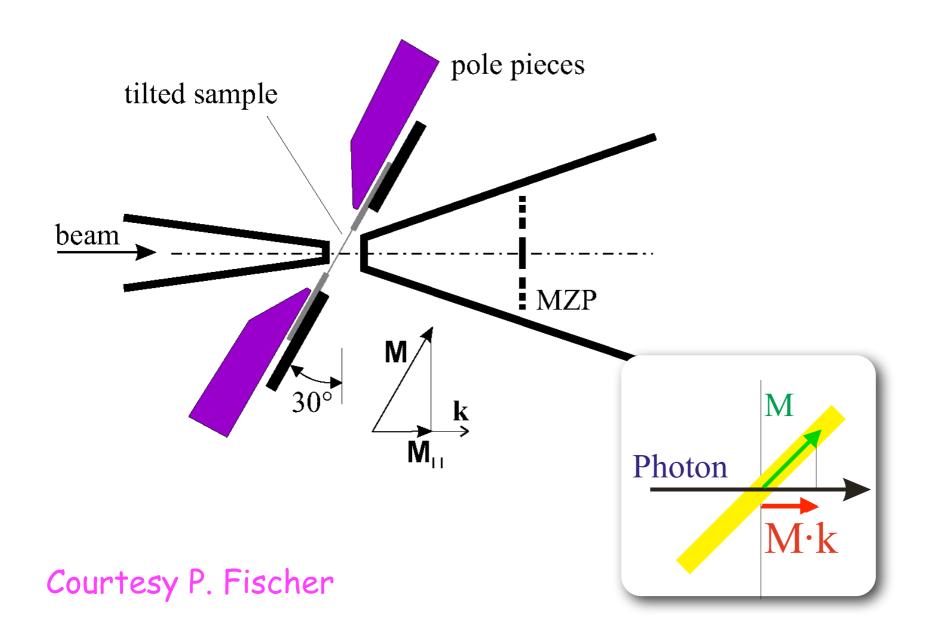


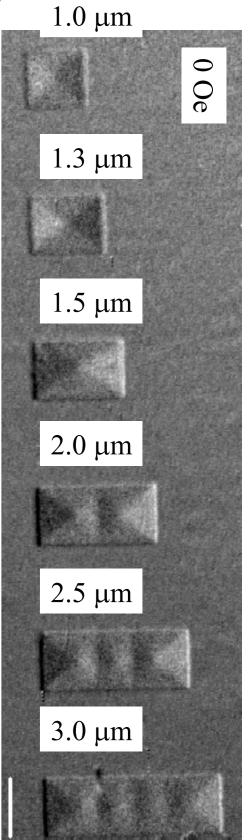
- MTXM images of an amorphous
 Gd₂₅Fe₇₅ layer recorded at the
 spin- orbit-coupled Fe L₃ (a) and
 L₂ (b) as well as at the Gd M₅ (c)
 and M₄ (d) absorption edges
- Contrast inversion: magnetic moments on Cd and Fe couple antiparallel

5.1 Transmission X-Ray microscopy

In-plane imaging

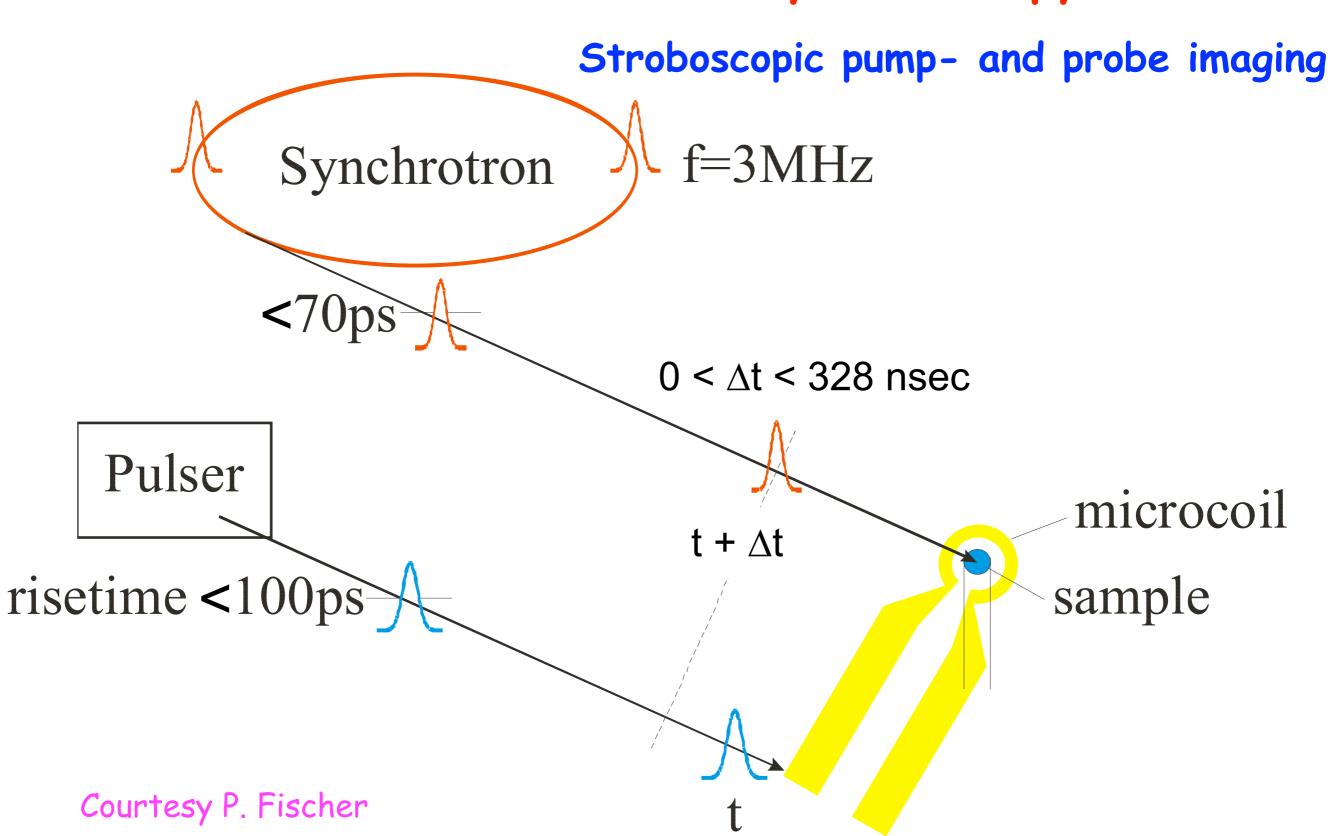
Dichroic contrast: given by projection of M on photon propagation direction. In-plane imaging by tilting the sample (30°):

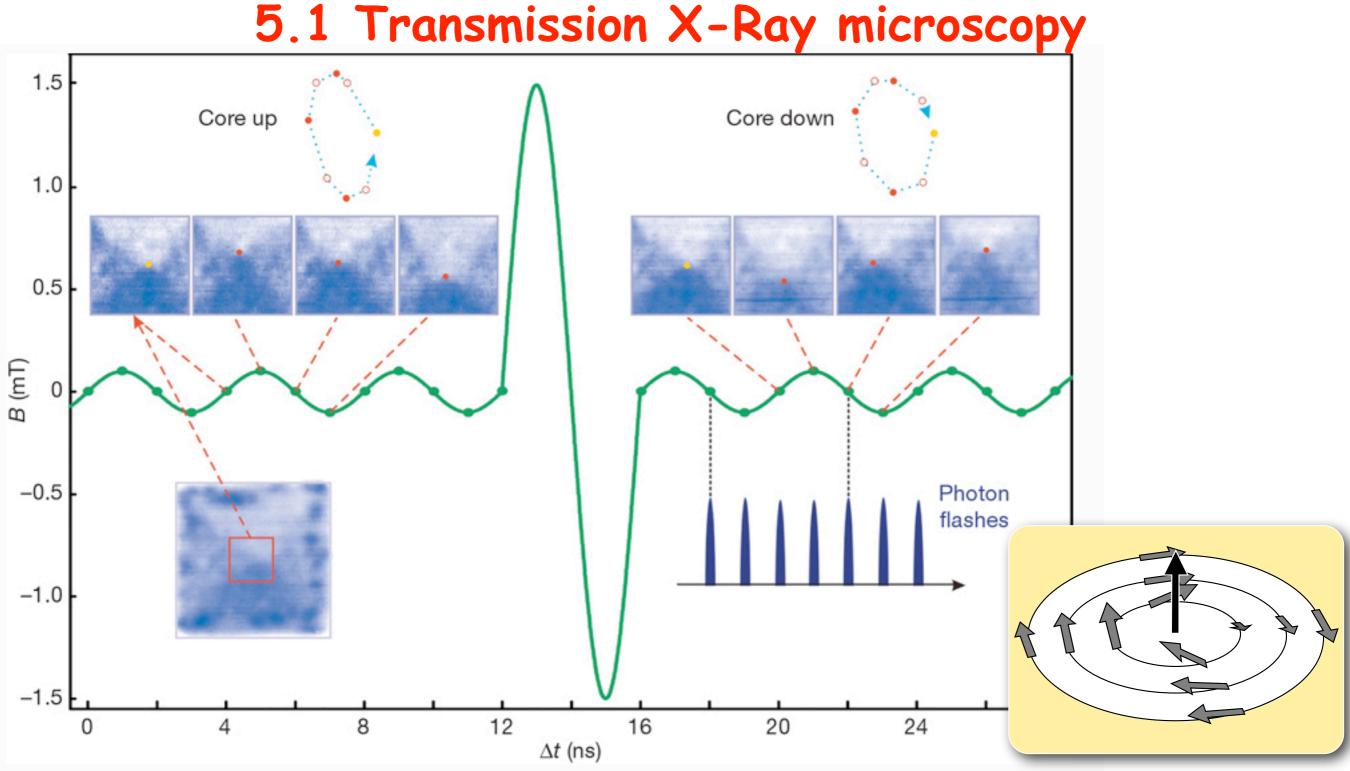




1 µm

5.1 Transmission X-Ray microscopy





Excitation of vortex structure in ac field (frequency 250 MHz, amplitude 0.1 mT). After a 4 ns 'single period' burst (amplitude 1.5 mT) the vortex core polarity is inverted B. Van Waeyenberge et al., Nature 444, 461 (2006)

5.1 Transmission X-Ray microscopy

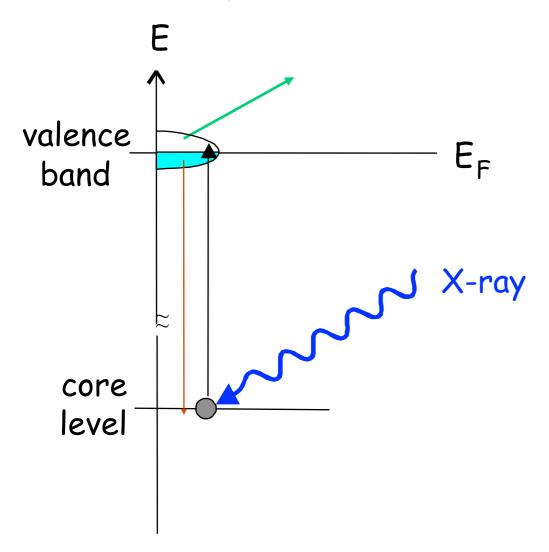
Advantages

- · Lateral resolution at approx. 15 nm
- · Imaging in applied magnetic fields (currently some kOe)
- Quantitative (contrast proportional to M)
- Probing of in- and out-of-plane magnetization
- Time resolution in the sub-ns regime
- · Element specific imaging
- · High sensitivity to few nm layers (for Fe: < 2 nm)

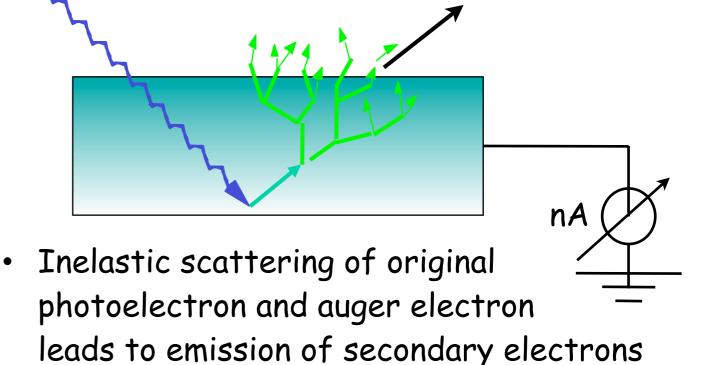
Disadvantages

- Sample must be transparent (d < 100 nm)
- Thin substrates
- Synchrotron radiation necessary

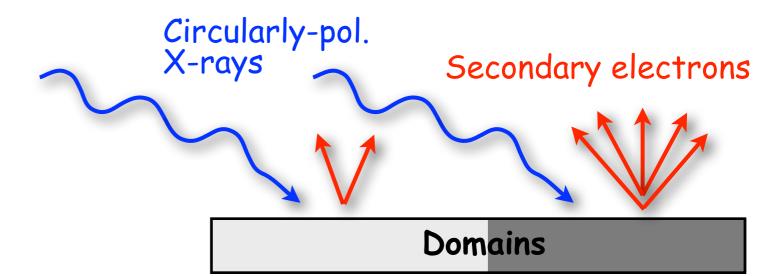
- Excitation of core electron into empty valence state by incoming X-ray
- Recombination (e.g.) by Auger decay

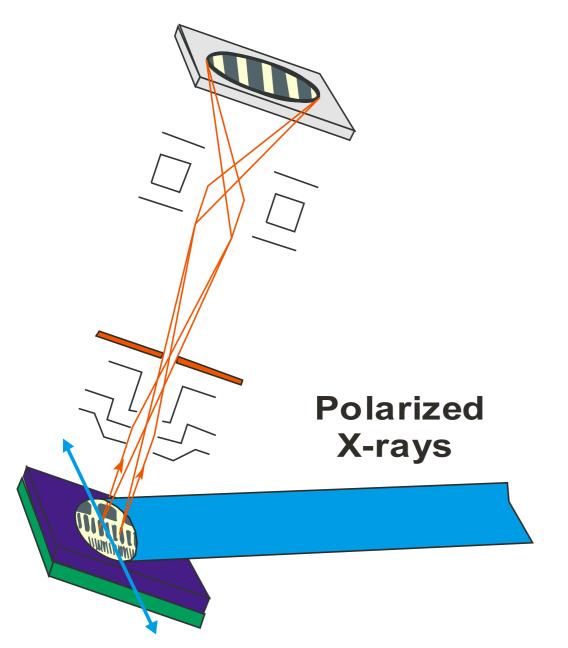


- Excitation of core electron into empty valence state by incoming X-ray
- Recombination (e.g.) by Auger decay

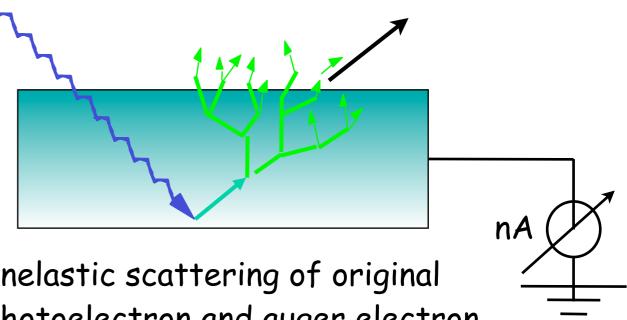


- Electron yield ~ X-ray absorption coefficient
- Probing depth ~ electron escape length $\exp(-\lambda t)$ with λ ~ 2 nm

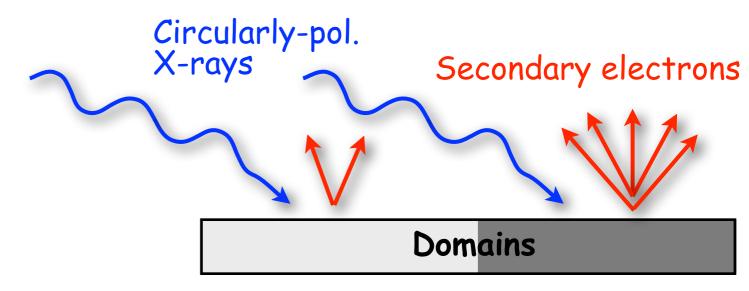


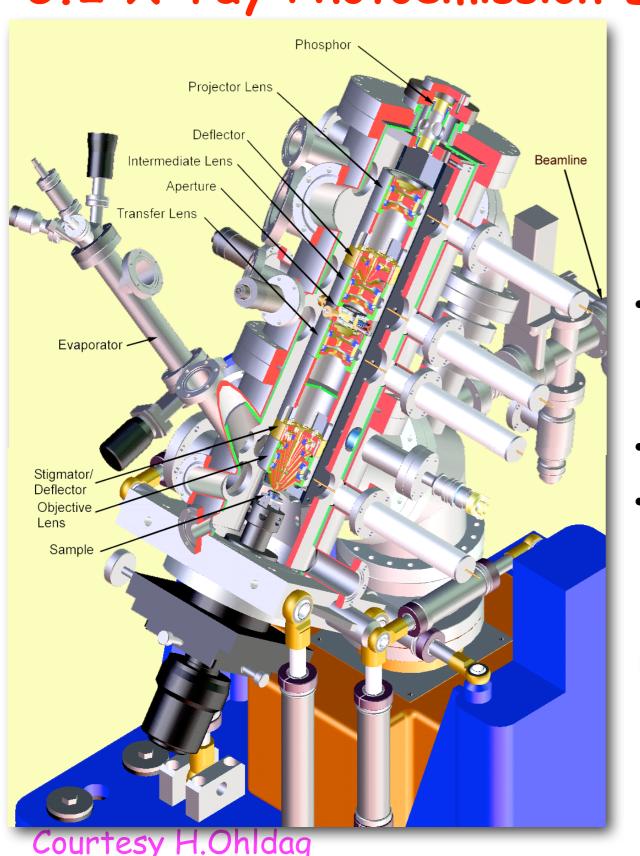


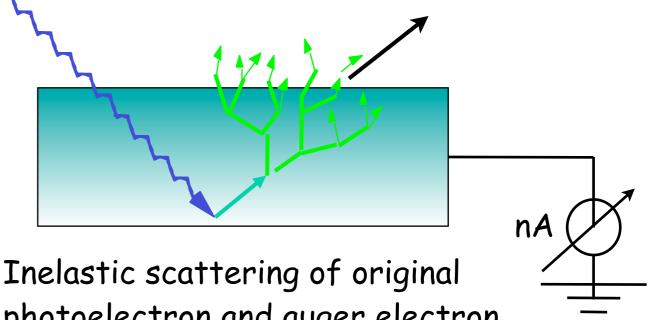
- Full Field Imaging
- 20 50 nm Resolution
- Linear and circular polarization



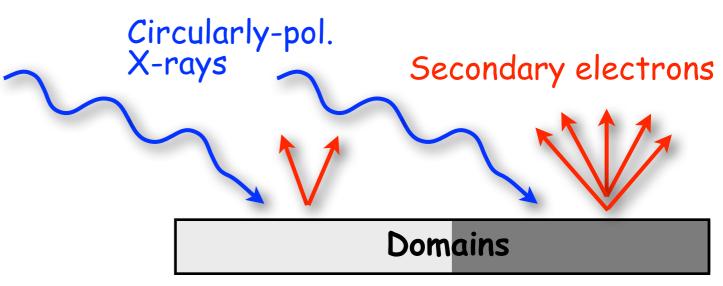
- Electron yield ~ X-ray absorption coefficient
- Probing depth ~ electron escape length $\exp(-\lambda t)$ with λ ~ 2 nm

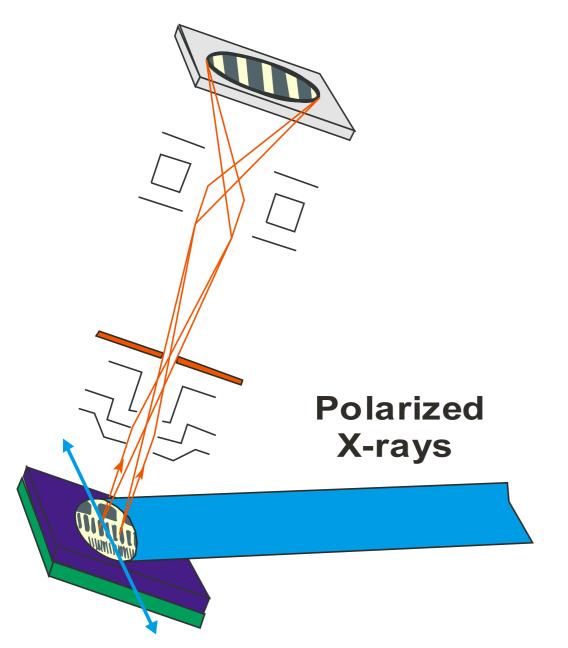




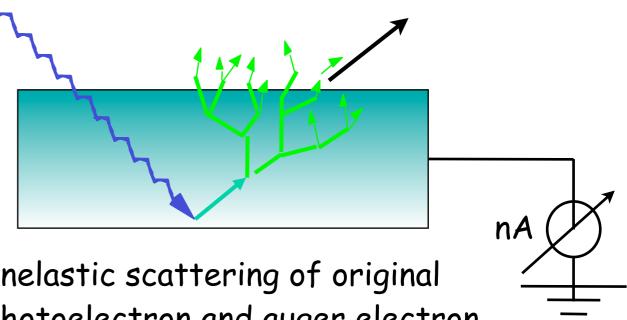


- Electron yield ~ X-ray absorption coefficient
- Probing depth ~ electron escape length $\exp(-\lambda t)$ with λ ~ 2 nm

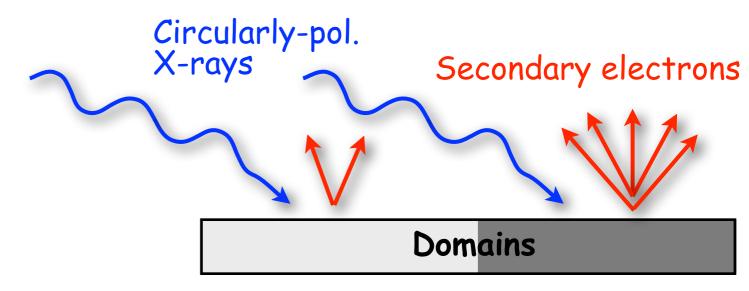




- Full Field Imaging
- 20 50 nm Resolution
- Linear and circular polarization

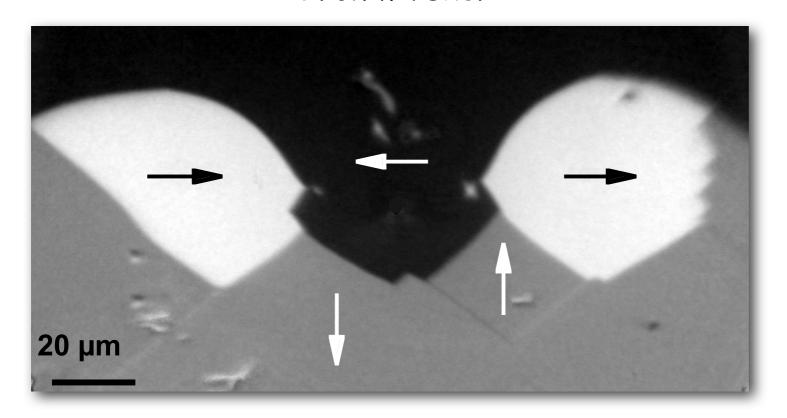


- Electron yield ~ X-ray absorption coefficient
- Probing depth ~ electron escape length $\exp(-\lambda t)$ with λ ~ 2 nm

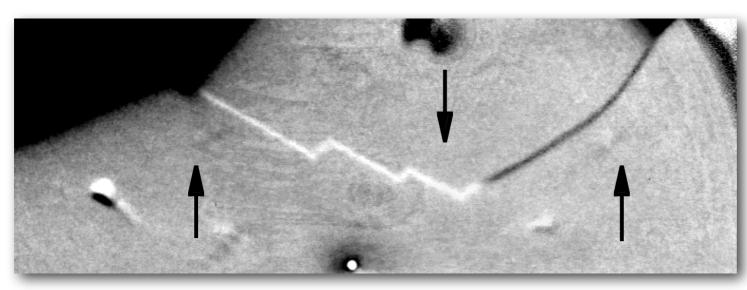


5.2 X-ray Photoemission Electron Microscopy (X-PEEM)

Iron whisker



Excitation by circularlypolarized electrons (MXCD)

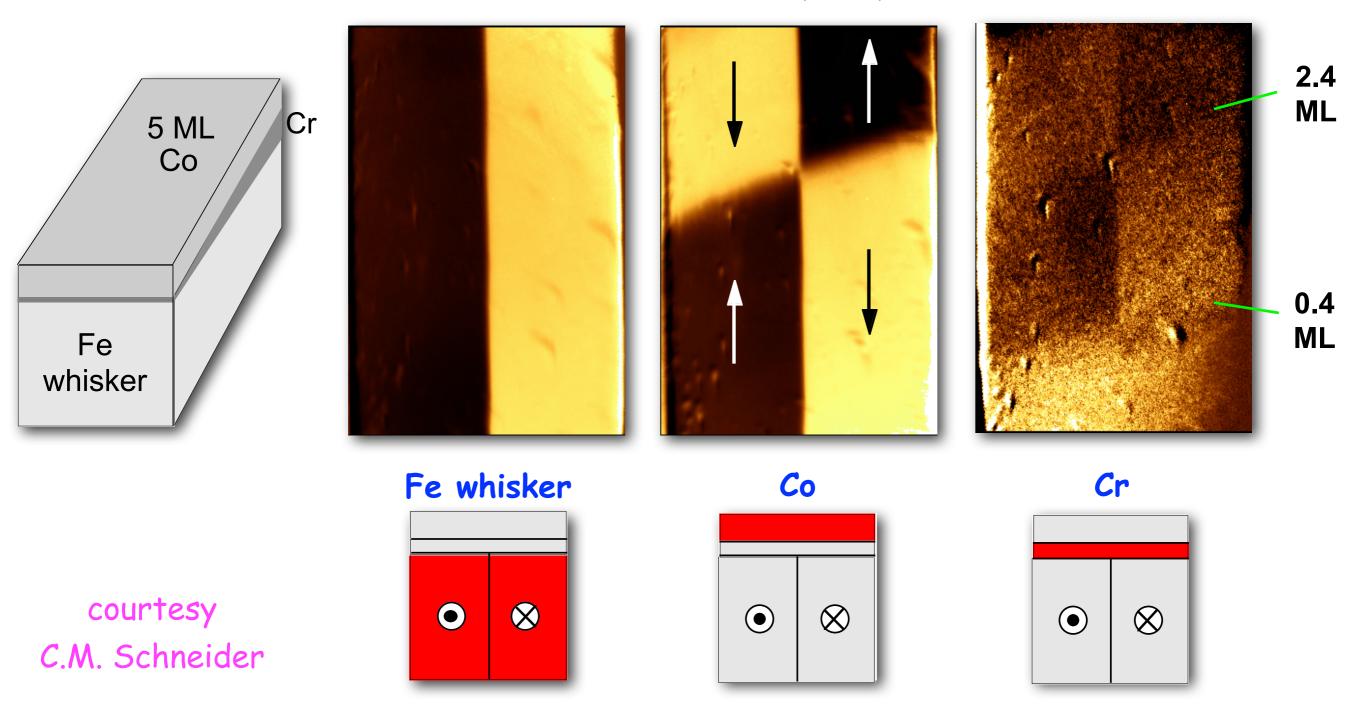


← → Sensitivity

Courtesy C.M. Schneider

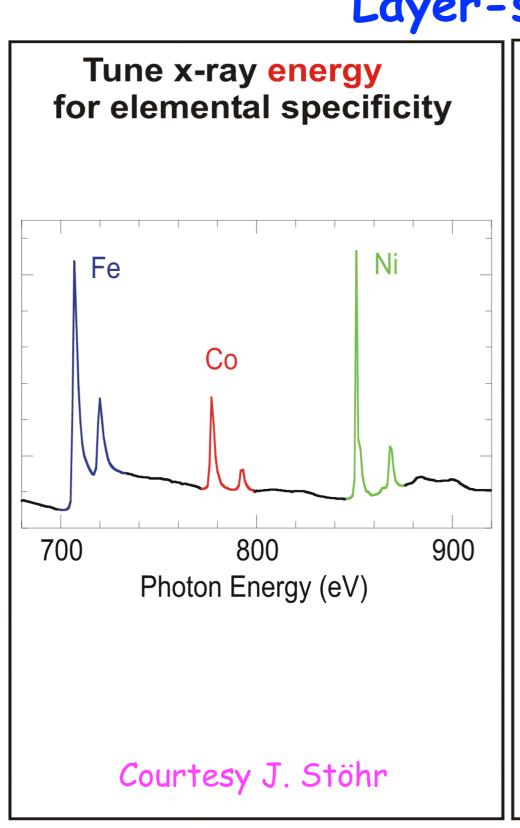
5.2 X-ray Photoemission Electron Microscopy (X-PEEM) Depth-selectivity by element-specific PEEM imaging

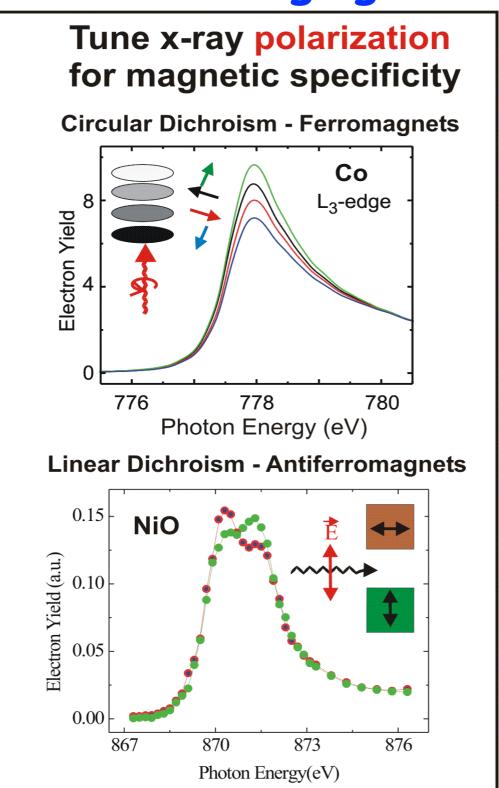
Fe-Cr-Co layer system



5.2 X-ray Photoemission Electron Microscopy (X-PEEM)

Layer-selective imaging





FeCo FeNi NiO

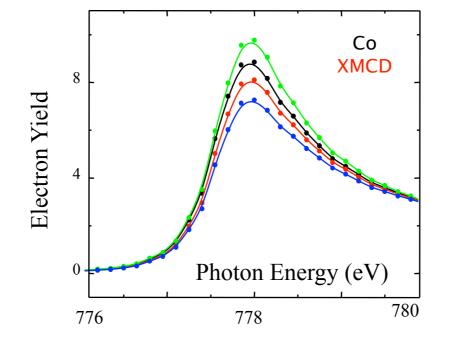
5.2 X-ray Photoemission Electron Microscopy (X-PEEM) Layer-selective imaging

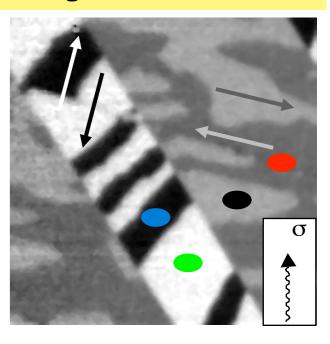
Tune to Co edge, use circular polarization: ferromagnetic domains

Circular polarization:
Sensitive to direction of magnetic moment

Co

NiO

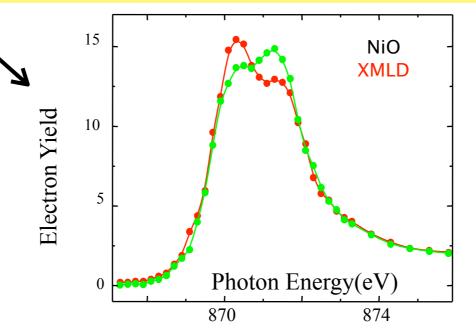


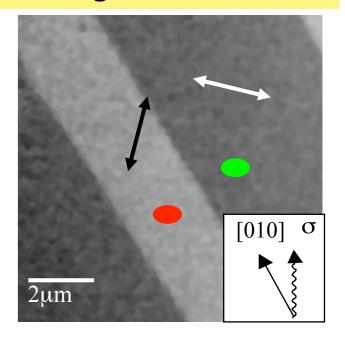


Tune to Ni edge, use linear polarization: antiferromagnetic domains

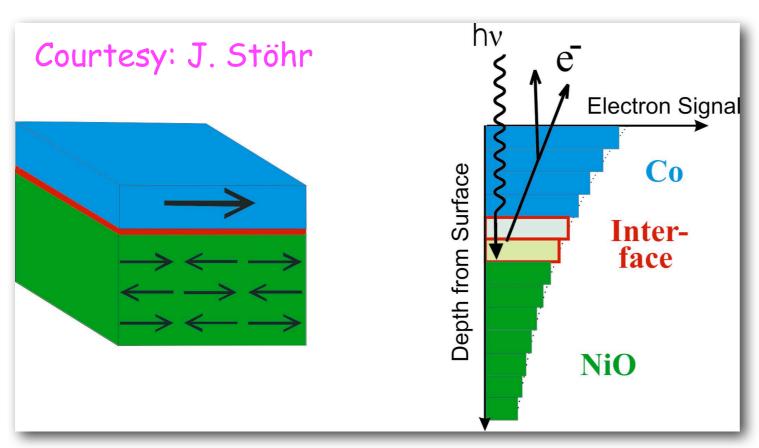
Linear polarization: Sensitive to axis of magnetic moment

H. Ohldag et al., PRL 86, 2878 (2001)





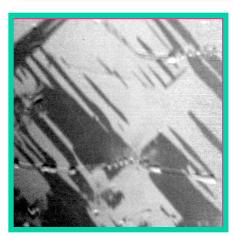
Interface studies of Ferromagnets on Antiferromagnets



FM Co - tune to Co edge - circular polarization

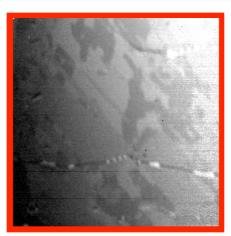
AFM NiO - tune to Ni edge - linear polarization

FM Ni(O) - tune to Ni edge - circular polarization



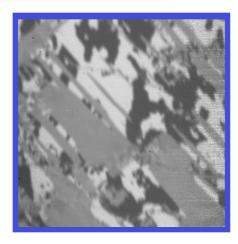
AFM: NiO

Linear pol. Ni edge



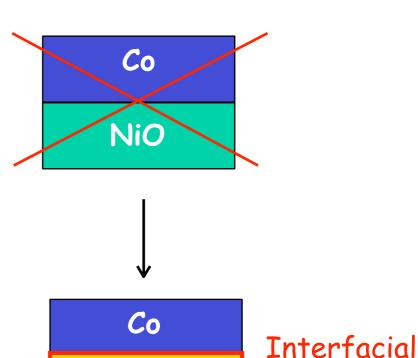
FM: Ni-rich NiO

Circular pol. Ni edge



FM: Co

Circular pol.
Co edge

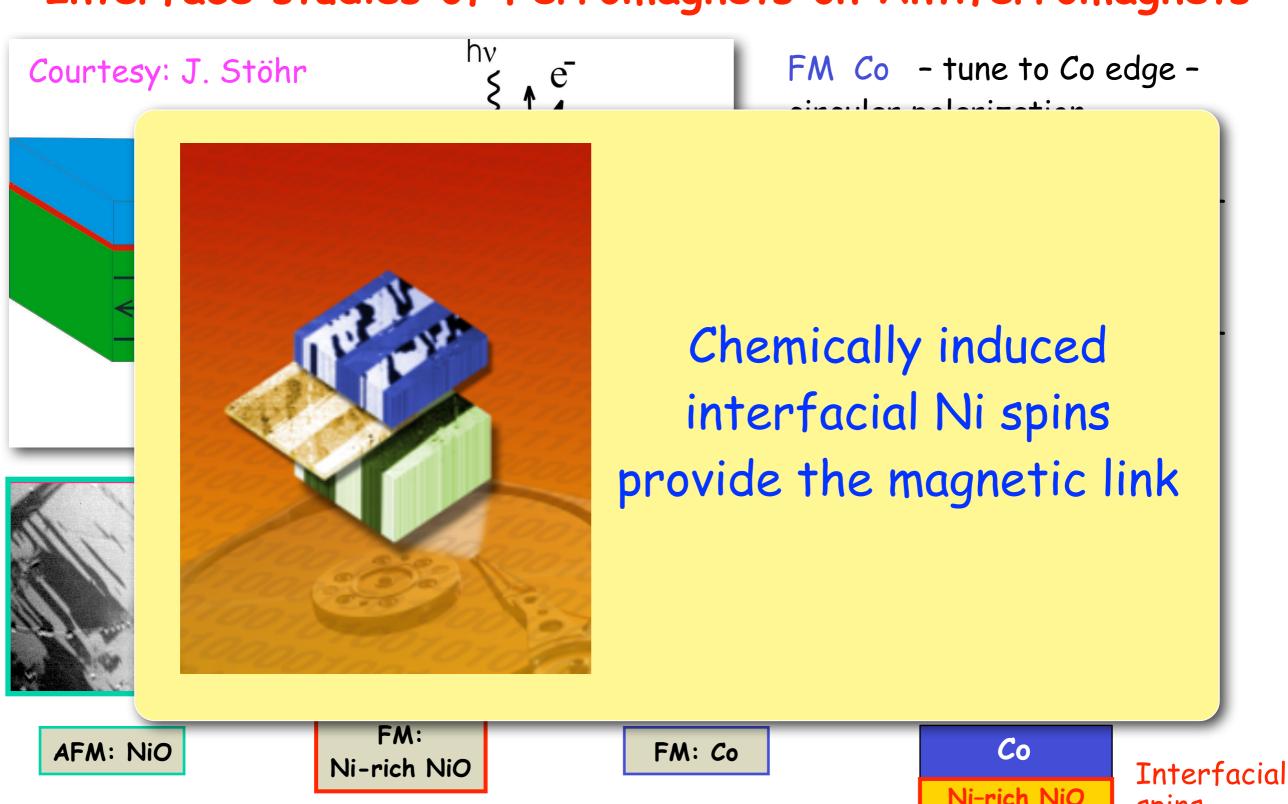


Ni-rich NiO

NiO

spins

Interface studies of Ferromagnets on Antiferromagnets



Linear pol. Ni edge

Circular pol. Ni edge

Circular pol. Co edge

Ni-rich NiO NiO

spins

Comparison of X-ray microscopy with PEEM imaging

Equal

- XMCD as contrast
- · element-specific
- · quantitative
- · in- and out-of-plane

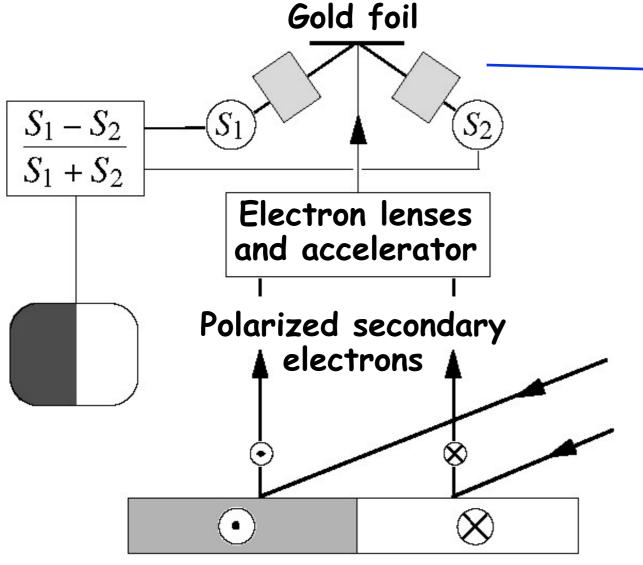
Advantages of PEEM

- no sample thinning
- · higher sensitivity
- · higher spectral resolution

Disadvantages of PEEM

- imaging in fields difficult
- · time consuming adjustment
- · lower standard resolution
- UHV conditions

6.1 Scanning Electron Microscopy with Polarization Analysis Gold foil (SEMPA)



Mott detector:

Scattering of polarized electrons by gold foil is asymmetric (spin-orbit coupling effects)

- · Secondary electrons are spin polarized, moment along magnetization direction
- Surface sensitive (secondary electrons emerge from top nanometer)
- Quantitative (independent measurement of 3 magnetization components)
- · Resolution in 10 nm range

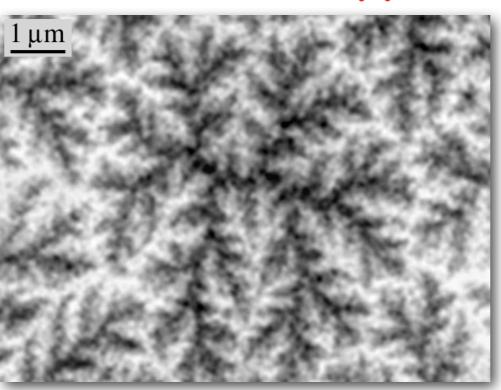
6.1 Scanning Electron Microscopy with Polarization Analysis

Basal plane of Co crystal

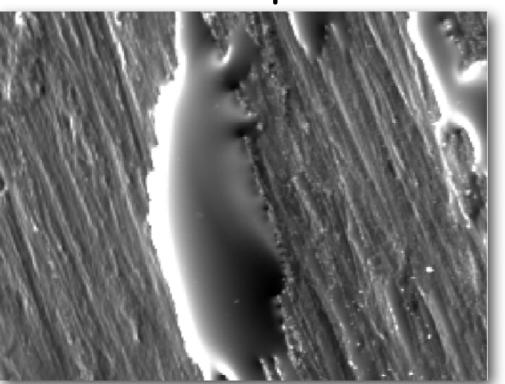


"Wheel side" of amorphous ribbon

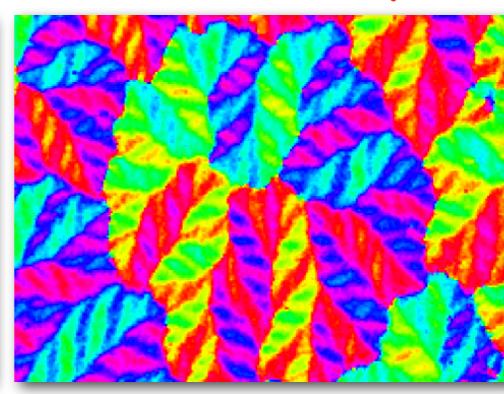
courtesy J. Unguris



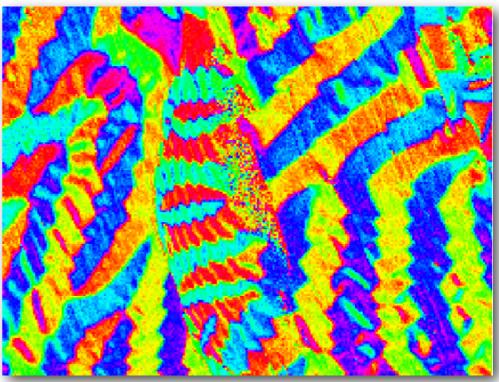
Polar components



Topography



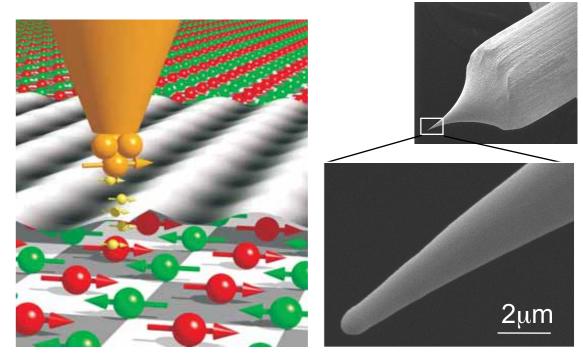
In-plane components



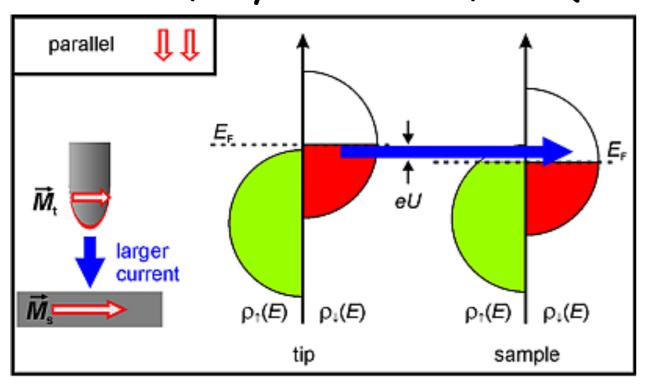
In-plane components

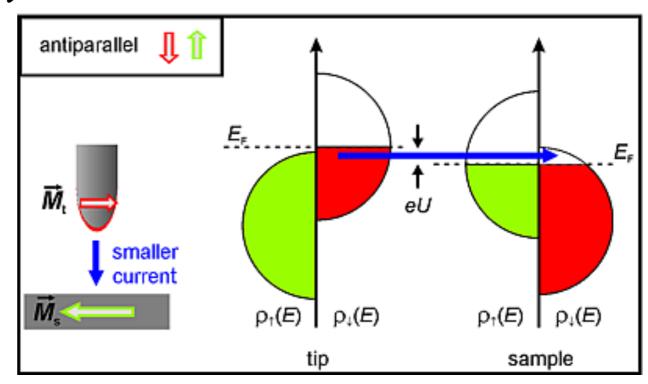
6.2 Spin-polarized Tunneling Microscopy

- Tunneling of spin-polarized current between tip and sample surface
- Tunneling resistance depends on relative orientation of current polarity and domain magnetization
- Extreme resolution



M. Julliere, Phys. Lett. 54A, 225 (1975):





from Wiesendanger homepage

http://www.nanoscience.de/nanojoom/index.php/en/methods/sp-stm.html

6.2 Spin-polarized Tunneling Microscopy

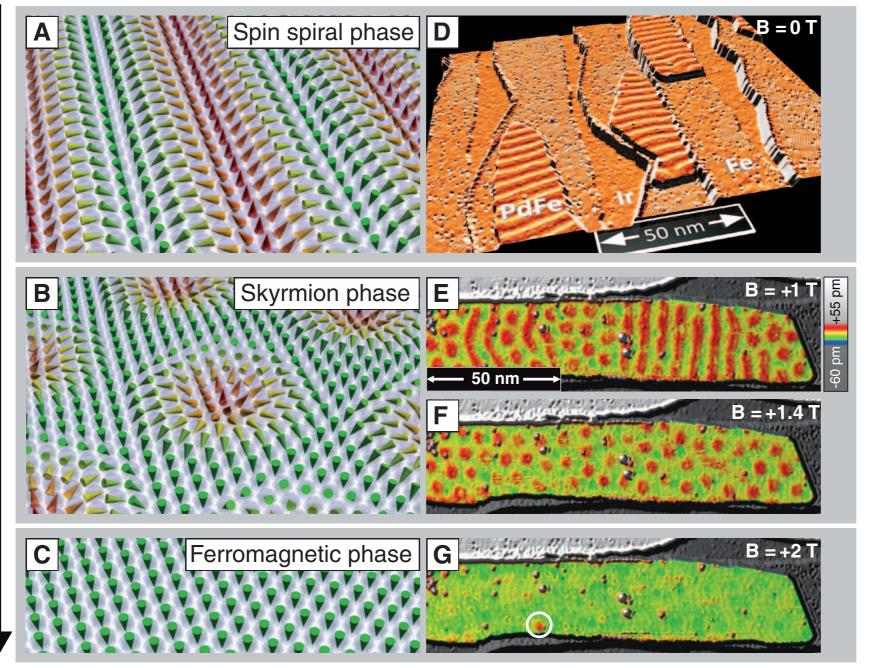


Fig. 1. Magnetic field dependence of the PdFe bilayer on the Ir(111) surface at T = 8 **K.** (**A** to **C**) Perspective sketches of the magnetic phases. (**D**) Overview SP-STM image, perspective view of constant-current image colorized with its derivative. (**E** to **G**) PdFe bilayer at different magnetic fields (U = +50 mV, I = 0.2 nA, magnetically out-of-plane sensitive tip). (E) Coexistence of spin spiral and skyrmion phase. (F) Pure skyrmion phase. (G) Ferromagnetic phase. A remaining skyrmion is marked by the white circle.



Writing and Deleting Single Magnetic Skyrmions.
Niklas Romming et al.
Science 341, 636 (2013);
DOI: 10.1126/science.
1240573

Sensitivity of imaging methods

$$\mathbf{B} = \mu_0 (\mathbf{H} + \mathbf{M})$$
 $(\mathbf{H} = \mathbf{H}_{ext} + \mathbf{H}_{stray})$
 $\operatorname{div} \mathbf{B} = 0$
 $\operatorname{div} \mathbf{H}_{stray} = -\operatorname{div} \mathbf{M}$

• Sensitive to H_{stray}

· Sensitive to M

- · Sensitive to B
- Sensitive to distortions

- 1. Bitter technique
- 2. Magnetic force microscopy
- 3. Hall probe microscopy
- 4. Magneto-optical microscopy
- 5. X-ray spectroscopy
- 6. Polarized electrons (SEMPA, SPT)
- Transmission electron microscopy
- X-ray, neutron scattering

Sensitivity of imaging methods

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- 6. Polarized electrons (SEMPA, SPT)
- 7. Transmission electron microscopy
- X-ray, neutron scattering

Principle

· Electrons are deflected by Lorentz force

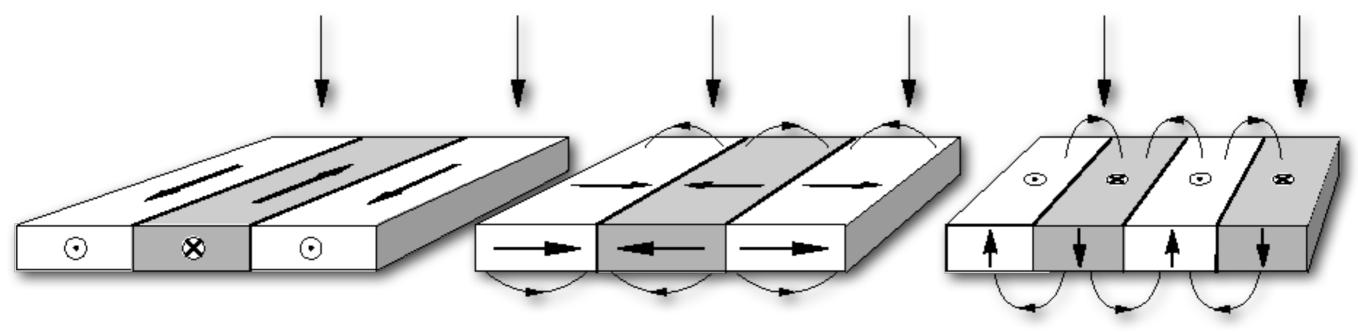
$$F_{L} = q_{e} (v_{e} \times B)$$

 q_e : Electron charge

 v_e : Electron velocity

B: Magnetic flux density

· Stray fields outside the sample contribute to contrast



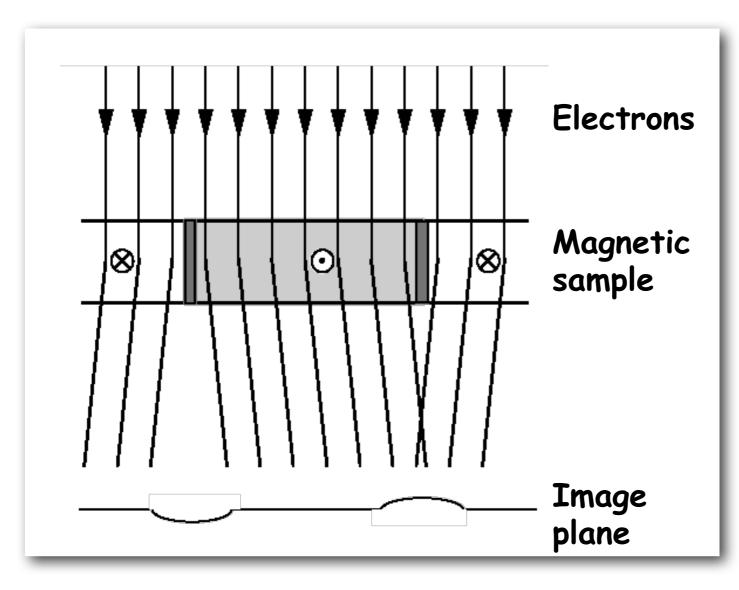
Net deflection of electrons

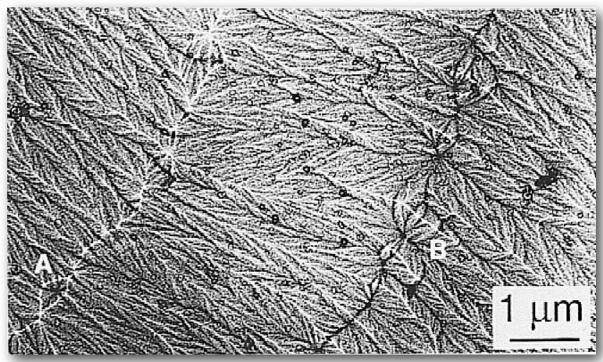
Deflection by magnetization is canceled by deflections due to stray field

No deflection by magnetization, stray field deflection cancels

- Tilting of sample may be required
- Maximum sample thickness: some 100 nm

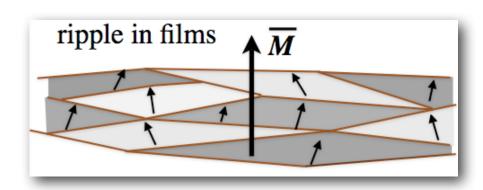
7.1 Fresnel technique (defocused mode imaging)





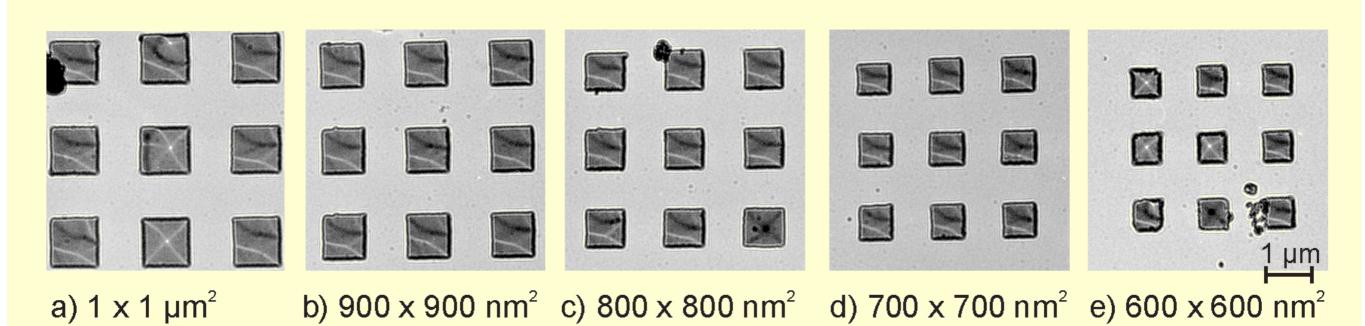
Metallic glass, partially crystallized (courtesy J. Chapman)

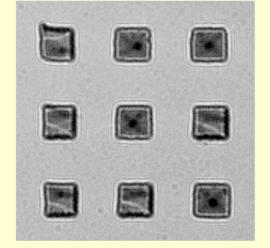
- · Out-of-focus: shadow effects delineate domain boundaries
- Magnetization direction can be derived from ripple (if present)

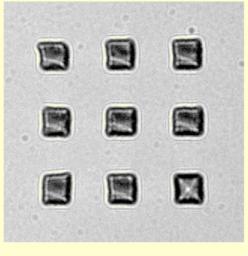


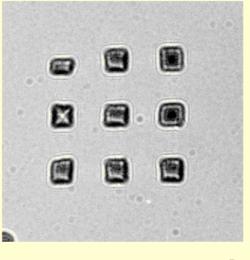
7.1 Fresnel technique (defocused mode imaging)

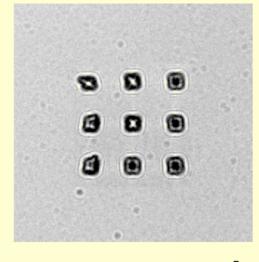
Fresnel imaging of differently sized magnetic particles (Co, 35 nm thick)

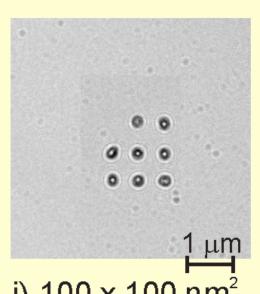






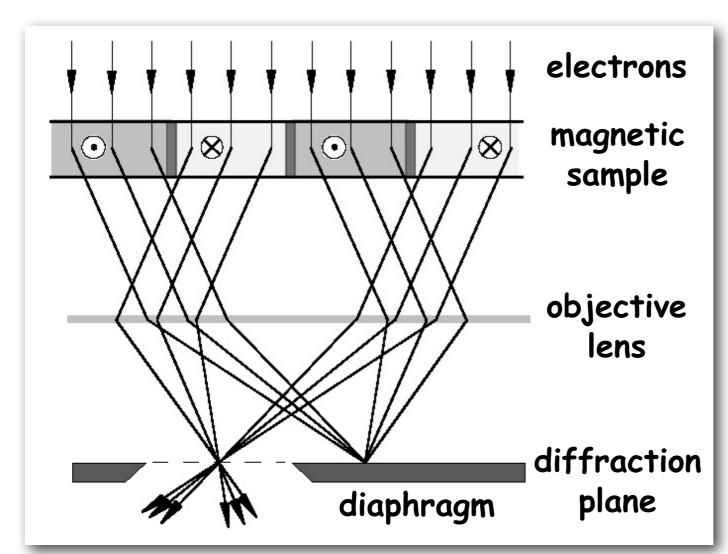


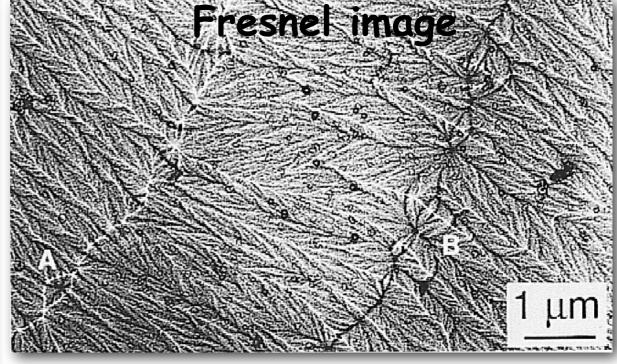


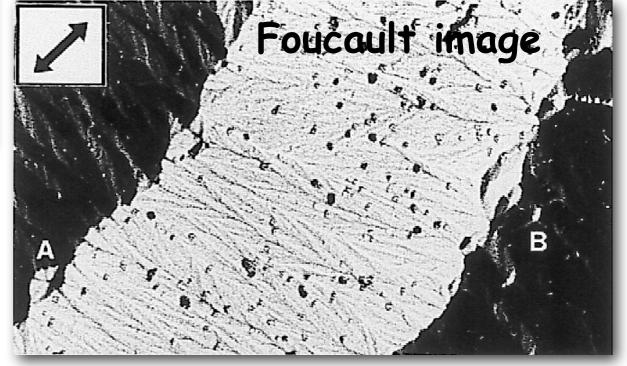


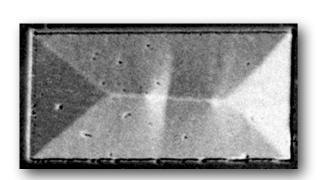
f) 500 x 500 nm² g) 400 x 400 nm² h) 300 x 300 nm² i) 200 x 200 nm² j) 100 x 100 nm²

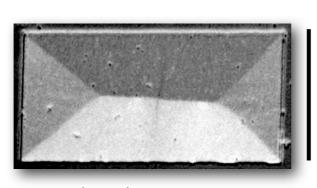
7.2 Foucault technique (in-focus)









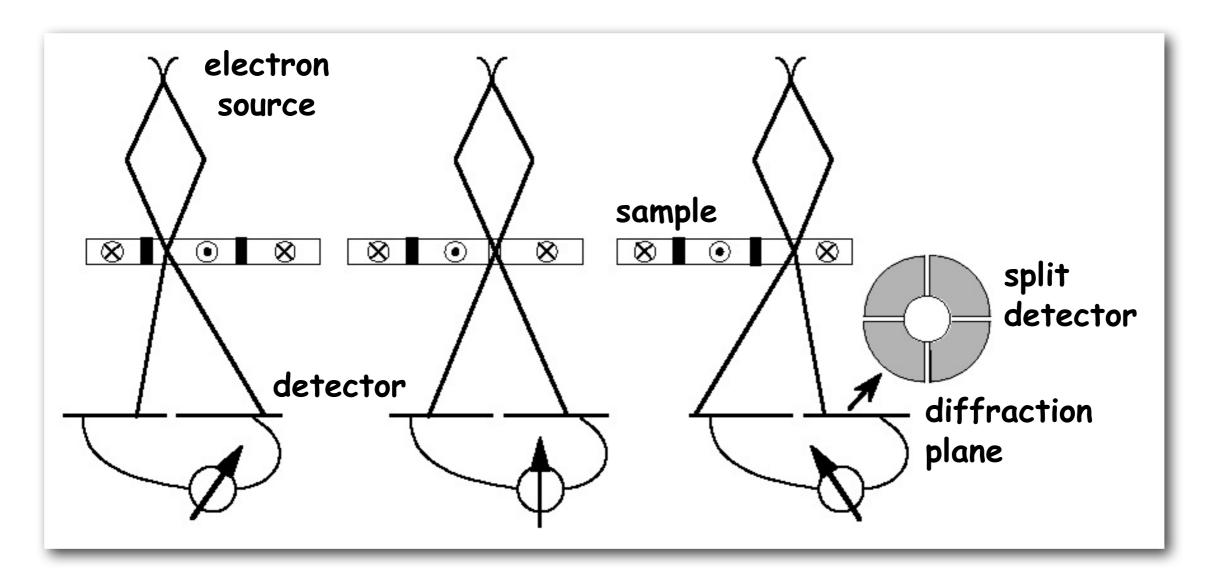


 $2\;\mu m$

Permalloy, 24 nm thick (courtesy J. Chapman)

Metallic glass, partially crystallized (courtesy J. Chapman)

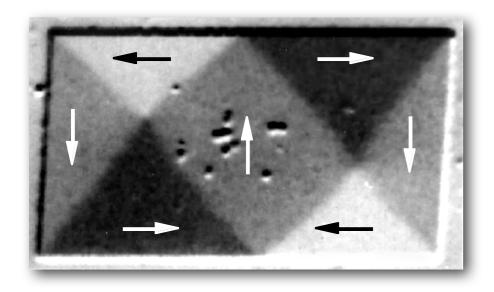
7.3 Differential Phase Contrast (DPC) Microscopy

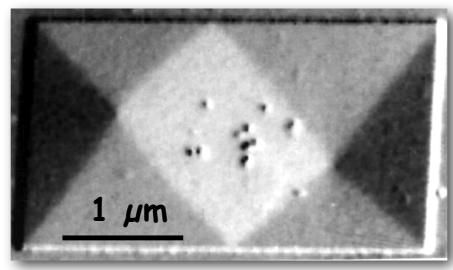


- Domain contrast like in Kerr microscopy
- Resolution better than 10 nm
- Quantitative determination of magnetization direction (by combining signals of a quadrant detector)

7.3 Differential Phase Contrast (DPC) Microscopy

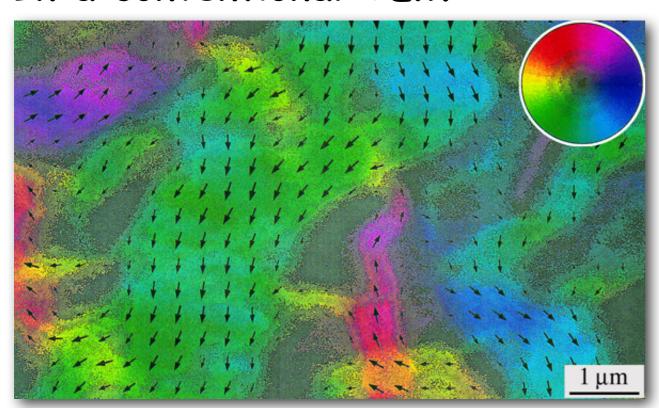
In a scanning TEM





Permalloy, 60 nm thick (courtesy J. Chapman)

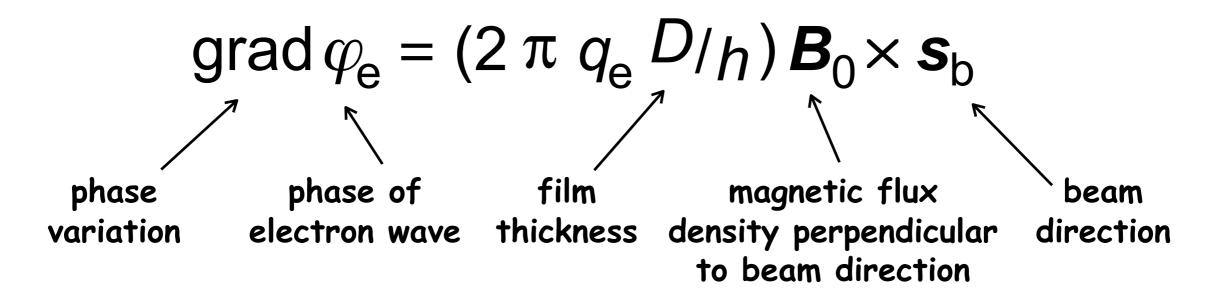
In a conventional TEM



AFM coupled Co-Cr-Co sandwich (courtesy J.P. Jakubovics)

Difference between Foucault images, obtained at different angles of incidence

7.4 Electron Holography Principle



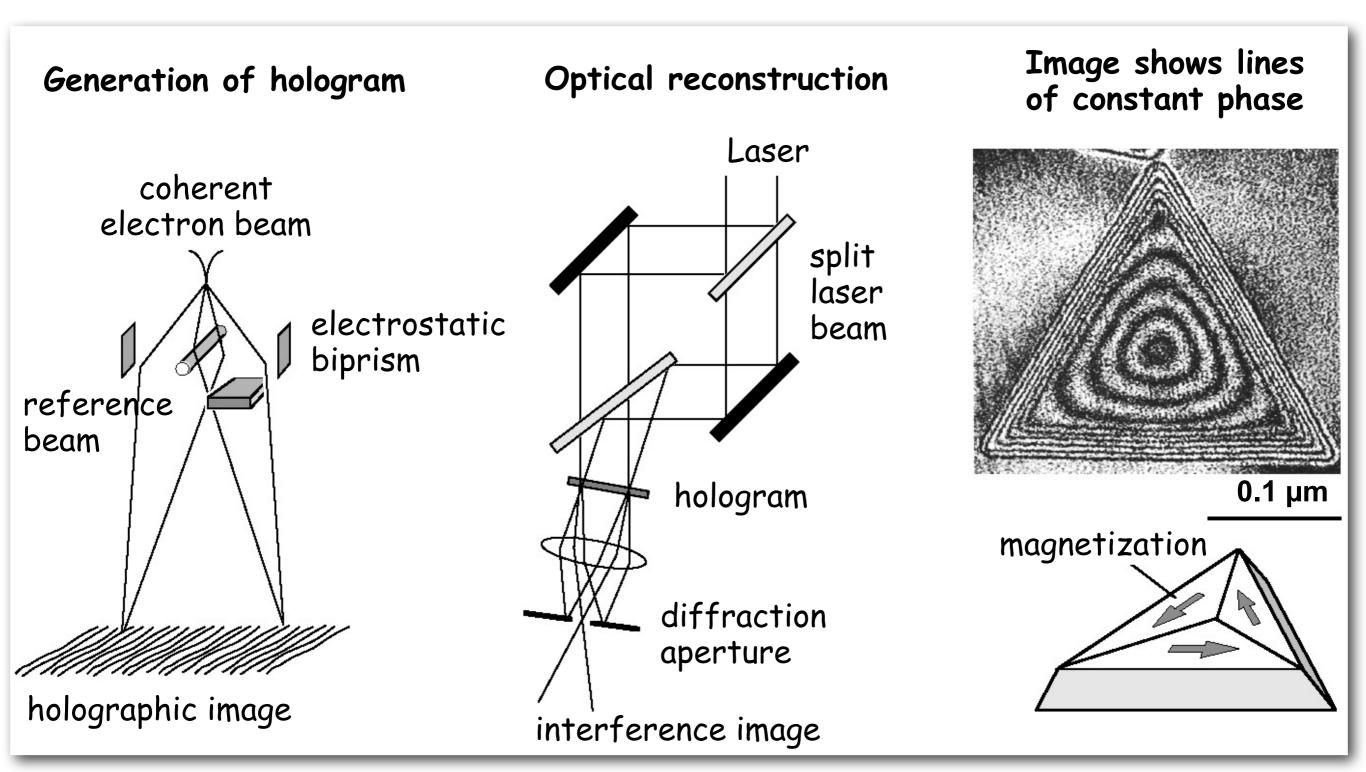
- · Magnetization influences phase of electron wave
- Phase gradient is perpendicular to B_0
- Lines of constant phase are parallel to B_0
- Flux between two lines is equal to flux quantum $h/q_{\rm e}$

Electron Holography:

- Interference pattern of 2 electron waves shifted in phase
- Evaluation in optical interferometer

7.4 Electron Holography

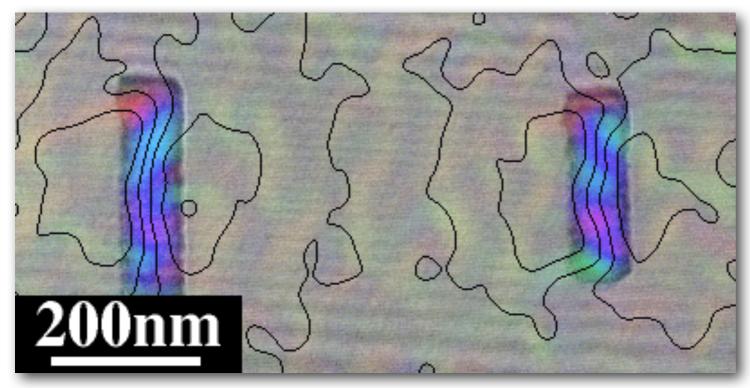
Off-axis holography (Tonomura et al. 1980)



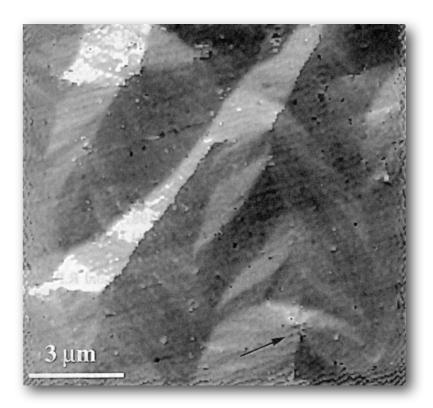
7.4 Electron Holography

Differential Holography (Mankos et al. 1994)

- Both interfering beams pass through sample along slightly different paths (distance: 10 nm)
- Reconstruction contains information about their phase difference
 - -> phase gradient is recorded, which is proportional to magnetization
 - -> "real" domain images like in Kerr microscopy
- · Quantitative information about magnetization direction at high resolution



Co/Au/Ni/Al multilayer (courtesy M. McCartney)



30 nm Co film (courtesy M. Scheinfein)

Sensitivity of imaging methods

$$\mathbf{B} = \mu_0 (\mathbf{H} + \mathbf{M})$$
 $(\mathbf{H} = \mathbf{H}_{ext} + \mathbf{H}_{stray})$
 $\operatorname{div} \mathbf{B} = 0$
 $\operatorname{div} \mathbf{H}_{stray} = -\operatorname{div} \mathbf{M}$

• Sensitive to H_{stray}

· Sensitive to M

- · Sensitive to B
- Sensitive to distortions

- 1. Bitter technique
- 2. Magnetic force microscopy
- 3. Hall probe microscopy
- 4. Magneto-optical microscopy
- 5. X-ray spectroscopy
- 6. Polarized electrons (SEMPA, SPT)
- 7. Transmission electron microscopy
- X-ray, neutron scattering

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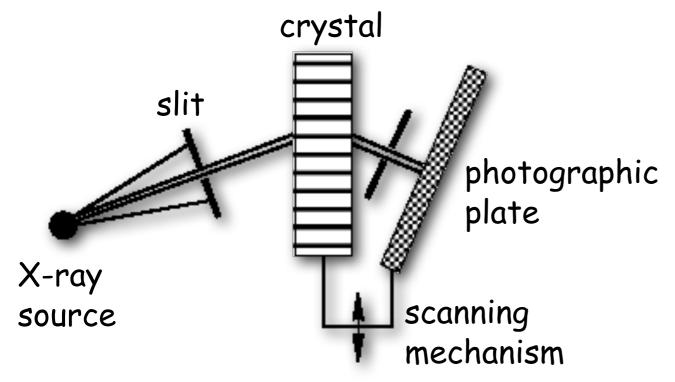
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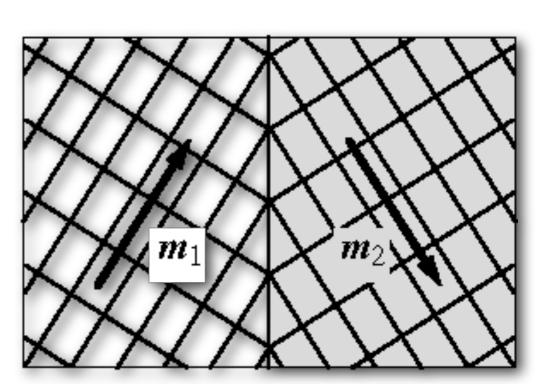
8.1 X-ray Topography

- · Plane-parallel X-ray beam, restricted to narrow strip
- Bragg condition fulfilled for some set of lattice planes
- Diffracted beam recorded by photographic plate
- · Crystal and plate are advanced synchronously (scanning)

Contrast mechanism:

- Magnetostrictive strains disturb Bragg reflection
- · Contrast at those positions, where rotation or spacing of lattice changes

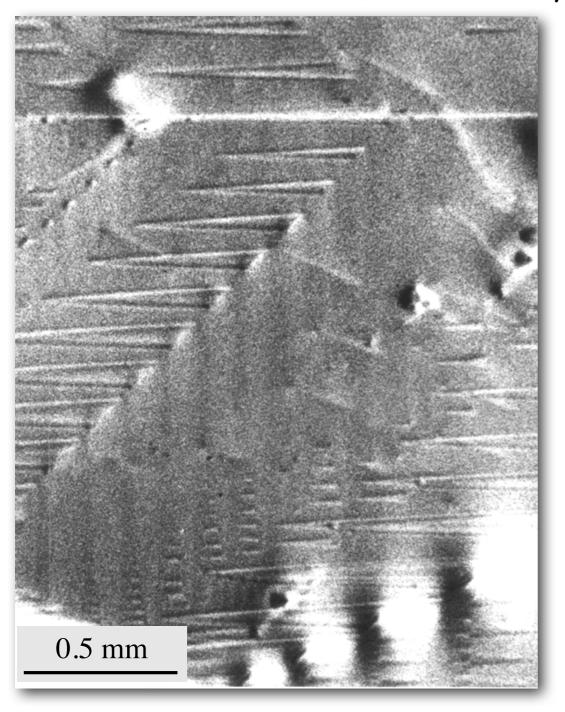


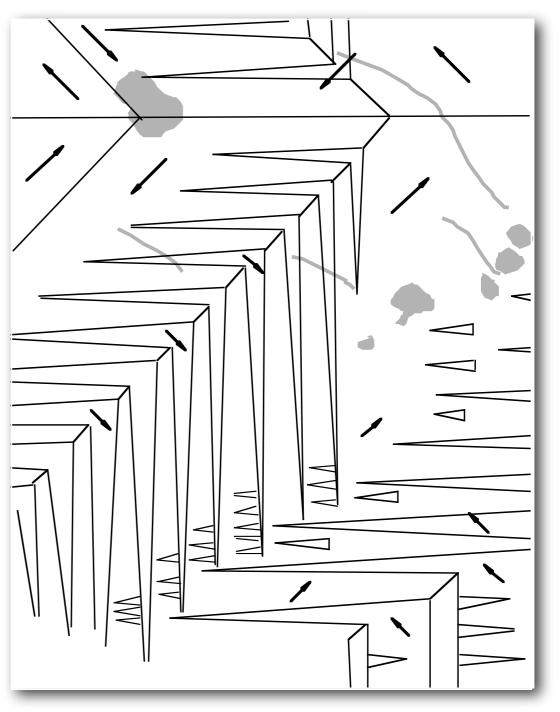


Change of lattice orientation at 90° wall (10 - 5 radian)

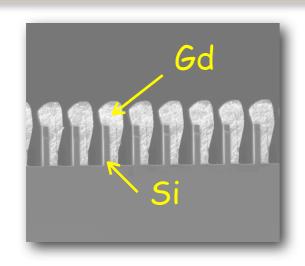
8.1 X-ray Topography

X-ray topogram of fir-tree domains on slightly misoriented (100) FeSi crystal (0.1 mm thick)

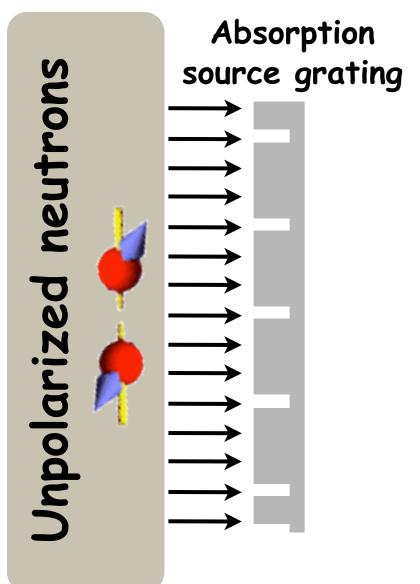




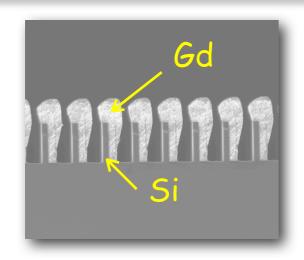
(Courtesy J. Miltat)



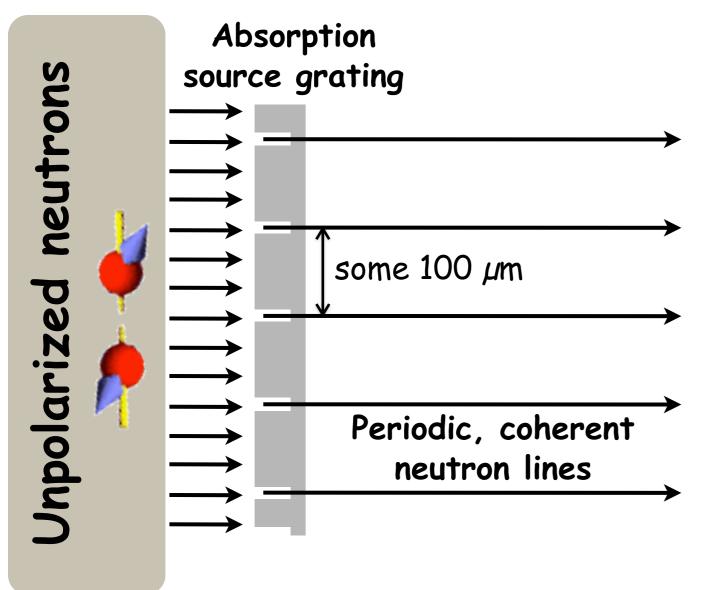
C. Grünzweig, et al., Phys. Rev. Lett. 101, 025504 (2008)



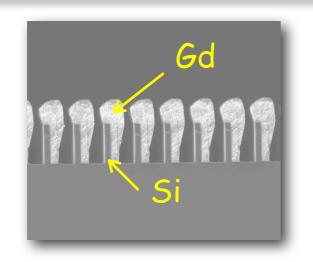
Imaae detektor

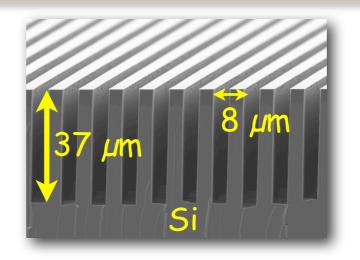


C. Grünzweig, et al., Phys. Rev. Lett. 101, 025504 (2008)



Imaae detektor





C. Grünzweig, et al., Phys. Rev. Lett. 101, 025504 (2008)

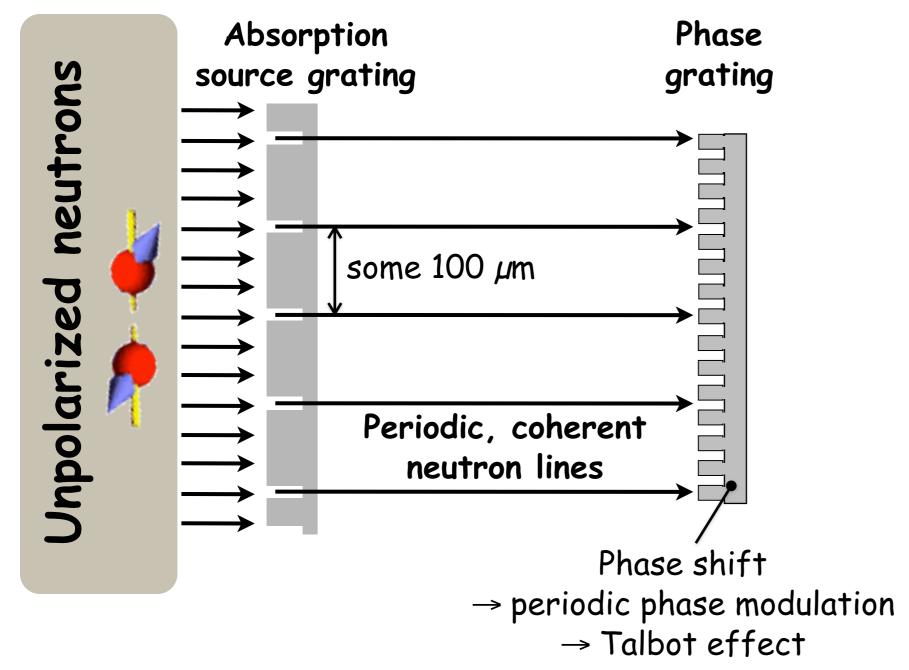
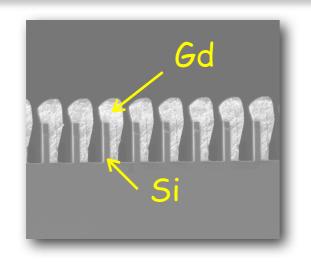
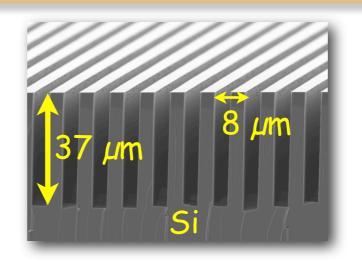
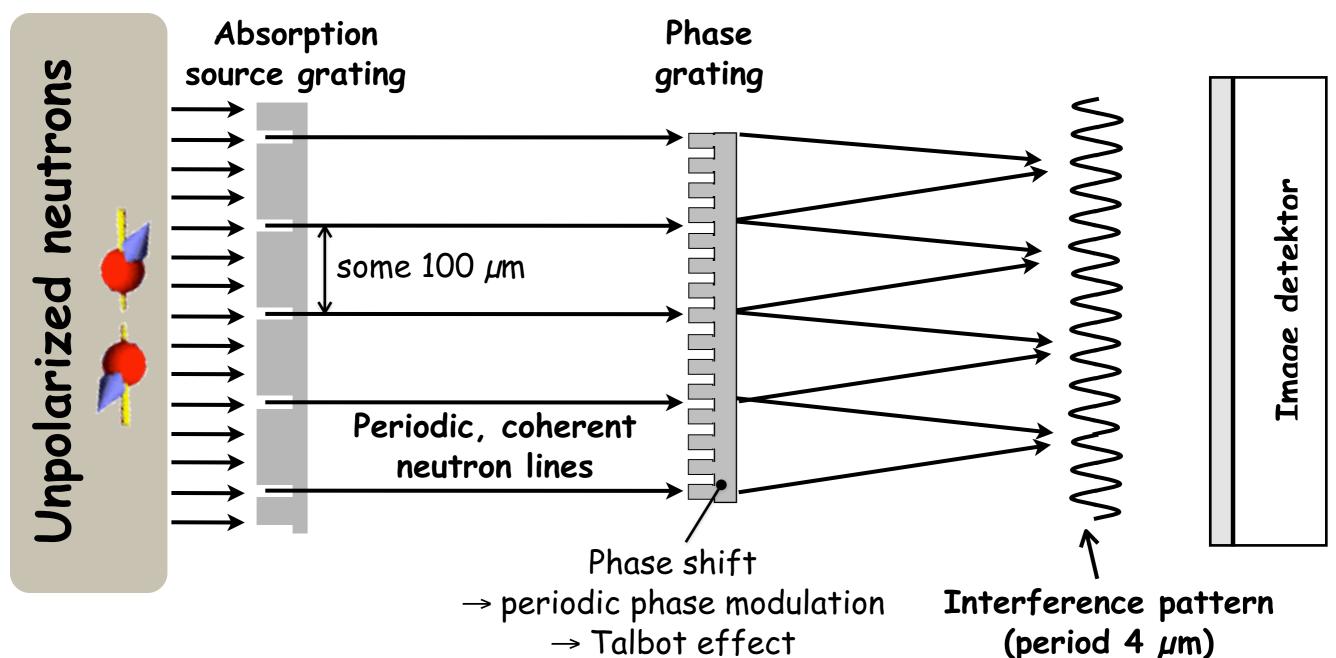


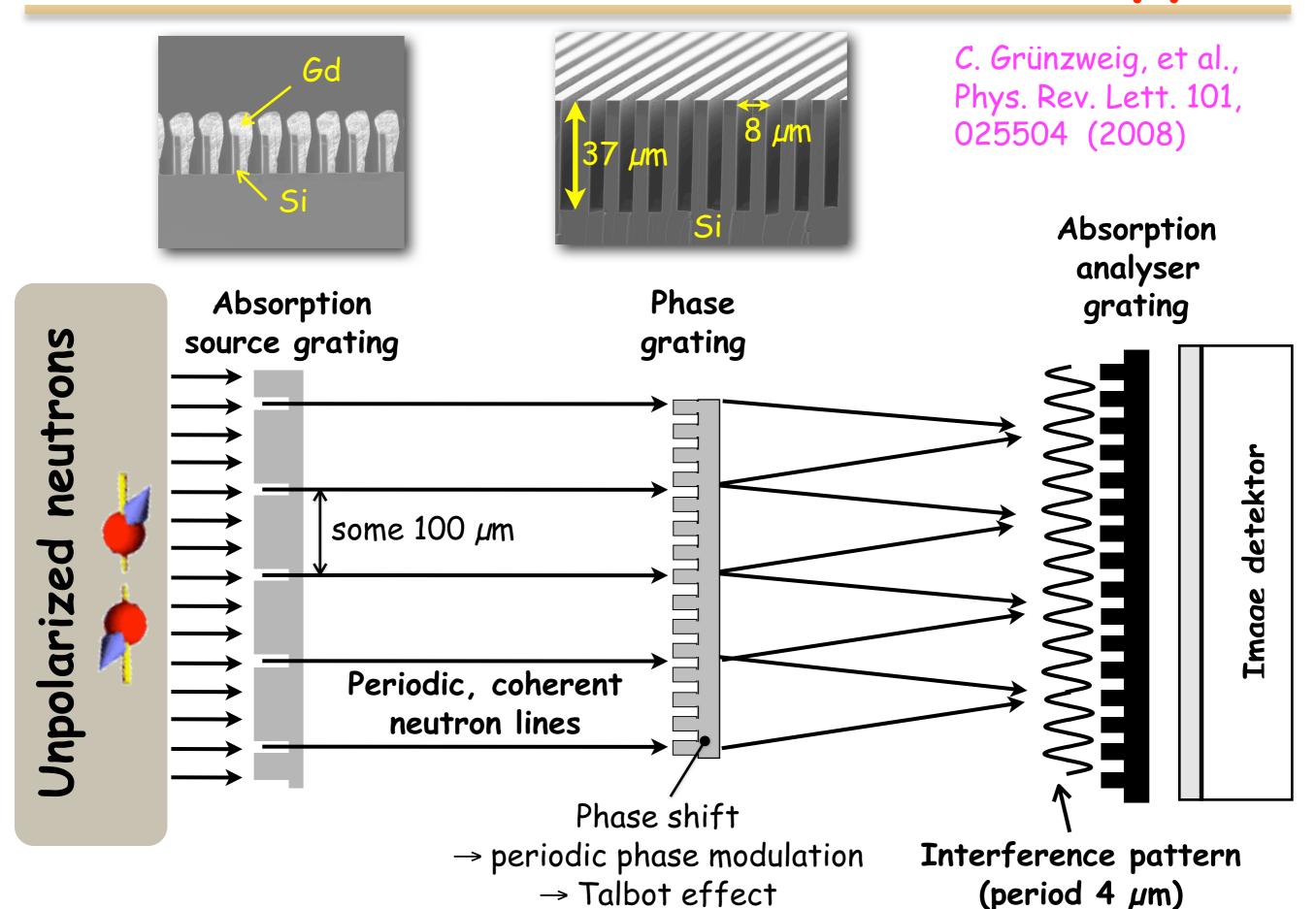
Image detektor

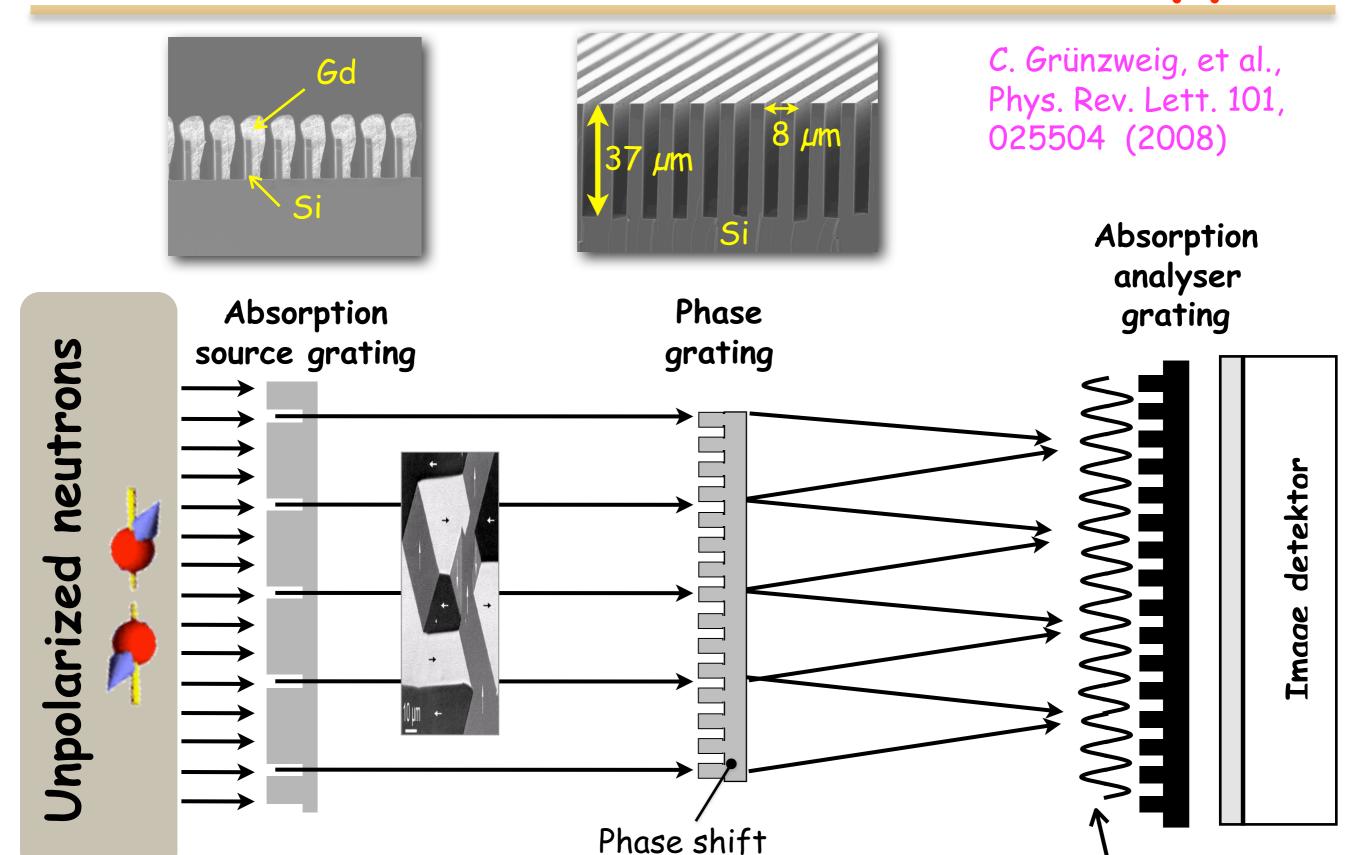




C. Grünzweig, et al., Phys. Rev. Lett. 101, 025504 (2008)



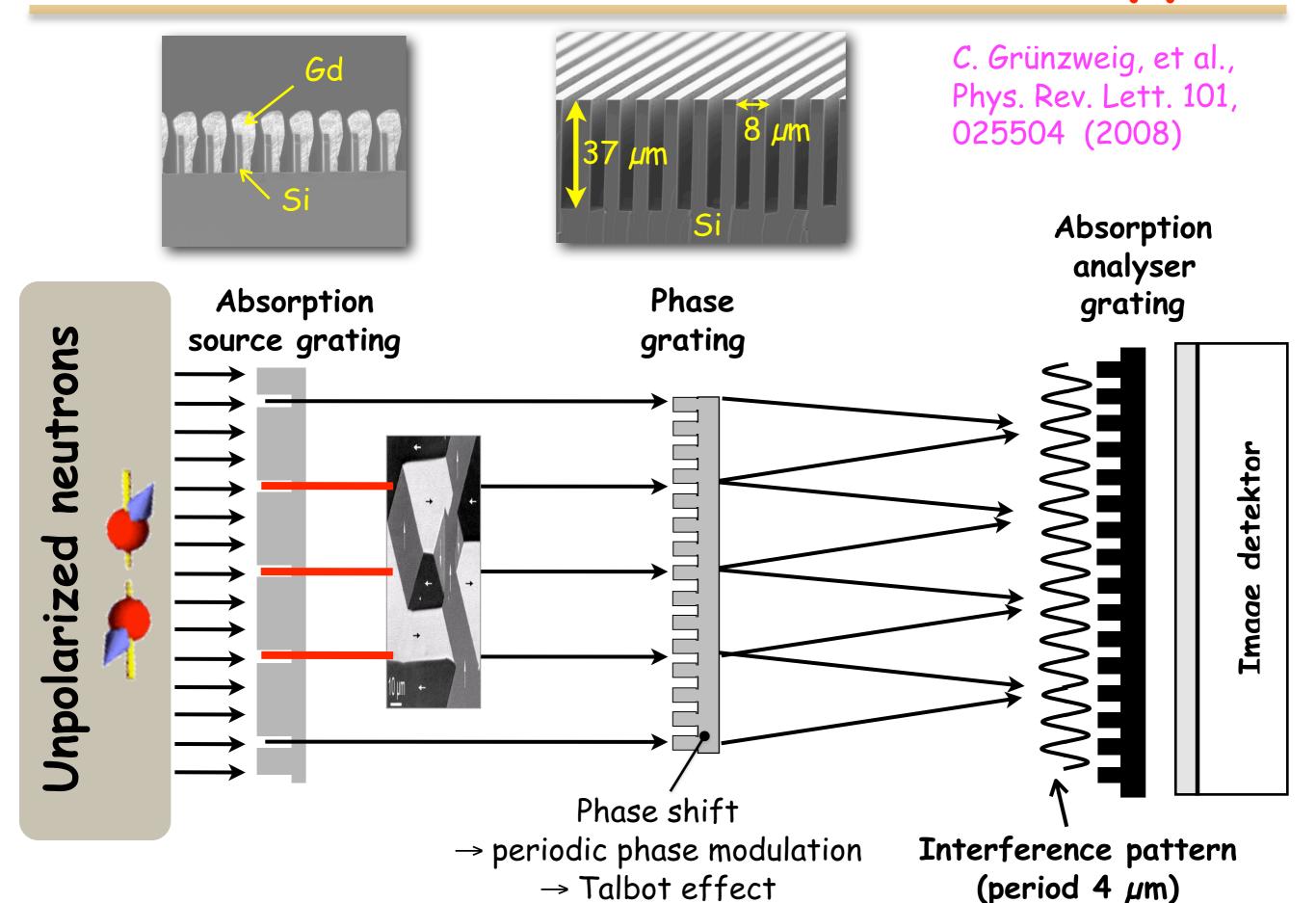


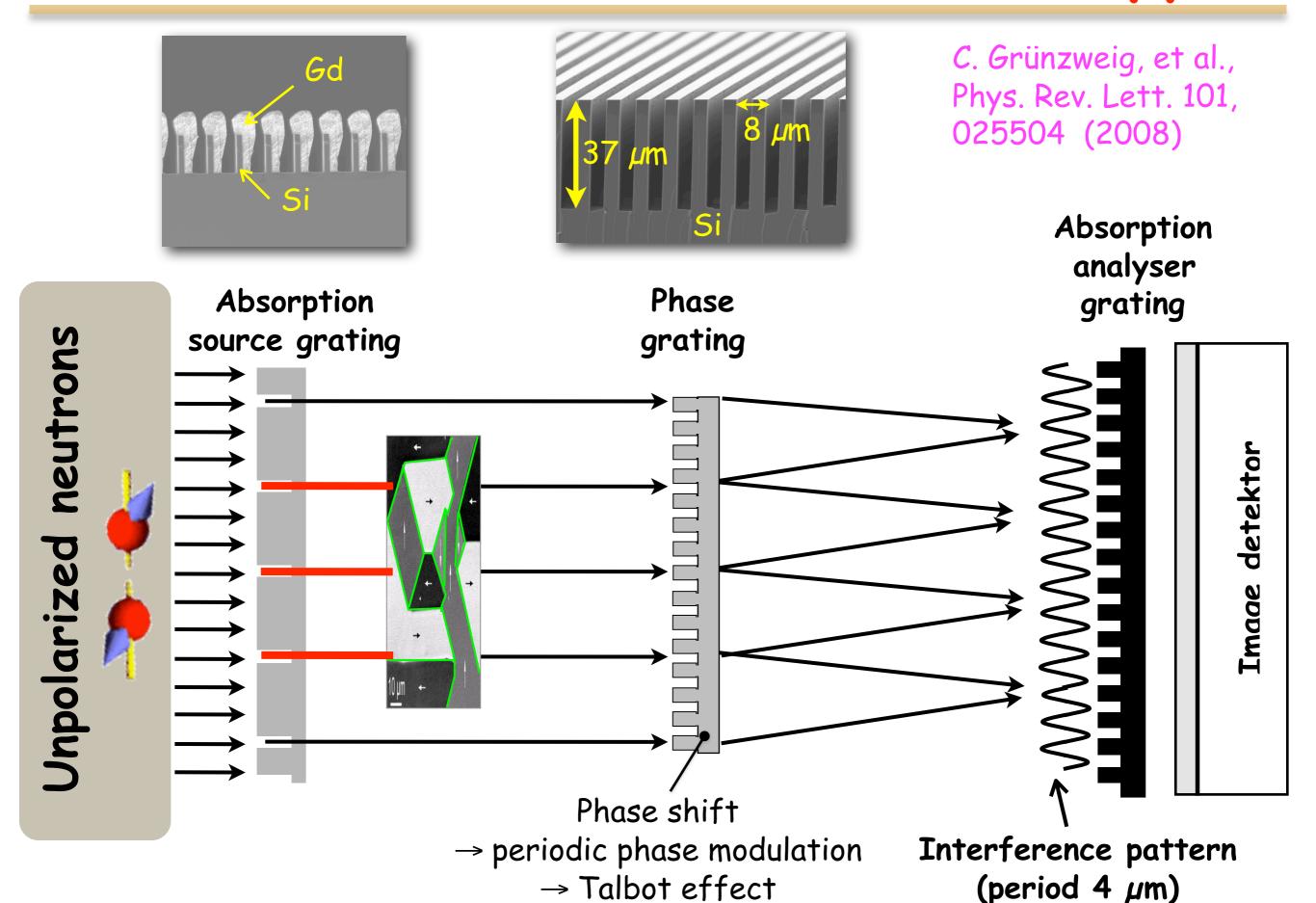


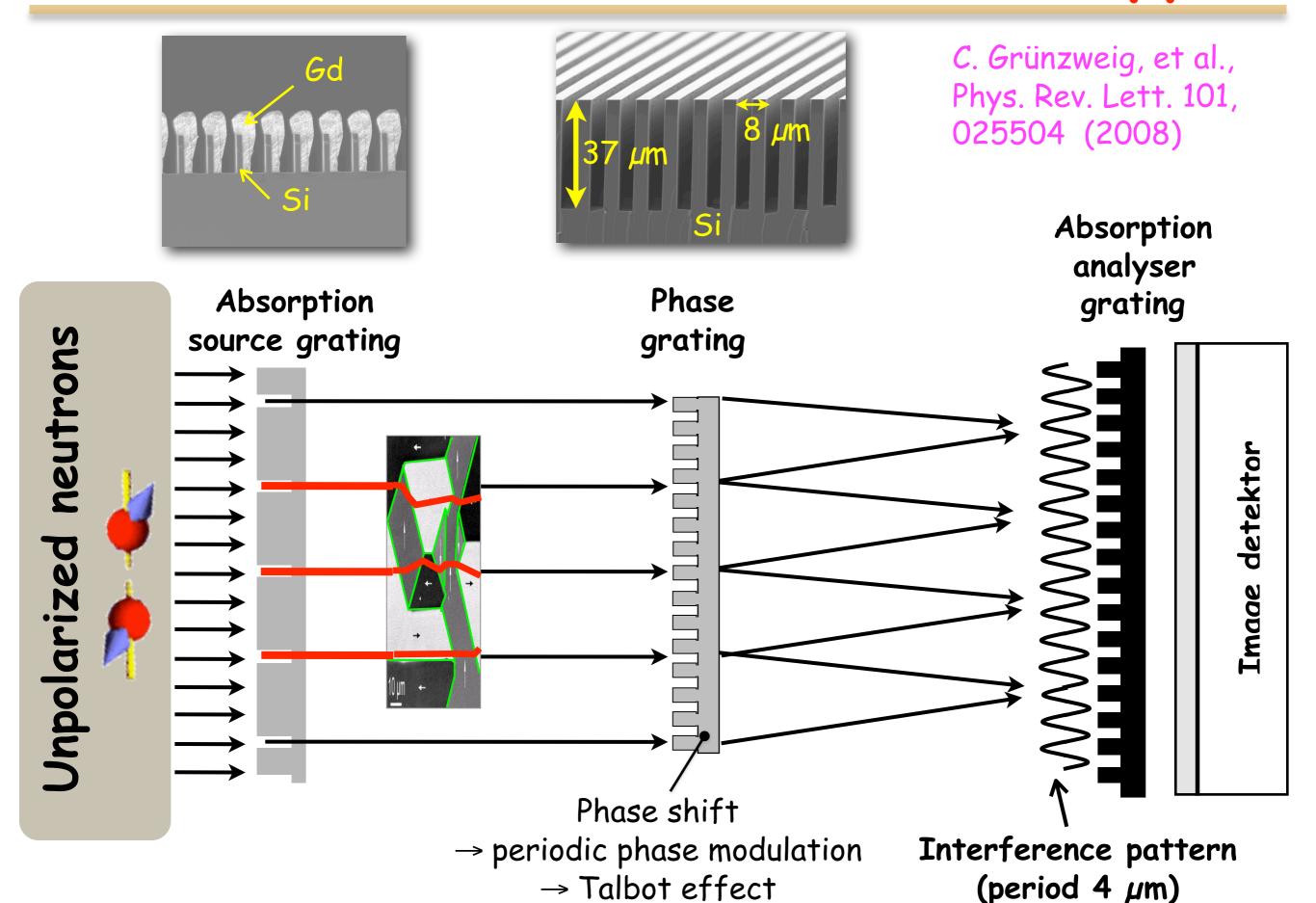
→ periodic phase modulation

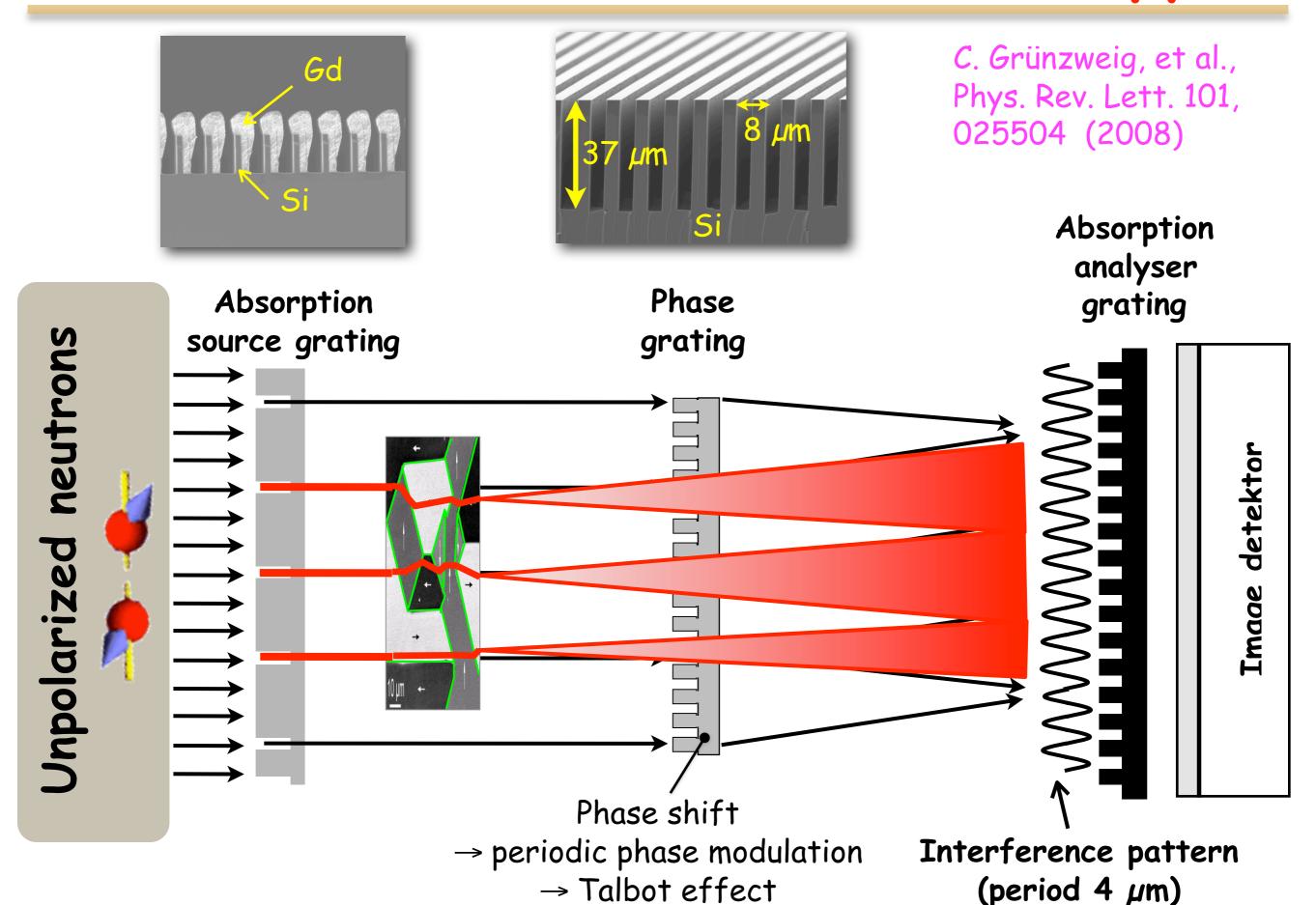
→ Talbot effect

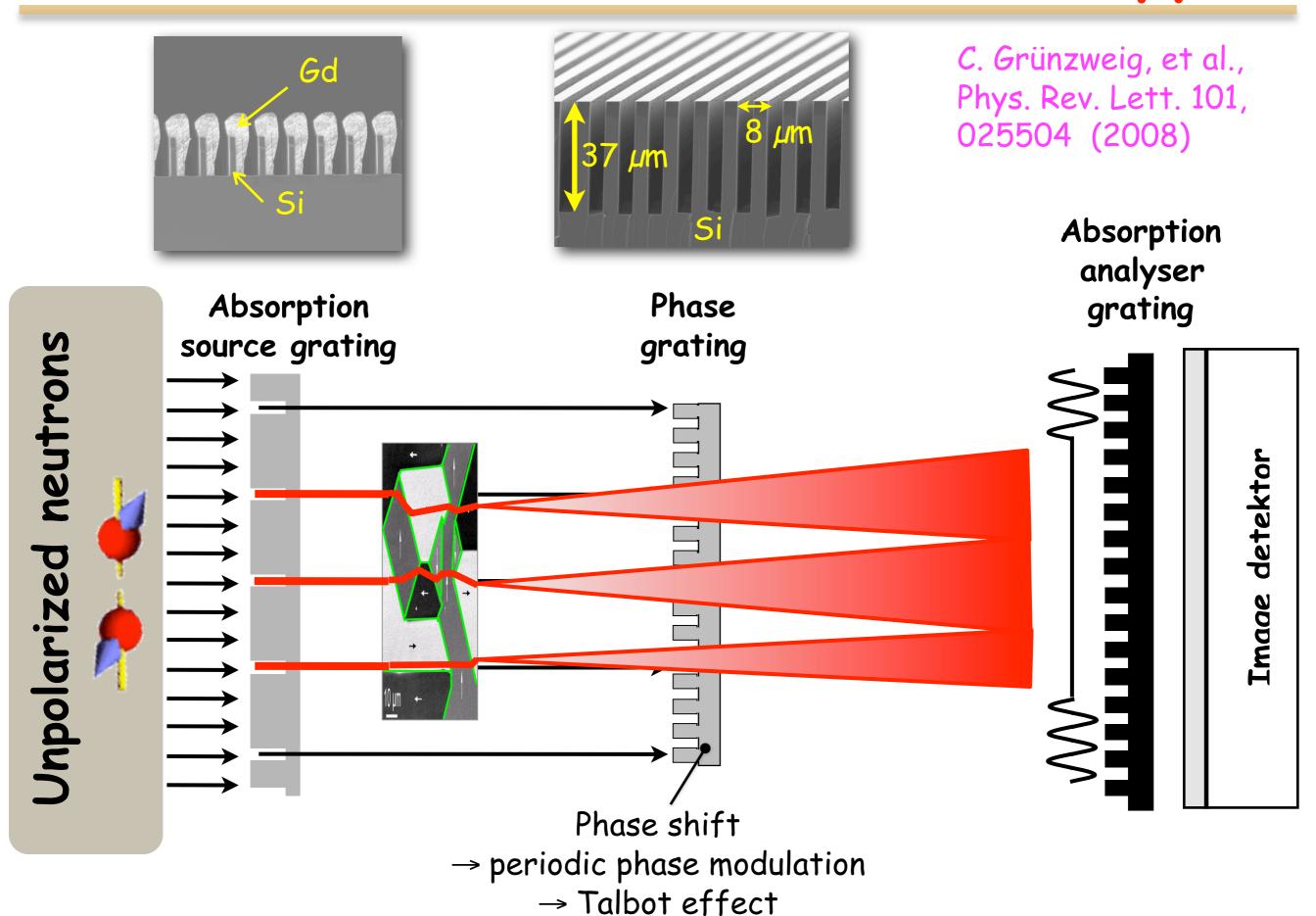
Interference pattern (period 4 μ m)





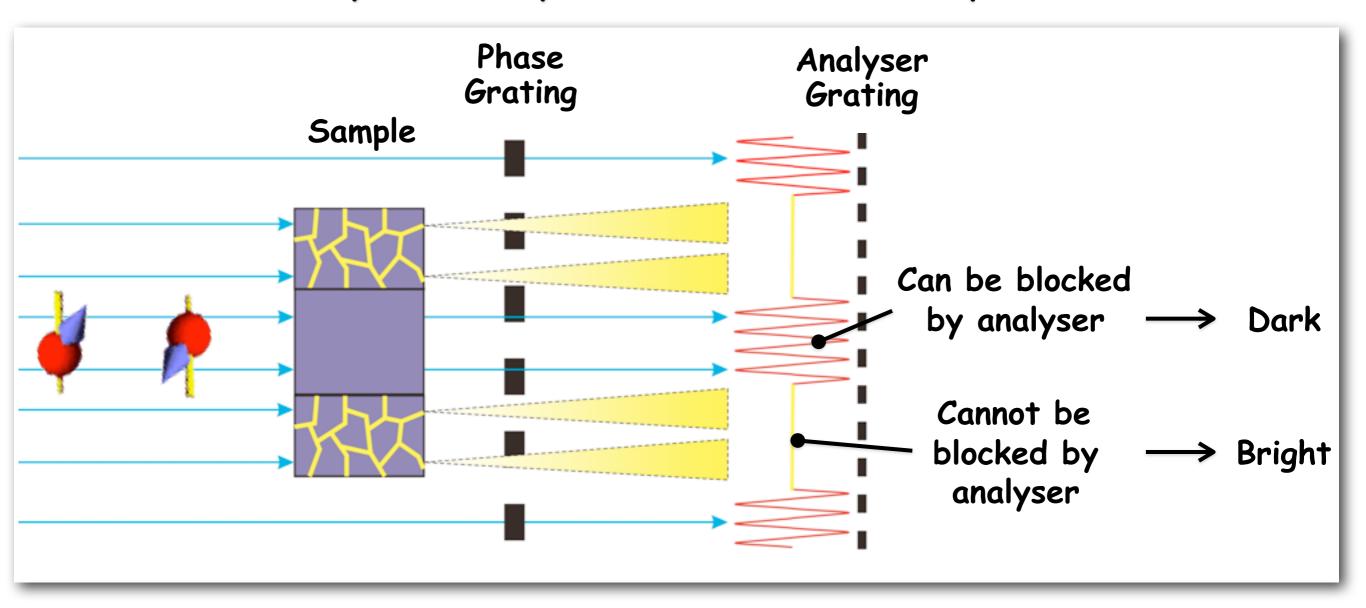




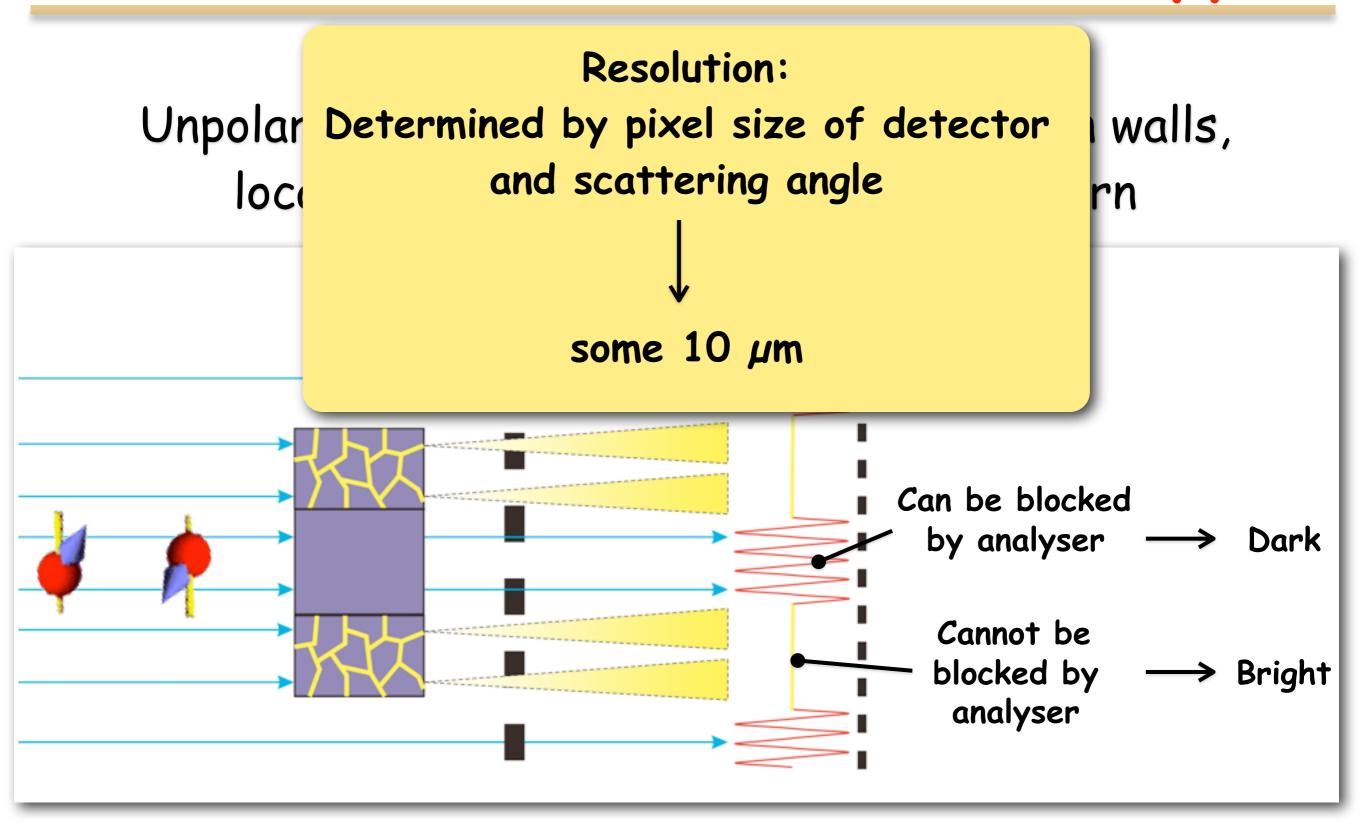


Principle:

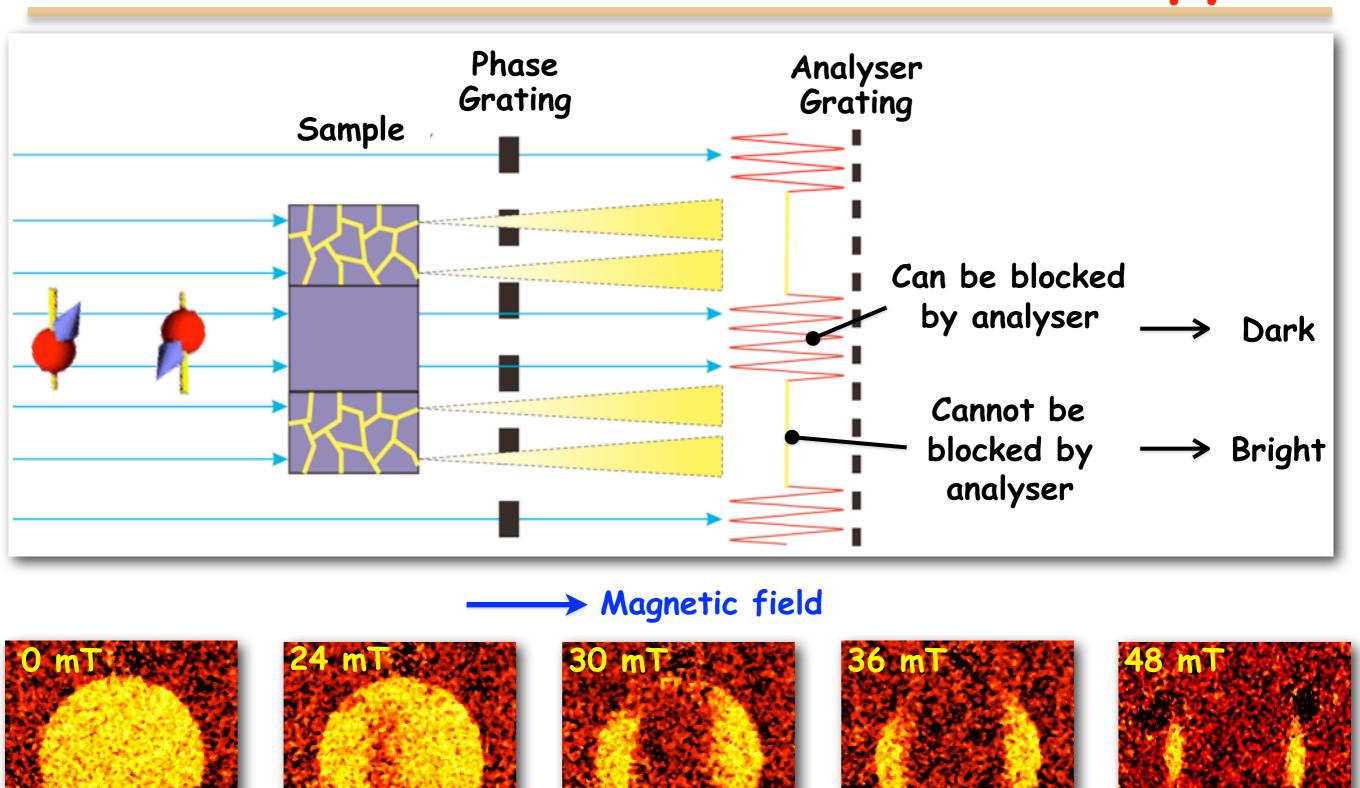
Unpolarized neutrons, refracted at domain walls, locally destroy the interference pattern



Bright contrast is caused by refraction
 Dark field imaging

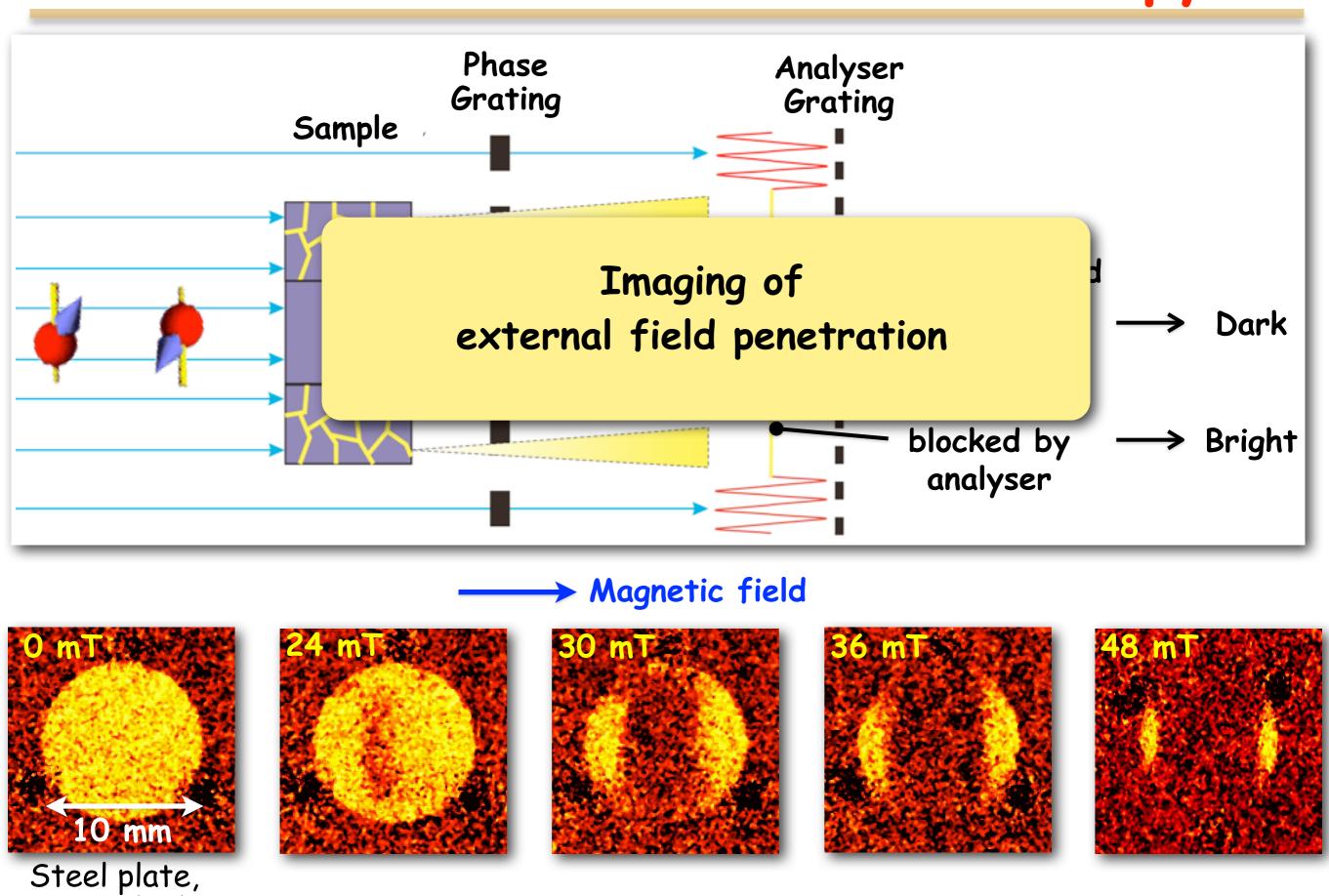


Bright contrast is caused by refraction
 Dark field imaging



Steel plate, 2 mm thick

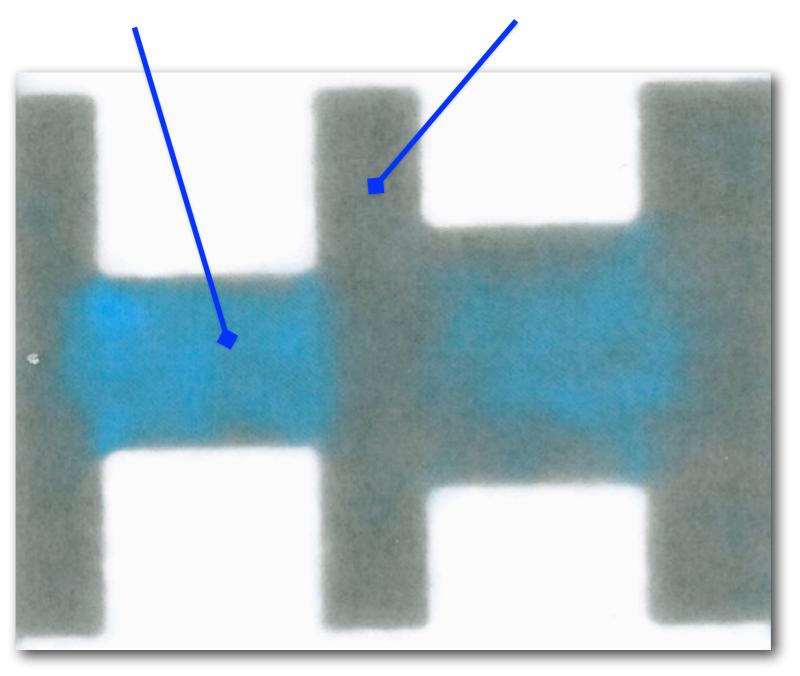
10 mm



2 mm thick

No walls: higher flux density

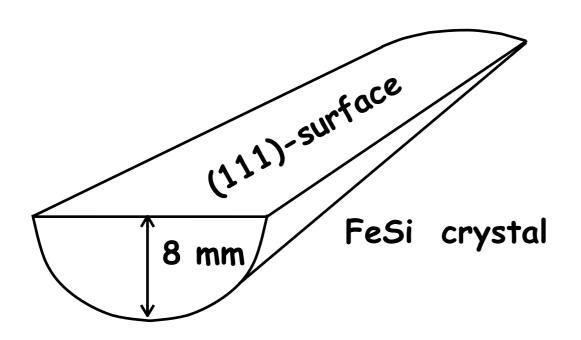
Many walls: lower flux density

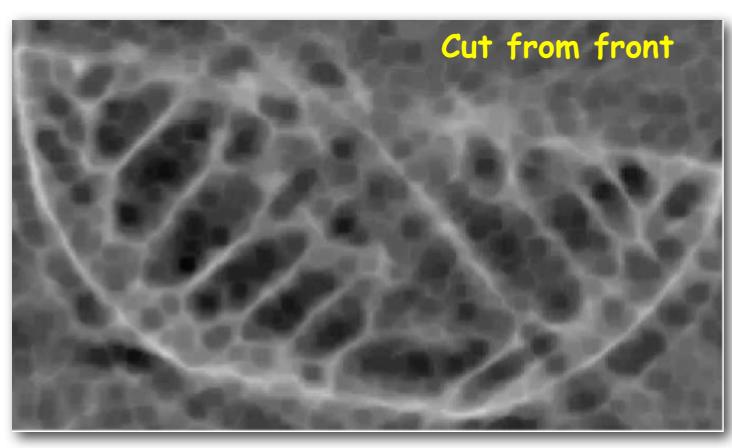


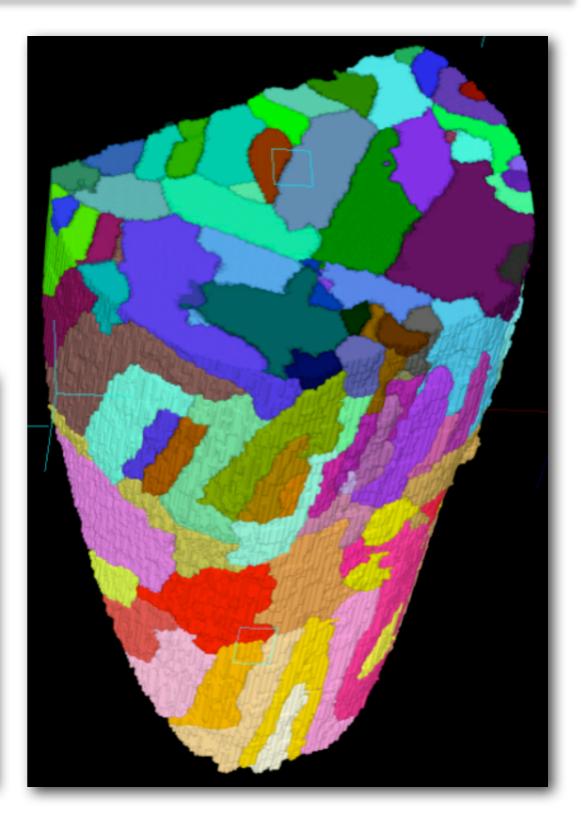
Non-oriented FeSi steel

Together with B. Betz and C. Grünzweig (PSI Villigen),
R. Siebert (Fraunhofer IWS Dresden)
unpublished

Magnetic field

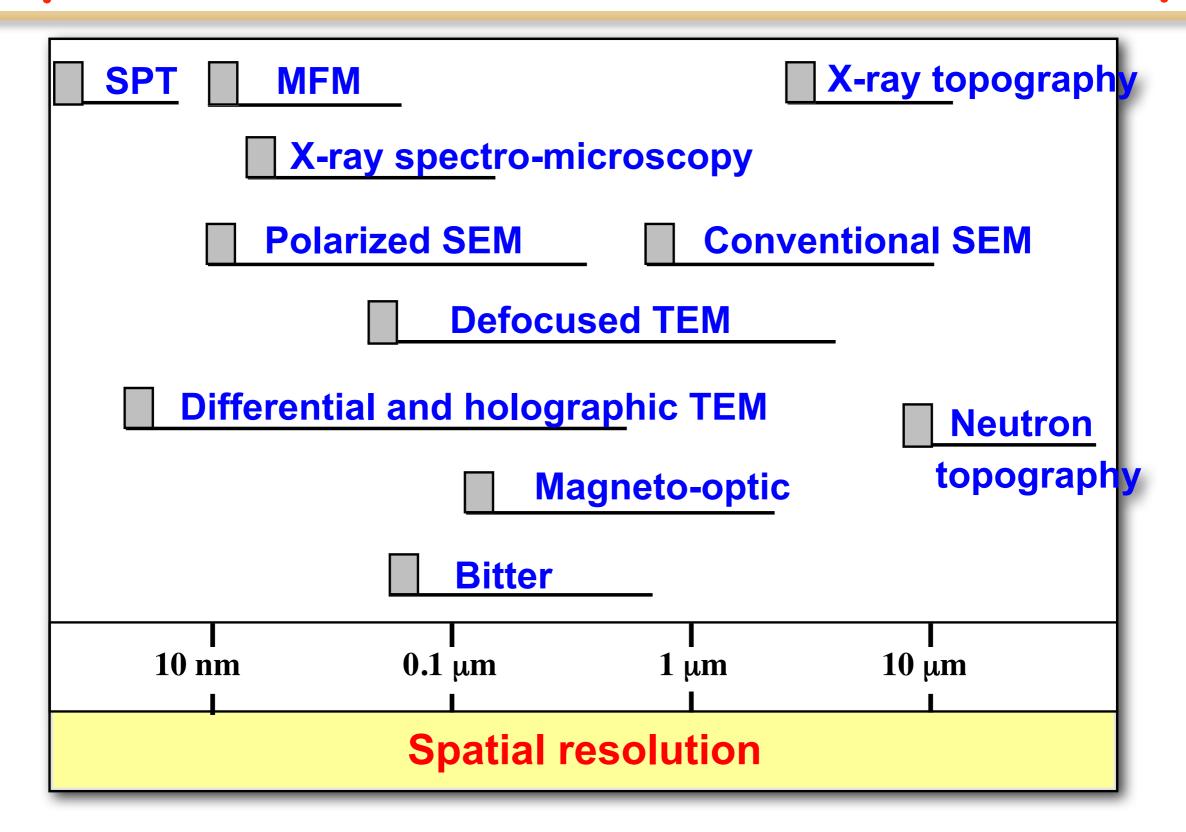






I. Manke, et al.: Three-dimensional imaging of magnetic domains. Nature Communications, 1:125 doi: 10.1038/ncomms1125 (2010)

Comparison of Domain Obervation Techniques



MFM: Magnetic Force Microscopy

SPT: Spin-Polarized Tunneling

SEM: Scanning (reflection) Electron Microscopy

TEM: Transmission Electron Microscopy